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Optimization Of The Lattice For Intrabeam Scattering For Short Bunches Operation Mode (90 Degree Advance Cell)

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RHIC-PG-7

OPTIMIZATION OF THE LATTICE FOR INTRABEAM SCATTERING FOR SHORT BUNCHES OPERATION MODE (90° PHASE ADVANCE CELL)

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(BNL, November 21, 1983)

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$$\frac{B^{\prime}l_{\alpha}}{B_{q}}L = \sqrt{2}$$
(1)

$$\beta_{max} = (2+\sqrt{2})L$$

$$\beta_{min} = (2-\sqrt{2})L$$
(2)

$$\mathcal{N}_{\max} = (2 + 1/\sqrt{2}) L \Theta \qquad (3)$$
  
$$\mathcal{N}_{\min} = (2 - 1/\sqrt{2}) L \Theta$$

with the average values

$$\overline{\beta} = 2L \qquad (4)$$

$$\overline{\eta} = 2L\Theta \qquad (5)$$

As in RHIC-6, the number of half-cells is  

$$N = 2\pi R_0 / L \qquad (R_0 = 381.2325 m)$$
and the bending angle per helf regular cell  

$$Q = 2\pi / N$$

Develope eq. (5) can be replaced with
$$\overline{\eta} = 2 \frac{L^2}{R_0}$$
(6)

De results, des in RHic-6, ave given in the Table at the end of the paper. In this table we have marked with a star our choice udich corresponds to a luminosity lifetime well in excess of one hour and a Jull cell length

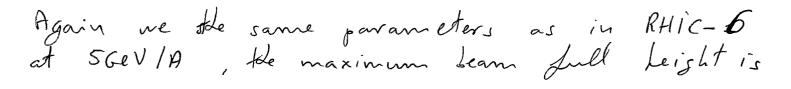
2L = 30 m

For this cell length

= 51 m= 1.6 mBmax 2max

Also

 $N = \frac{160}{9} = 39.27 \text{ mrad}$ 



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$$a_v = 12.8 \text{ mm}$$

and be maximum full width is

 $a_{\mu} = 13.2$  to 16.0 mm

These numbers corresponds to about 5 standard deriations.

We show in a second table the same calcula tion for an initial rms morgy gread  $\overline{\sigma_E/E} = 2 \times 10^{-4}$  as one can see the luminority lifetime is reduced down to  $\frac{1}{3}$  of the previous value and the allowable coyling ingredance is down to =14 of the original value.

Sketch of a Regular Cell (Approximated) Take L = 15 m la = 1.5 m anadrysle Length Bp Jor Gold at 100 GeV/A 800 T-m 2 Ruadrysle Gradient = Bore Radius = 50.3 T/m 4 cm Field at Pole Tip = 2.0 T N = 160 half-cells O = 39.27 mrad, bending angle / half-cell Take B = 3.0T Make 2 dipoles per half a cell Hen 2 lB = 310111 10. 472 m Hat is  $l_{B} = 5.236 m$ Q0/2 , QF/2 B ß 1.264 M 1.264 m 0.5m

0.75m

 $6_{E}/E = 4 \times 10^{-4}$ 

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| 1_     | B        | n     | $\gamma_{E}^{-1}$                     | 25            | tL        | Ϋ́т  | Z/n       |   |
|--------|----------|-------|---------------------------------------|---------------|-----------|------|-----------|---|
|        |          |       |                                       | -)            | <br> <br> |      |           |   |
| m      | m        | m     | h                                     | n.            | hours     |      | ohm       |   |
|        |          |       |                                       |               |           |      |           |   |
| 2.5    | 5        | 0.033 |                                       |               |           | 136  | 0.77      |   |
| <br>5. | 10       | 0.131 |                                       | <u> </u>      | -         | 68   | 2.        |   |
| 7.5    | 15       | 0.295 |                                       |               |           | 45   | 6.6       |   |
| 10.    | 20       | 0.525 | .0036                                 | .0020         | 1.5       | 34   | 13        |   |
| 12.5   | 25       | 0.82  | .0028                                 | .0013 / .0051 | 2./1.0    | 27.3 | 21        |   |
| 15.    | 30       | 1.18  | .0024                                 | .0037         | 1.37      | 22.7 | 31        | * |
| 17.5   | 35       | 1.61  | .0020                                 | .0060         | 1.0       | 19.5 | 42        |   |
| 20.    | 40       | 2.10  | .0017                                 | .0078         | 0.9       | 17.  | 56        |   |
| 22.5   | 45       | 2.66  | .0014                                 | .0092         | 0.8       | 15.  | 73        |   |
| 25.    | 50       | 3.28  | .0011                                 | .0120         | 0,64      | 13.6 | 89        |   |
|        |          |       |                                       |               |           |      |           |   |
|        |          |       |                                       |               |           |      |           |   |
|        |          |       |                                       |               |           |      |           |   |
|        |          |       |                                       |               |           |      |           |   |
|        |          |       |                                       |               |           |      | <br>      |   |
|        |          |       |                                       |               |           |      |           |   |
|        |          |       |                                       |               |           |      |           |   |
|        |          |       |                                       |               |           |      | <br>      |   |
|        |          |       |                                       |               |           |      | <br> <br> |   |
|        |          |       |                                       |               |           |      |           |   |
|        |          |       | · · · · · · · · · · · · · · · · · · · |               |           |      |           |   |
|        |          |       |                                       |               |           |      |           |   |
|        | <u> </u> |       |                                       |               |           |      |           |   |
|        |          |       |                                       |               | <u></u>   | ·    |           |   |

 $\sigma_{E}/E = 2 \times 10^{-4}$ 

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| L    | Ā  | Ī     | $T_{e}^{-1}$ | 2-1           | t_        | γ <sub>T</sub> | Z/n  |       |
|------|----|-------|--------------|---------------|-----------|----------------|------|-------|
| M    | m  |       | 1            | 1<br>h        | hours     |                | ahns |       |
| 2.5  | 5  | .033  | -            |               | -         | 136            | 0.19 | · · · |
| 5    | 10 | 0.131 | -            | +             | -         | 68             | 0.5  |       |
| 7.5  | 15 | 0-295 |              |               | -         | 45             | 1.7  |       |
| 10   | 20 | 0.525 |              | 0.0027        | 0.4       | 34             | 3.2  |       |
| 12.5 | 25 |       |              | 0.0018 1.0074 |           |                | 5.2  |       |
| 15   | 30 | 1.18  |              | 0.0055        | 0.4       | 22.7           | 7.7  | *     |
| 17.5 | 35 | 1.61  |              | 0.00 92       | 0,4       | 19.5           | 10.5 |       |
| 20   | 40 | 2.10  | 0.0107       |               | 0.36      |                | 14   |       |
| 22.5 | 45 | 2.66  | 1            | 0.0154        | 0.34      | 15             | 18.2 |       |
| 25   | 50 | 3.28  | 0.008        | 0.0178/0.0229 | 0.32/0.2/ | 13.6           | 22_2 |       |
|      |    |       |              |               |           |                |      |       |
|      |    |       |              |               |           |                |      |       |
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|      |    |       |              |               |           |                |      |       |
|      |    |       |              |               |           |                |      |       |