

Intrabeam Scattering and the Beam Life-Time

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Intrabeam Scattering and the Beam Life-Time

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Abstract

The Fokker-Planck equation is derived to describe the time evolution of the longitudinal density distribution of a bunched hadron beam in the presence of intrabeam scattering. A computer program has been developed to numerically solve this equation. Both the beam loss and bunch-shape evolution are investigated for the $^{197}\text{Au}^{79+}$ beams during the 10-hour storage in the proposed RHIC collider.

I. Introduction

The problem of intrabeam scattering, namely the Coulomb interaction between the particles in a beam, has been explored by many authors. Most of the theories¹⁻⁴ developed on this subject are concerned with the growth of the rms beam dimensions under the assumption that the particle distribution remains Gaussian in both transverse and longitudinal phase space, often disregarding aperture limitations and particle loss. Previous studies⁵ using this kind of theory indicate that during the 10-hour storage of the intense heavy-ion bunches in the RHIC, the growth of longitudinal bunch area and, consequently, the requirement on the rf voltage, are of primary concern. On the other hand, because the bunch area is in most cases comparable to the rf-bucket area, it is expected that particle loss through the edge of the rf bucket is appreciable. Under this circumstance, intrabeam-scattering calculation without taking into account the beam loss might not be adequate to describe the bunch behaviour.

This paper presents a new approach to the problem based on the Fokker-Planck equation⁶⁻¹⁰ for the density distribution function of the particles of the bunched beam in the presence of intrabeam scattering. Section II introduces the simplified transport equation which, in terms of the action variable J , describes the time evolution of the longitudinal distribution function. Both the dynamic friction and the diffusion coefficients are obtained in terms of the distribution function itself. A computer program is developed to solve the transport equation for given initial distribution and boundary conditions. Section III briefly addresses the numerical method used to evaluate the beam loss and to obtain the instantaneous particle distribution. Results are applied in section IV to the bunched beam of fully-stripped gold ions during the 10-hour storage in the RHIC collider.

II. Theoretical Approaches

A. The Fokker-Planck equation

A well known approach to the problem of treating changes in a distribution function resulting from frequently occurring “events”, each of which produces a small change in the configuration of the particles, is to use the Fokker-Planck equation. Let $x, x' \equiv \frac{dx}{dz}$ and y, y' be the horizontal and vertical displacements and velocities, respectively, and z the azimuthal displacement along the closed orbit. The longitudinal motion of the particles can either be described by the rf phase deviation ϕ and the energy deviation $W = \Delta E / h\omega_s$ or, equivalently, the action-angle variables Q and J .¹¹ Here h is the harmonic number, ΔE is the deviation from the synchronous energy, and ω_s is the synchronous revolution frequency.

Longitudinal distribution function $\Psi_{T,L}(x, x', y, y', Q, J; t)$ is defined as the number of particles per unit volume in the 6-dimensional phase space. The Fokker-Planck equation gives time rate of change of $\Psi_{T,L}$ due to intrabeam scattering in the laboratory frame as

$$\frac{\partial \Psi_{T,L}}{\partial t} = -\frac{\partial}{\partial x^\mu} \left(\Psi_{T,L} \frac{\langle \Delta x^\mu \rangle_C}{\Delta t} \right) + \frac{1}{2} \frac{\partial^2}{\partial x^\mu \partial x^\nu} \left(\Psi_{T,L} \frac{\langle \Delta x^\mu \Delta x^\nu \rangle_C}{\Delta t} \right), \quad \mu, \nu = x, x', y, y', Q, J, \quad (1)$$

where the time interval Δt , as observed in the laboratory frame, is long compared with the correlation time of the intrabeam-scattering process but short compared with other time scales. Δx^μ is the increment of x^μ during Δt . $\langle \rangle_C$ indicates the average over collision events. The derivation of this equation is based on the justified assumption that the distant collisions are of predominant importance, which implies that small changes in x^μ are the most probable and that terms involving higher powers of Δx^μ contribute negligibly to $\frac{\partial \Psi_{T,L}}{\partial t}$.

Rewrite the distribution function as the product of the longitudinal and the normal-

ized transverse distribution function,

$$\Psi_{T,L}(x, x', y, y', Q, J; t) = \rho_H(x, x'; t) \rho_V(y, y'; t) \Psi_L(Q, J; t), \quad (2)$$

where H and V refer to the horizontal and vertical dimensions, respectively. The 6-dimensional Fokker-Planck equation can be reduced to a 2-dimensional equation by integrating both sides of eq. 1 over all the transverse variables x , x' , y , and y' ,

$$\frac{\partial \Psi_L}{\partial t} = -\frac{\partial}{\partial x^\mu} \left(\Psi_L \frac{\langle \Delta x^\mu \rangle_{C,T}}{\Delta t} \right) + \frac{1}{2} \frac{\partial^2}{\partial x^\mu \partial x^\nu} \left(\Psi_L \frac{\langle \Delta x^\mu \Delta x^\nu \rangle_{C,T}}{\Delta t} \right), \quad (3)$$

$\mu, \nu = Q, J,$

where the subscript T denotes the average over all the transverse variables.

The time for intrabeam scattering to produce appreciable effect (or the time of relaxation) is typically much longer than the synchrotron-oscillation period, which is again much longer than the correlation time of the collision process. In this case, eq. 3 can be further simplified by averaging over the angle variable Q for one synchrotron-oscillation period,

$$\frac{\partial \Psi(J; t)}{\partial t} = -\frac{\partial}{\partial J} \left(\Psi(J; t) \frac{\langle \Delta J \rangle_{C,T,Q}}{\Delta T} \right) + \frac{1}{2} \frac{\partial^2}{\partial J^2} \left(\Psi(J; t) \frac{\langle (\Delta J)^2 \rangle_{C,T,Q}}{\Delta T} \right), \quad (4)$$

where the subscript Q denotes an additional average over Q , and ΔT corresponds to a time long compared with the synchrotron-oscillation period, but still short compared with the relaxation time. $\Psi(J; t)$ is the averaged distribution function in longitudinal phase space expressed in terms of the phase-space area J enclosed by the particle performing synchrotron oscillation.

For the examination of eq. 4, the coefficients must be expressed in approachable forms. Consider the Coulomb interaction of a “test” particle with the “media” particles of the beam. Using the action-angle variables, the longitudinal equations of motion of this test

particle can in general be described by

$$\begin{cases} \dot{Q} &= \frac{\Omega_s(J)}{2\pi} + \frac{\Delta Q}{\Delta t} \\ j &= \frac{\Delta J}{\Delta t}, \end{cases} \quad (5)$$

where the synchrotron-oscillation frequency Ω_s is a function of J only. For simplicity, the angle variable Q is normalized to 1 so that J presents the phase-space area.

In eq. 5, $\frac{\Delta Q}{\Delta t}$ and $\frac{\Delta J}{\Delta t}$ are the time rates of change in Q and J due to the collisions. Since the change in distribution is small within one synchrotron-oscillation period, both $\frac{\Delta Q}{\Delta t}$ and $\frac{\Delta J}{\Delta t}$ can be written as periodic functions in Q . It is thus straightforward to verify that the average of these quantities can be expressed as

$$\frac{\langle \Delta J \rangle_{C,T,Q}}{\Delta T} \approx F^0(J;t) + F^1(J;t), \quad (6)$$

where

$$F^0(J;t) = \int_0^1 dQ \left. \frac{\langle \Delta J \rangle_{C,T}}{\Delta t} \right|_0, \quad F^1(J;t) = \frac{1}{2} \frac{d}{dJ} \left[\int_0^1 dQ \left. \frac{\langle (\Delta J)^2 \rangle_{C,T}}{\Delta t} \right|_0 \right] = \frac{1}{2} \frac{dD(J;t)}{dJ}, \quad (7)$$

and

$$\frac{\langle (\Delta J)^2 \rangle_{C,T,Q}}{\Delta T} \approx D(J;t) = \int_0^1 dQ \left. \frac{\langle (\Delta J)^2 \rangle_{C,T}}{\Delta t} \right|_0. \quad (8)$$

The subscript 0 in eqs. 7 and 8 implies that the integration over Q is performed along the contours of particle motion in the absence of intrabeam scattering for one synchrotron-oscillation period.

As a result of these considerations, the Fokker-Planck equation can finally be simplified as a partial differential equation in J and t with simple coefficients for the determination of the distribution function Ψ ,

$$\frac{\partial \Psi}{\partial t} = -\frac{\partial}{\partial J} (F^0 \Psi) + \frac{1}{2} \frac{\partial}{\partial J} \left(D \frac{\partial \Psi}{\partial J} \right). \quad (9)$$

The boundary condition to this equation is that Ψ vanishes at the separatrix \hat{J} , and that the flux vanishes at $J = 0$, i.e.

$$\begin{cases} J = 0 : & -F^0\Psi + \frac{D}{2}\frac{\partial\Psi}{\partial J} = 0 , \\ J = \hat{J} : & \Psi = 0 . \end{cases} \quad (10)$$

The coefficient D of diffusion is always positive, indicating the tendency of bunch-area growth due to intrabeam scattering. The existence of a non-zero coefficient F^0 of dynamic friction reflects the non-uniform environment seen by the test particles in velocity space. Both F^0 and D are dependent on the particle distribution itself. Their explicit expressions will be derived in the following subsections.

B. The canonical transformation

The increment ΔJ in the action J of the test particle can be related to that in the energy deviation W by a transformation. In terms of ϕ and W , the longitudinal equations of motion become

$$\begin{cases} \dot{W} &= \frac{qe\hat{V}}{2\pi h} [\sin(\phi_s + \phi) - \sin \phi_s] + \frac{\Delta W}{\Delta t} \\ \dot{\phi} &= \frac{h^2\omega_s^2\eta}{E\beta^2} W , \end{cases} \quad (11)$$

where \hat{V} is the peak voltage, $\eta = 1/\gamma_T^2 - 1/\gamma^2$, γ_T is the transition energy, $E = Am_0c^2\gamma$ and βc are the synchronous energy and velocity, respectively, and q and A are the charge and atomic number of the particles. For simplicity, the synchronous phase ϕ_s will be taken as π , which represents the storage mode above transition in the RHIC.

Regarding the rate of energy increment $\frac{\Delta W}{\Delta t}$ due to intrabeam scattering as a perturbation, the unperturbed particle motion is derivable from an Hamiltonian

$$H(\phi, W) = C_W W^2 + C_\phi \sin^2 \frac{\phi}{2}, \quad (12)$$

where

$$C_W = \frac{h^2 \omega_s^2 \eta}{2E\beta^2} \quad \text{and} \quad C_\phi = \frac{qe\hat{V}}{\pi h}$$

may be time dependent. The transformation to the action-angle variables may be achieved by means of a generating function of Goldstein's second type,¹²

$$F_2(\phi, J; t) = \int^\phi \sqrt{\frac{1}{2\pi C_W} \int^J \Omega_s(J') dJ' - \frac{C_\phi}{C_W} \sin^2 \frac{\phi'}{2}} d\phi'. \quad (13)$$

Obviously, the action variable J is an invariant of motion in the absence of intrabeam scattering,

$$J = \oint W d\phi = 8\sqrt{\frac{C_\phi}{C_W}} [(k^2 - 1)K(k) + E(k)], \quad k = \sqrt{\frac{H}{C_\phi}} \leq 1, \quad (14)$$

where

$$K(k) = \int_0^{\frac{\pi}{2}} \frac{dt}{\sqrt{1 - k^2 \sin^2 t}}, \quad \text{and} \quad E(k) = \int_0^{\frac{\pi}{2}} \sqrt{1 - k^2 \sin^2 t} dt \quad (15)$$

are the complete elliptical integrals¹³ of first and second kind. The synchrotron-oscillation frequency

$$\Omega_s = 2\pi\dot{Q} = \frac{\pi\sqrt{C_W C_\phi}}{2K(k)}, \quad k \leq 1, \quad (16)$$

is a monotonic function of J . At the boundary (separatrix) of the stable region, $\hat{J} = 8\sqrt{\frac{C_\phi}{C_W}}$, and $\Omega_s(\hat{J}) = 0$.

The contribution $\frac{\Delta W}{\Delta t}$ from intrabeam scattering is a function of ϕ and W of the test particle. This part is not derivable from an Hamiltonian. Due to this contribution, the action J generally increases with time, which results a growth in bunch area. Using eq. 14 and the canonical relations, the rate of increment in J can be expressed in terms of $\frac{\Delta W}{\Delta t}$ as

$$\frac{\Delta J}{\Delta t} = \left. \frac{\partial W}{\partial J} \right|_\phi^{-1} \frac{\Delta W}{\Delta t}. \quad (17)$$

It follows from ref. 11 that the coefficient in eq. 17 can be written as a series expansion using the order parameter

$$\xi = \exp[-\pi K'(k)/K(k)], \quad K'(k) = K(\sqrt{1 - k^2}),$$

as

$$\left. \frac{\partial W}{\partial J} \right|_{\phi}^{-1} = 8k K(k) \cos 2\pi Q \left[1 - 4\xi \sin^2 2\pi Q + O(\xi^2) \right], \quad (18)$$

where k is a function of J only (eq. 14). Note that ξ becomes significant only near the separatrix (fig. 1 in ref.11).

C. Rutherford scattering in the rest frame

It is convenient to evaluate the rate of energy increment $\frac{\Delta W}{\Delta t}$ in the rest frame of the synchronous particle where the motion of particles in the bunch is non-relativistic. The four components of the momentum vector in the rest frame can be expressed in terms of those in the laboratory frame by means of the Lorentz transformation,

$$\begin{cases} \bar{p}_{x,y} &= p_{x,y}, \\ \bar{p}_z &\approx \frac{Am_0c}{\beta} \frac{\Delta\gamma_z}{\gamma}, \\ \bar{E} &\approx Am_0c^2, \end{cases} \quad (19)$$

where the bar indicates the value in the rest frame. β and γ again represent the synchronous values.

Let $\mathbf{u} = \bar{\mathbf{v}}_1 - \bar{\mathbf{v}}_2$ denote the relative velocity between the test particle 1 and a media particle 2 in the beam observed in the rest frame. $u = |\mathbf{u}|$ is related to the three momentum components in the laboratory frame by

$$u \approx \beta c \sqrt{\left(\frac{\Delta p_1}{p} - \frac{\Delta p_2}{p} \right)^2 + \gamma^2 (x'_1 - x'_2)^2 + \gamma^2 (y'_1 - y'_2)^2}. \quad (20)$$

To evaluate $\frac{\Delta W}{\Delta t}$, Rutherford's formula is used for the cross section of the Coulomb scattering,

$$\sigma(u, \theta) = \frac{q^4 e^4}{A^2 m_0^2 u^4 \sin^4 \theta / 2}, \quad (21)$$

where θ is the angle through which the velocity vector \mathbf{u} undergoes a rotation during the collision. Integrating over both θ and the azimuthal scattering angle, the change in

the longitudinal component of the velocity of the test particle and its square per unit rest-frame time can be shown as

$$\langle \Delta \bar{v}_{z1} \rangle_{\Omega} = -2\Gamma \frac{u_z}{u^3}, \quad \text{and} \quad \langle (\Delta \bar{v}_z)_1^2 \rangle_{\Omega} = \Gamma \frac{u_x^2 + u_y^2}{u^3}, \quad (22)$$

where

$$\Gamma \equiv \frac{4\pi q^4 e^4 \text{Log}}{A^2 m_0^2}, \quad \text{Log} \equiv -\ln \sin \frac{\theta_{min}}{2},$$

and θ_{min} is the minimum scattering angle. The Coulomb logarithm Log can be verified to be much larger than 1. This fact implies that the Fokker-Planck equation is a good approximation to describe the particle motion. Because of the insensitivity of Log to the precise value of u , a fixed value of 20 is currently designated to Log to simplify further development.

Based on the results of eq. 22, it is possible to evaluate the time rate of average energy increment of the test particle in the laboratory frame by integrating over all the velocity components of the media particles involved in the collision ($x_2 = x_1$ and $y_2 = y_1$),

$$\begin{aligned} \frac{\langle \Delta W \rangle_C}{\Delta t} &= \frac{1}{\gamma} \frac{\beta E}{h \omega_{sc}} \int dx'_2 \rho_{x_\beta x'_\beta}(x_{\beta 2}, x'_{\beta 2}; t) \int dy'_2 \rho_{yy'}(y_2, y'_2; t) \\ &\quad \frac{h}{\gamma R} \int dW_2 \Psi[J(\phi_1, W_2)] \langle \Delta \bar{v}_{z1} \rangle_{\Omega}, \\ \frac{\langle (\Delta W)^2 \rangle_C}{\Delta t} &= \frac{1}{\gamma} \left(\frac{\beta E}{h \omega_{sc}} \right)^2 \int dx'_2 \rho_{x_\beta x'_\beta}(x_{\beta 2}, x'_{\beta 2}; t) \int dy'_2 \rho_{yy'}(y_2, y'_2; t) \\ &\quad \frac{h}{\gamma R} \int dW_2 \Psi[J(\phi_1, W_2)] \langle (\Delta \bar{v}_z)_1^2 \rangle_{\Omega}. \end{aligned} \quad (23)$$

Note that the horizontal displacement of the particle from the closed orbit is the sum of the contribution of betatron oscillation and momentum deviation,

$$x = x_\beta + x_p \frac{\Delta p}{p}, \quad \text{and} \quad x' = x'_\beta + x'_p \frac{\Delta p}{p}, \quad (24)$$

where x_p is the horizontal dispersion function. The three integrals in eq. 23 refer to the horizontal, vertical, and longitudinal components of velocity of the media particles,

respectively, and $2\pi R$ is the circumference of the machine. Obviously, the evaluation of the first two integrals requires the knowledge of the transverse distribution which is generally time dependent.

D. Evaluation of the dynamic-friction and the diffusion coefficients

According to the previous studies⁵ on intrabeam scattering, the transverse emittance of the beam is expected to be much smaller than the transverse admittance during the entire 10-hour period of operation in the RHIC. Beam loss in transverse direction due to intrabeam scattering is therefore negligible. Under this circumstance, the distribution in horizontal and vertical phase space may be assumed as

$$\begin{aligned}\rho_{x_\beta x'_\beta}(x_\beta, x'_\beta; t) &= \frac{\sqrt{1 + \alpha_x^2}}{2\pi\sigma_{x_\beta}\sigma_{x'_\beta}} \exp \left[-\frac{1 + \alpha_x^2}{2} \left(\frac{x_\beta^2}{\sigma_{x_\beta}^2} + \frac{2\alpha_x x_\beta x'_\beta}{\sqrt{1 + \alpha_x^2}\sigma_{x_\beta}\sigma_{x'_\beta}} + \frac{x'^2_\beta}{\sigma_{x'_\beta}^2} \right) \right] \\ \rho_{yy'}(y, y'; t) &= \frac{\sqrt{1 + \alpha_y^2}}{2\pi\sigma_y\sigma_{y'}} \exp \left[-\frac{1 + \alpha_y^2}{2} \left(\frac{y^2}{\sigma_y^2} + \frac{2\alpha_y y y'}{\sqrt{1 + \alpha_y^2}\sigma_y\sigma_{y'}} + \frac{y'^2}{\sigma_{y'}^2} \right) \right].\end{aligned}\quad (25)$$

The time dependence of the transverse distribution can be expressed through the normalized transverse emittance $\epsilon_{Nx,y}$,

$$\sigma_{x_\beta, y} = \sqrt{\frac{\beta_{x,y}\epsilon_{Nx,y}(t)}{6\beta\gamma}}, \quad \sigma_{x'_\beta, y'} = \sqrt{\frac{(1 + \alpha_{x,y}^2)\epsilon_{Nx,y}(t)}{6\beta\gamma\beta_{x,y}}}, \quad (26)$$

where $\beta_{x,y}$ and $\alpha_{x,y}$ are the Courant-Snyder lattice parameters. The time variation in $\epsilon_{Nx,y}$ is in principle determined by the instantaneous bunch configuration under intrabeam scattering.

Based on the above assumptions on the transverse distribution, the evolution of the longitudinal distribution function can be determined by the transport equation (eq. 9) under the boundary condition (eq. 10). Define dimensionless quantities

$$\kappa = \frac{1}{\gamma} \left(\frac{\Delta p_1}{p} - \frac{\Delta p_2}{p} \right), \quad a = \frac{1}{2} \sqrt{\frac{6\beta\gamma\beta_{x,y}}{\epsilon_{Nx,y}}}, \quad b = \left| \frac{\gamma\kappa}{2\sigma_{x_\beta}} (\beta_x x'_p + \alpha_x x_p) \right|. \quad (27)$$

Substituting eqs. 17 and 23 into eqs. 7 and 8 and employing the above definition, the coefficients F^0 and D can finally be obtained by integrating over all the transverse components ($x_{\beta 1}$, $x'_{\beta 1}$, y_1 , and y'_1) of the test particle,

$$F^0(J) = \int \frac{2dz}{\pi R} \int_0^{\frac{1}{4}} dQ \left. \frac{\partial W}{\partial J} \right|_{\phi}^{-1} (Q, J) \int_{J_{\min}}^J \left. \frac{\partial W}{\partial J} \right|_{\phi} (Q', J') [A_F(\kappa_1) + A_F(\kappa_2)] \Psi(J') dJ', \quad (28)$$

and

$$D(J) = \int \frac{2dz}{\pi R} \int_0^{\frac{1}{4}} dQ \left[\left. \frac{\partial W}{\partial J} \right|_{\phi}^{-1} (Q, J) \right]^2 \int_{J_{\min}}^J \left. \frac{\partial W}{\partial J} \right|_{\phi} (Q', J') [A_D(\kappa_1) + A_D(\kappa_2)] \Psi(J') dJ', \quad (29)$$

where $\kappa_{1,2} = \frac{h\omega_s}{\gamma\beta^2 E} (W \mp W')$, and

$$\begin{aligned} A_F(\kappa) &= -2\Gamma \frac{1}{\gamma} \frac{\beta E}{h\omega_s c} \frac{h}{\gamma R} \frac{1}{(\beta c \gamma)^2} \frac{1}{4\pi\sigma_{x\beta}\sigma_y} I_F(\kappa), \\ A_D(\kappa) &= \Gamma \frac{1}{\gamma} \left(\frac{\beta E}{h\omega_s c} \right)^2 \frac{h}{\gamma R} \frac{1}{\beta c \gamma} \frac{1}{4\pi\sigma_{x\beta}\sigma_y} I_D(\kappa). \end{aligned} \quad (30)$$

The first integral in eqs. 28 and 29 represents the average over the machine lattice; the second integral represents the average over synchrotron-oscillation period; while the third integral describes the contribution from particles of different action J' involved in the collision. Fig. 1 shows that for given J and Q , the integration over J' is performed such that $k(J') \sin 2\pi Q' \approx \sin [\phi(Q, J)/2]$, extending from J_{\min} to the separatrix \hat{J} , with $k(J_{\min}) \approx [\sin \phi(Q, J)/2]$. It is evident that the time dependence of F^0 and D is governed by the instantaneous longitudinal distribution function Ψ and the transverse emittance.

For a round beam with $\beta_x/\epsilon_{Nx} \sim \beta_y/\epsilon_{Ny}$ on the average, the quantities I_F and I_D in eq. 30 can be obtained in integral forms,

$$\begin{aligned} I_F(\kappa) &= \frac{4a^2\chi\lambda}{\pi} \int_0^\infty \frac{e^{-\rho^2} E(r) \rho d\rho}{[(\rho - b)^2 + \lambda^2][(\rho + b)^2 + \lambda^2]^{\frac{1}{2}}} \\ I_D(\kappa) &= \frac{4a\chi}{\pi} \int_0^\infty \frac{e^{-\rho^2} \rho d\rho}{[(\rho + b)^2 + \lambda^2]^{\frac{1}{2}}} \left[K(r) - \frac{\lambda^2 E(r)}{(\rho - b)^2 + \lambda^2} \right], \end{aligned} \quad (31)$$

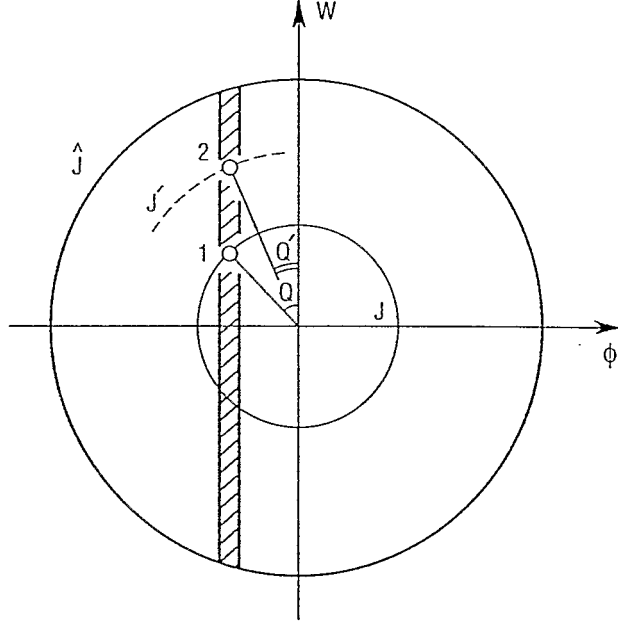


Figure 1: Integration in longitudinal phase space.

where

$$\lambda = a\kappa, \quad r = \left[\frac{4b\rho}{(\rho - b)^2 + \lambda^2} \right]^{\frac{1}{2}}, \quad \text{and} \quad \chi = \exp \left[- \left(\frac{x_p \gamma \kappa}{2\sigma_{x_\beta}} \right)^2 \right]. \quad (32)$$

If, as in many cases, $\beta_x x'_p + \alpha_x x_p \sim 0$, the integrals in eq. 32 can be performed to yield simpler expressions in terms of the error function Φ ,

$$\begin{aligned} I_F(\kappa) &= 2a^2 \text{sgn}(\kappa) \chi \left\{ 1 - \sqrt{\pi} |\lambda| e^{\lambda^2} [1 - \Phi(\lambda)] \right\} \\ I_D(\kappa) &= a\chi \left\{ \sqrt{\pi} (1 + 2\lambda^2) e^{\lambda^2} [1 - \Phi(\lambda)] - 2|\lambda| \right\}, \end{aligned} \quad (33)$$

where $\text{sgn}(\kappa)$ is 1 if $\kappa \geq 0$, and is -1 if otherwise. χ represents the damping effect of the dispersion x_p on the diffusion process. Intuitively, the dispersion effectively increases the transverse beam size σ_{x_β} by the amount $x_p \sigma_{\Delta p/p}$. The diffusion rate is therefore decreased accordingly.

Analytical solutions to the non-linear partial differential equation (eq. 9 with eqs. 28, 29, 30 and 33) with the boundary condition (eq. 10) and the initial condition $\Psi(J; 0)$, are in general difficult to obtain. Fortunately, computer algorithm can be developed to

numerically achieve an iterative solution $\Psi(J, t)$. Once $\Psi(J, t)$ is known, both beam loss and particle distribution in longitudinal space can be readily obtained.

III. Computer Techniques

The computer program originally developed for the investigation of the bunched-beam stochastic cooling¹¹ has been modified to study the intrabeam scattering. First, the J -space $(0, \hat{J})$ is equally divided into N_J bins of width ΔJ . Assumed as a truncated Gaussian in phase space, an initial distribution $\Psi(J_i, 0)$, $i = 1, \dots, N_J$, is then generated. The evolution of the distribution function $\Psi(J; t)$ is obtained by numerically iterating the transport equation which is written in a difference form, while keeping the boundary condition satisfied. The change in bunch area, i.e. the first moment $(\sum_{i=1}^{N_J} J_i \Psi(J_i) \Delta J)$ in J , is used to obtain the growth rate, while the zeroth moment $(\sum_{i=1}^{N_J} \Psi(J_i) \Delta J)$ in J is used to determine the particle loss.

During the entire period the distribution in transverse phase space is assumed to be Gaussian. The instantaneous rate of change of the transverse emittance is provided by the standard intrabeam-scattering calculations.⁴

IV. Application to the RHIC

Once the transport equation and the computer techniques are developed, the problem of beam life-time and bunch-area growth originated from intrabeam scattering can be readily approached. In this section, we apply the results to the storage of heavy-ion beams in the RHIC collider.

The heavy-ion beams will be stored in the RHIC for experiments at the energy of 100 GeV per nucleon using the 160 MHz, $h = 2052$ rf system. Consider the beam of one of the highest charge-state ions $^{197}\text{Au}^{79+}$ in the RHIC where intrabeam scattering is

expected to be the severest. Each of the 57 or 114 bunches circulating in the ring contains 10^9 particles. With the currently designed lattice, it is assumed that $\overline{\beta_{x,y}} \approx 25\text{m}$, and that $x_p/\sqrt{\beta_x} \approx 0.22\text{m}^{1/2}$. The initial bunch area is assumed to be $0.3\text{eV}\cdot\text{s}$ per nucleon.

In the following, we study several operational scenarios for the RHIC storage using either a constant rf voltage, or a voltage programmed to achieve the so-called “tight bucket”, with or without the initial blow-up of the transverse emittance.

A. Constant voltage with initial emittance blow-up

For the purpose of minimizing beam growth and luminosity variation during the storage, it is suggested that the transverse emittance should be initially blown-up to a normalized value of $60\pi\text{mm}\cdot\text{mrad}$. Thereafter the growth in transverse emittance is small.¹⁴

Keeping the peak rf voltage at a constant value of 4.5MV , fig. 2 shows the time evolution of the distribution function $\Psi(J)$ in J during the 10-hour period of operation. The area of the rf bucket is about $1.5\text{eV}\cdot\text{s}/\text{amu}$. The initial time $t = 0$ corresponds to the moment that the ion bunches are transferred from the $h = 342$ rf system for acceleration to the $h = 2052$ rf system for storage. Fig. 3 shows the initial and final line-density distribution as a function of the azimuthal displacement (ϕ) along the ring. It is indicated in fig. 4 that beam loss becomes significant after about 3 hours when the bunch area is comparable with the bucket area and, at the same time, when the growth in bunch length σ_l starts to saturate (fig. 5). The total beam loss during the 10-hour period is about 20%.

It is observed that the final distribution in longitudinal phase space (ϕ, W) is Gaussian-like, independent of the initial distribution. The final ratio of the bucket area to the average phase-space area $\langle J \rangle$ of the beam is about 3~4, which again depends weakly on

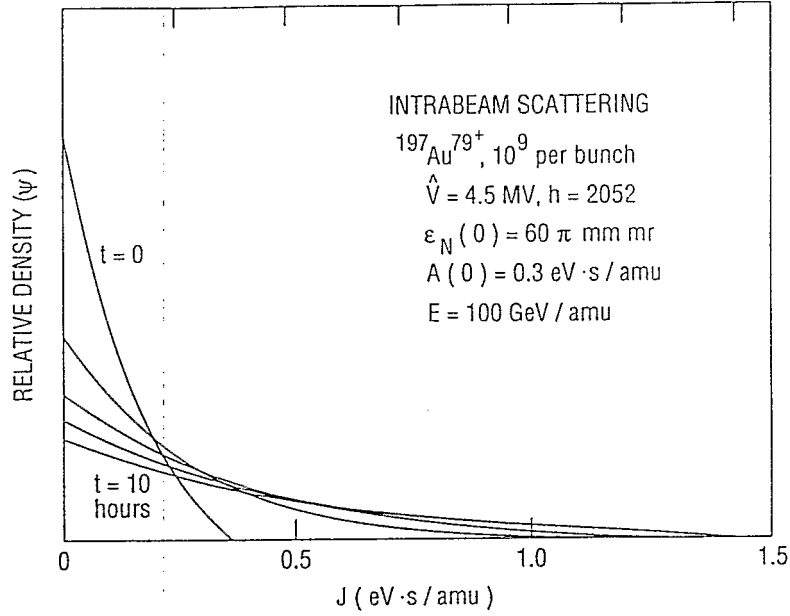


Figure 2: Evolution of the longitudinal distribution function Ψ as a function of longitudinal phase space area J . ($t=0, 2.5, 5, 7.5$, and 10 hour).

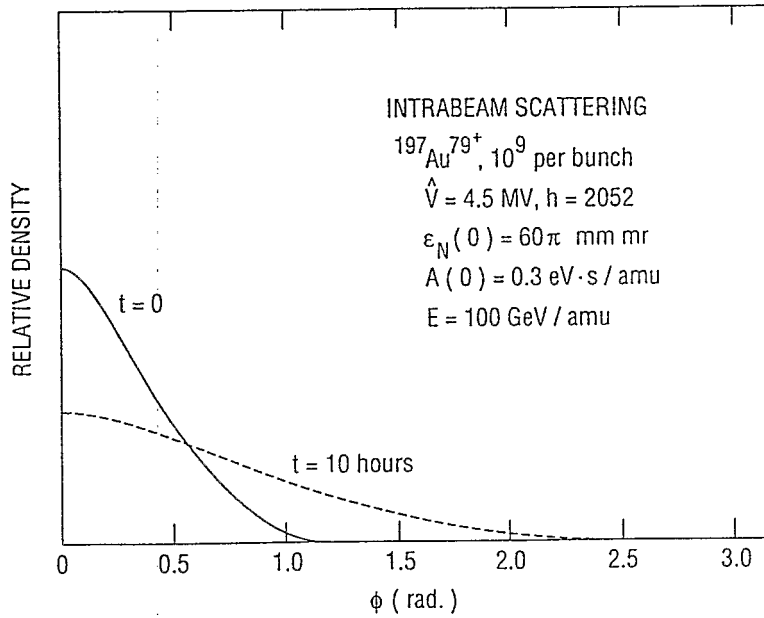


Figure 3: The initial and final density distribution along the azimuthal displacement ϕ .

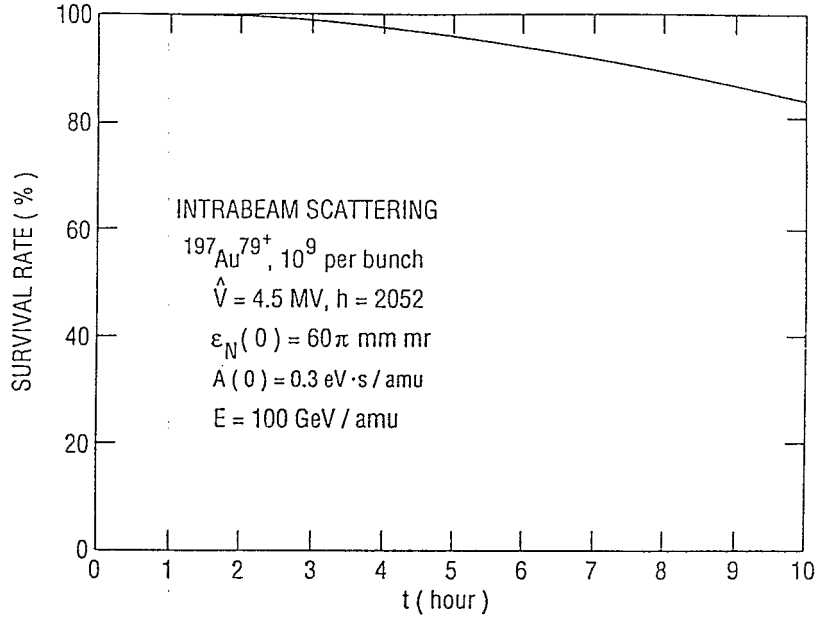


Figure 4: The beam survival rate as a function of time during the 10-hour operation.

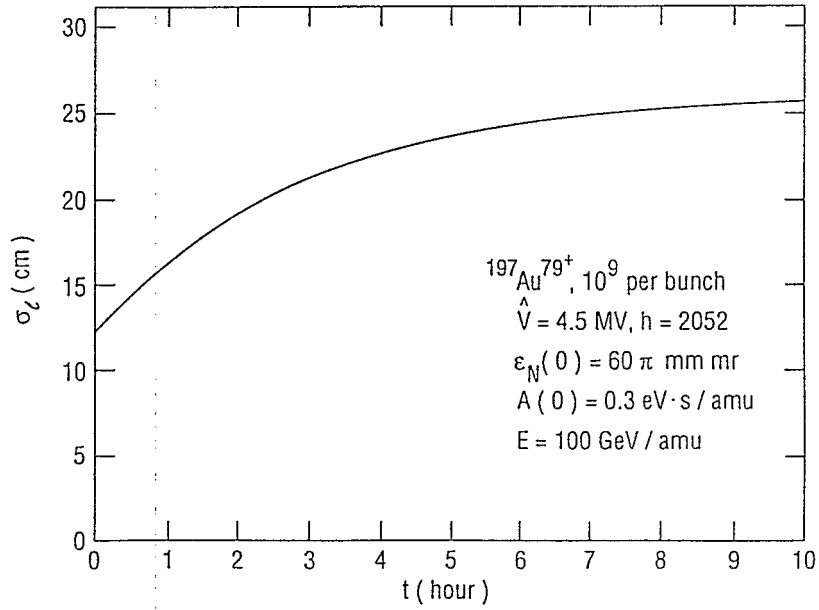


Figure 5: The growth in rms bunch length due to intrabeam scattering during the 10-hour operation.

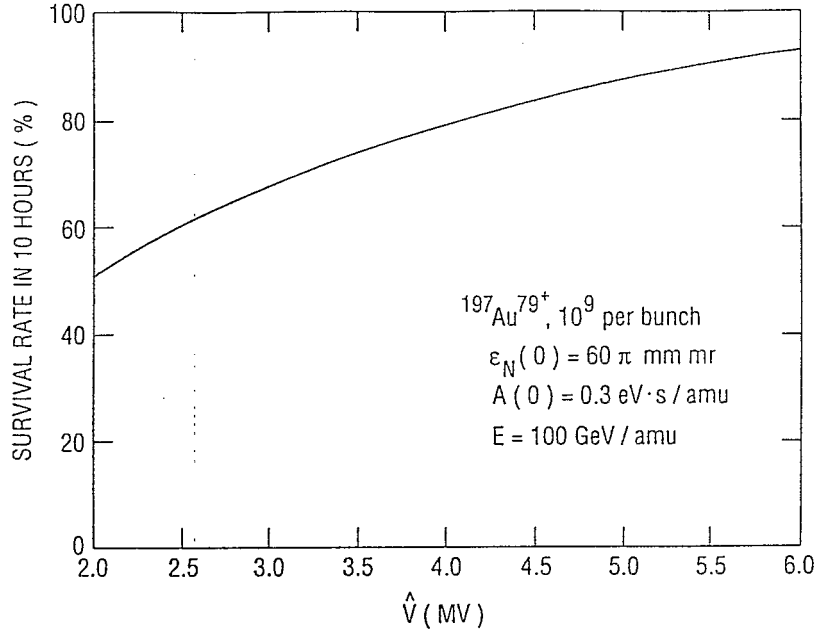


Figure 6: The final beam survival rate as a function of the peak rf voltage for the 10-hour operation using a constant rf voltage.

the initial conditions. During the operation the rms bunch length σ_l varies from about 12cm to 27cm.

Figs. 6 and 7 show the final beam survival rate and bunch lengths as functions of the constant peak voltage. A larger peak voltage provides a larger bucket area which allows a larger bunch. Both the loss rate and the growth rate of this larger bunch are smaller. Therefore, the total beam loss reduces with the increasing peak voltage.

B. Tight bucket with initial emittance blow-up

If a constant bunch length is required during the operation, the rf voltage has to be programmed to accommodate the beam growth due to intrabeam scattering. The “tight bucket” condition resulted from this programming implies that the ratio of the bucket area to the bunch area is a constant.

The criterion for the voltage programming adopted in our computer calculation is that

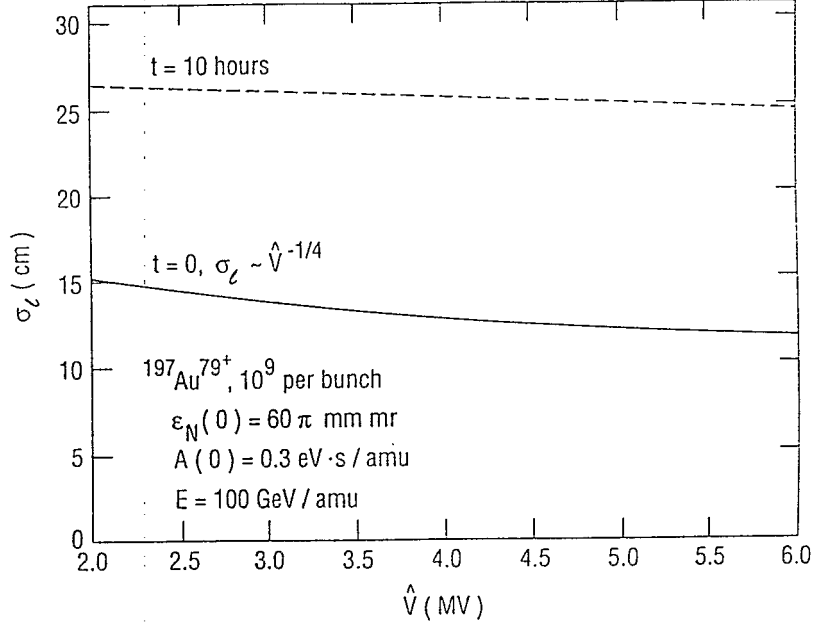


Figure 7: The initial and final bunch length as a function of the peak rf voltage for the 10-hour operation using a constant rf voltage.

the bucket area A_B is about 3.5 times that of the average area $\langle J \rangle$. Correspondingly, the ratio of the maximum momentum spread Δ_B of the bucket to the rms momentum spread $\sigma_{\Delta p/p}$ of the bunch is[†] about 2.5. The programming of the peak voltage to satisfy this criterion is shown in fig. 8. During the early period of operation, the voltage increases drastically to accommodate the fast growth in bunch area. Since the bunch area is always comparable to the bucket area, beam loss is severe (fig. 9) during the entire period. The growth rate decreases with the increasing bunch size and the decreasing beam intensity. The required voltage reaches 4.5MV in 10 hours. The total beam loss is 50~60%.

C. Constant voltage without initial emittance blow-up

The initial normalized transverse emittance without the blow-up is about $10\pi\text{mm-mrad}$. Due to this small value, the beam grows appreciably in both the transverse and the

[†] The originally proposed⁵ tight-bucket criterion is $\Delta_B/\sigma_{\Delta p/p} = 2$. However, this can not be realized in the calculation when the beam loss at the boundary is taken into account.

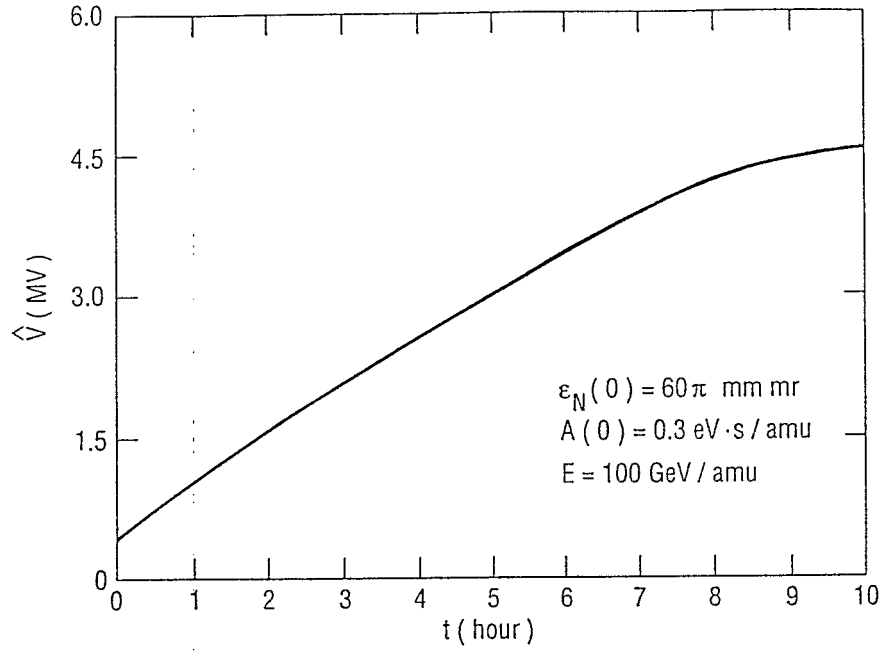


Figure 8: The programming of the peak rf voltage during the tight-bucket operation.

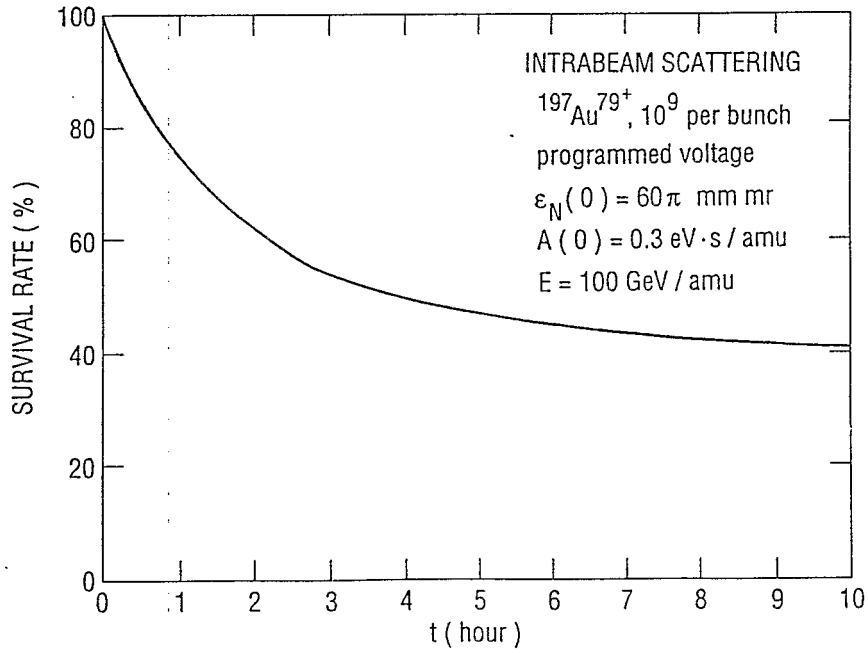


Figure 9: The beam survival rate during the tight-bucket operation.

longitudinal directions. According to G.Parzen's calculation,¹⁴ the transverse emittance increases to about 34π mm-mrad in 10 hours.

With a constant voltage of 4.5MV, the beam loss in longitudinal direction is found to be 40%. If a constant voltage of 11.5MV is achievable, the beam loss will be reduced to about 10%.

D. Discussion

The calculation indicates that the most efficient and economical operational scenario consists of using a constant peak rf voltage of 4.5MV during the entire 10-hour period of storage with the transverse emittance initially blown-up to 60π mm-mrad. The total beam loss is about 20%, while the luminosity[†] is reduced by about 40% in 10 hours mainly due to this beam loss. The averaged rms bunch length is about 23cm.

The situation will be significantly improved if measures like stochastic cooling are adopted.

Acknowledgment

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REFERENCES

- 1) A.Piwinski, Proc. CERN Accelerator School on General Accelerator Physics, Gifsur-Yvette, Paris, 1984, p.405.
- 2) M.Martini, CERN PS/84-9 (AA) (1984).
- 3) J. Bjorken and S.Mtingwa, Particle Accelerators **13**, 115 (1983).

[†] In this case, the reduction in the average luminosity is about 15% compared with the calculation without considering the beam loss.

- 4) G.Parzen, Nucl. Instr. Meth. **A256**, 231 (1987).
- 5) Brookhaven National Laboratory, *Conceptual Design of the RHIC*, BNL-52195 (1989).
- 6) R.Cohen, L.Spitzer, and P.McRoutly, Phys. Rev. **80**, 230 (1950).
- 7) S.Gasiorowicz, M.Neuman, and R.Riddell, Phys. Rev. **101**, 922 (1956).
- 8) M.Rosenbluth, W.MacDonald, and D.Judd, Phys. Rev. **107**, 1 (1957).
- 9) A.H. Sørenssen, *Introduction to Intrabeam Scattering*, Conference contribution, p.135.
- 10) M. Rhoades-Brown and J.Claus, AD/AP-16, (1990).
- 11) J.Wei and A.G.Ruggiero, AD/RHIC-71 (1990).
- 12) H. Goldstein, *Classical Mechanics* (Addison-Wesley, New York, 1953).
- 13) I.S. Gradshteyn and I.M. Ryshik, *Table of Integrals, Series, and Products* (Academic, New York, 1965).
- 14) G.Parzen, private communications.