

BNL-102270-2014-TECH RHIC/AP/166;BNL-102270-2013-IR

#### KEK MQX Field Error Analysis and Compensation

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December 1998

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#### **U.S. Department of Energy**

USDOE Office of Science (SC)

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# KEK MQX Field Error Analysis & Compensation

J. Wei, V. Ptitsin, N. Gelfand, T. Sen

- \* Introduction
- \* Tracking Results
- \* Compensation Schemes
- \* Discussions

#### \* Introduction

- KEK IR quads (MQXA) have significant systematic error  $b_{10}$
- ullet Aside from  $b_{10}$ , KEK quads have similar errors as FNAL quads

#### Questions:

- \* What is the impact of KEK quad field errors?
- \* What compensation schemes can be used to minimize the impact?
- \* How much corrector strengths are needed and are they achievable?

# LHC IR Parameters at proton collision (7 TeV) (Version 5.1 from CERN SL/AP)

Betatron tunes (H/V)	63.31/59.32
Synchrotron tune	0.00212
Chromaticity (H/V)	2/2
$\beta^*$ , IP1, 5, 2, 8 (H/V) [m]	$0.5/0.5, \ 0.5/0.5, \ 15/10, \ 13/15$
$\Phi/2$ , IP1, 5, 2, 8 (H/V) [ $\mu$ r]	0/150, 150/0, 0/-150, 0/-150
Parallel sept., IP2, 8 [mm]	(H) 0.75, 0.75
Parasitic sept., IP1, 5, 2, 8 $[\sigma_{xy}]$	> 7.3, 7.3, 17, 18
Quad gradient, $ G_0 $ [T/m]	200
Coil i.d., MQX/D1,2 [mm]	70/80
Length, Q1,3/Q2A,B/D1,2 [m]	6.3/5.5/9.45
Max. $\beta$ [m]	4705
rms emittance, $\epsilon_N$ [m·r]	$3.75 \times 10^{-6}$
rms momentum dev., $\sigma_p$	$1.1 \times 10^{-4}$
Max. rms beam size, $\sigma_{xy}$ [mm]	1.5
Max. orbit offset (H/V) [mm]	$\pm 7.3/\pm 7.3$

Reference MQXB (FNAL) errors at collision: (v 2.0;  $R_0 = 17$  mm)

$\overline{n}$		Norma	1		Skew	
	$\langle b_n \rangle$	$d(b_n)$	$\sigma(b_n)$	$\langle a_n \rangle$	$d(a_n)$	$\sigma(a_n)$
Body	[unit]					
3	0.0	0.3	0.8	0.0	0.3	0.8
4	0.0	0.2	0.8	0.0	0.2	0.8
5	0.0	0.2	0.3	0.0	0.2	0.3
6	0.0	0.6	0.6	0.0	0.05	0.1
7	0.0	0.06	0.06	0.0	0.04	0.06
8	0.0	0.05	0.05	0.0	0.03	0.04
9	0.0	0.03	0.03	0.0	0.02	0.02
10	0.0	0.03	0.03	0.0	0.02	0.03
LE	$[\mathrm{unit}\cdot$	m	(Lengt	th=0.4	41 m)	
2	0.0	0.0	0.0	16.4	0.0	0.0
6	0.82	0.82	0.31	0.0	0.21	0.06
10	-0.08	0.08	0.04	0.0	0.04	0.04
RE	$[\mathrm{unit}\cdot$	m	(Leng	th=0.3	33 m)	
6	0.0	0.41	0.31	0.0	0.0	0.0
10	-0.08	0.08	0.04	0.0	0.0	0.0

Reference MQXA (KEK) errors at collision: (v 1.1;  $R_0 = 17$  mm)

$\overline{n}$		Norma	1		Skew	**************************************
	$\langle b_n \rangle$	$d(b_n)$	$\sigma(b_n)$	$\langle a_n \rangle$	$d(a_n)$	$\sigma(a_n)$
Body	[unit]			-		
3	0.0	0.51	1.0	0.0	0.51	1.0
4	0.0	0.29	0.57	0.0	0.29	0.57
5	0.0	0.19	0.38	0.0	0.19	0.38
6	0.0	0.5	0.19	0.0	0.10	0.19
7	0.0	0.05	0.06	0.0	0.05	0.06
8	0.0	0.02	0.03	0.0	0.02	0.03
9	0.0	0.01	0.01	0.0	0.01	0.01
10	-1.0	0.1	0.01	0.0	0.01	0.01
LE	[unit·	m	(Leng	th = 0.4	5 m)	
2	0.0	0.0	0.0	13.4	0.0	0.0
6	2.28	0.0	0.0	0.07	0.0	0.0
10	-0.17	0.0	0.0	-0.02	0.0	0.0
RE	[unit·r	n				
6	0.0	0.0	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0	0.0	0.0

Reference MQXA (KEK) errors at collision: (v 1.0;  $R_0 = 17$  mm)

$\overline{n}$		Norma	,1		Skew	
	$\langle b_n \rangle$	$d(b_n)$	$\sigma(b_n)$	$\langle a_n \rangle$	$d(a_n)$	$\sigma(a_n)$
Body	[unit]		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
3	0.0	0.51	1.0	0.0	0.51	1.0
4	0.0	0.29	0.57	0.0	0.29	0.57
5	0.0	0.19	0.38	0.0	0.19	0.38
6	1.25	0.10	0.19	0.0	0.10	0.19
7	0.0	0.05	0.06	0.0	0.05	0.06
8	0.0	0.02	0.03	0.0	0.02	0.03
9	0.0	0.01	0.01	0.0	0.01	0.01
10	-0.89	0.01	0.01	0.0	0.01	0.01
${ m LE}$	[unit·	m]	(Leng	th=0.4	45 m)	
2	0.0	0.0	0.0	13.4	0.0	0.0
6	2.28	0.0	0.0	0.07	0.0	0.0
10	-0.17	0.0	0.0	-0.02	0.0	0.0
RE	$[ ext{unit} \cdot$	m				
6	0.0	0.0	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0	0.0	0.0

Reference MQXB (FNAL) errors at collision: (v 1.1;  $R_0 = 17$  mm)

$\overline{n}$		Norma	ıl		Skew	
	$\langle b_n \rangle$	$d(b_n)$	$\sigma(b_n)$	$\langle a_n \rangle$	$d(a_n)$	$\sigma(a_n)$
Body	[unit]			<u>,                                      </u>		
3	0.0	0.34	0.85	0.0	0.34	0.85
4	0.0	0.26	0.87	0.0	0.26	0.87
5	0.0	0.20	0.34	0.0	0.20	0.34
6	0.0	0.17	0.25	0.0	0.17	0.25
7	0.0	0.14	0.11	0.0	0.14	0.11
8	0.0	0.10	0.07	0.0	0.10	0.07
9	0.0	0.08	0.07	0.0	0.08	0.07
10	0.0	0.06	0.03	0.0	0.06	0.03
LE	[unit·1	m	(Leng	th = 0.4	1 m)	
2	0.0	0.0	0.0	16.0	0.0	0.0
6	2.3	0.0	0.0	0.07	0.0	0.0
10	-0.09	0.0	0.0	-0.03	0.0	0.0
RE	[unit·r	n]	(Lengt	th = 0.3	3 m)	
6	0.39	0.0	0.0	0.0	0.0	0.0
10	-0.07	0.0	0.0	0.0	0.0	0.0

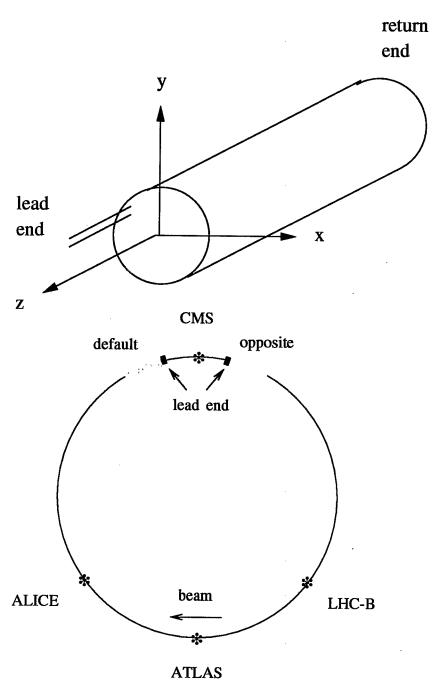
#### **Assumptions:**

- Previous studies: FNAL v1.1 assumed for all four IPs
- "KEK case": KEK's at IP1 & 2; FNAL's at IP5 & 8
- LHC collision lattice version 5.1 with crossing angle
- magnetic error only; no beam-beam, no misalignment

#### Tracking conditions:

- 10 seeds & 100 seeds,  $3\sigma$  cut on random errors; full positive or negative  $d(b_n)$  &  $d(a_n)$
- 5 initial x/y direction
- Refit to the nominal machine operating point  $(Q_x = 63.31, Q_y = 59.32, \xi_x = \xi_y = 2)$
- Comparing with  $10^3$ -turn tracking,  $10^5$ -turn tracking further reduces mean and min. DA by about  $0.5\sigma_{xy}$
- Physical aperture limitation: 60 mm for MQX
- multipole sign reversal according to magnet orientation
- ends separated, treated as lumped kicks
- ullet body divided into 8 pieces for eta variation

# Multipole measurement conventions:



Multipole transformation for "opposite" orientation magnets:

quadrupole:  $b_n => (-)^n$   $b_n$ ;  $a_n => (-)^{n+1}a_n$ 

dipole:  $b_n => (-)^{n+1} b_n; a_n => (-)^n a_n$ 

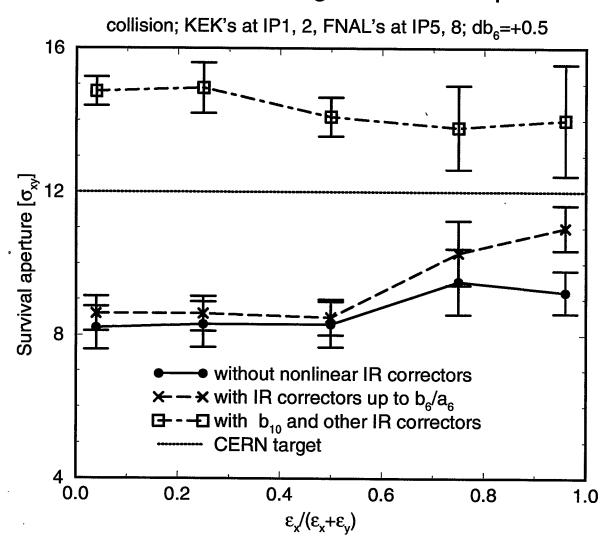
### \* Tracking Results

#### Effects of MQX field errors on dynamic aperture:

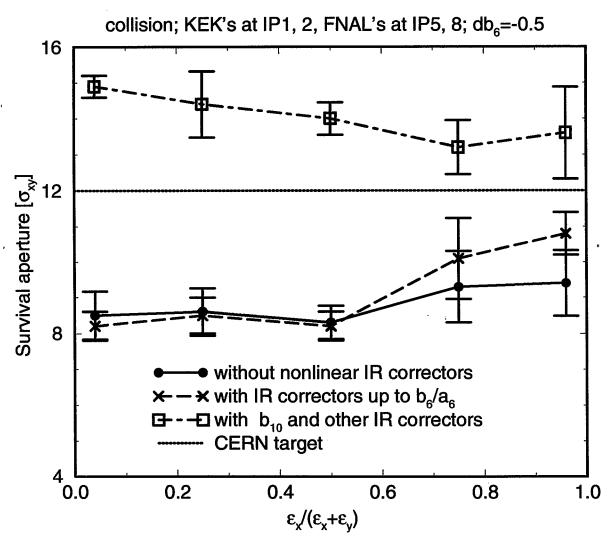
Case	$\begin{array}{c} \mathrm{DA} \; [\sigma_{xy}] \\ \mathrm{(mean \pm SD)} \end{array}$	Min. DA $[\sigma_{xy}]$
FNAL: $(10^3$ -turn)	10.7±1.7	8
KEK: v1.0 v1.0/1.1 without $b_6 \& b_{10}$ v1.1 v1.1 with $b_{10}$ at half strength	$7.9\pm2.4$ $11.4\pm2.2$ $8.7\pm0.9$ $9.4\pm1.7$	5 8 7 7
CERN target: $(10^5$ -turn)	12	10

- KEK (10<sup>5</sup>-turn) v1.1: 8.2 $\pm$ 0.9  $\sigma_{xy}$  6.5 $\sigma_{xy}$
- With either FNAL v1.0 or v2.0, the KEK error impact is the same

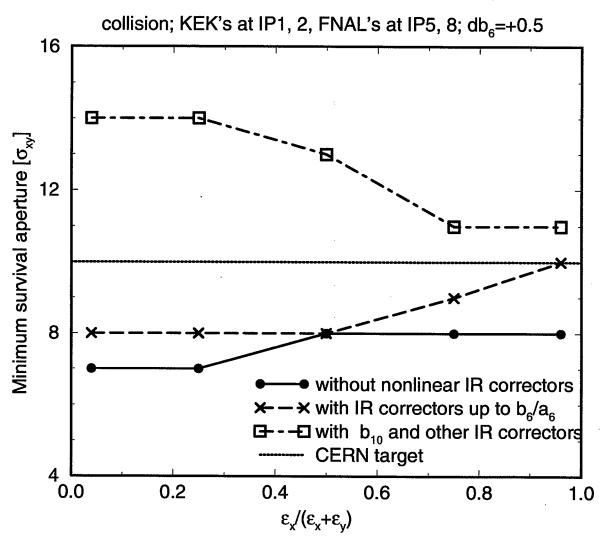
# (Dynamic aperture mean & SD for $b_{6,sys} = 0.5$ )



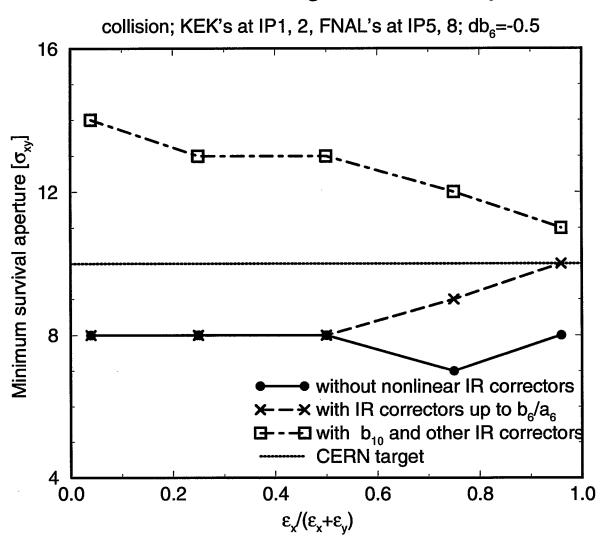
# (Dynamic aperture mean & SD for $b_{6,sys} = -0.5$ )



# (Minimum dynamic aperture for $b_{6,sys} = 0.5$ )



# (Minimum dynamic aperture for $b_{6,sys} = -0.5$ )



### \* Compensation Schemes

Figure of merit for IR local correction:

$$\int_{L} dl \beta_{z}^{n/2} B_{0} b_{n} + (-)^{n} \int_{R} dl \beta_{z}^{n/2} B_{0} b_{n}, \quad z = x, y \quad (1)$$

- to minimize both H and V kicks of the entire IP (two triplets)
- not to take into account the crossing-angle orbit offset
- works for both beams if the lattice is symmetric

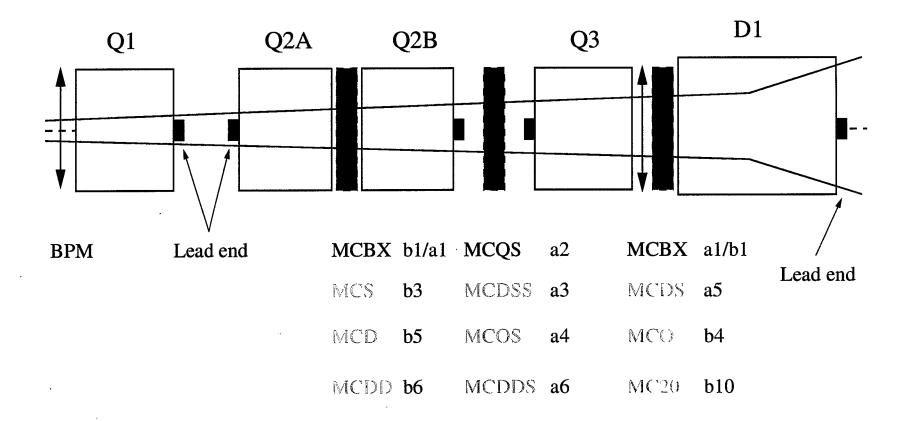
# \* Magnet Orientation Optimization

- cancelling MQX lead-end  $b_6$  among F and D quads
- benefit not significant for  $b_{10}$  due to high eta power dependence

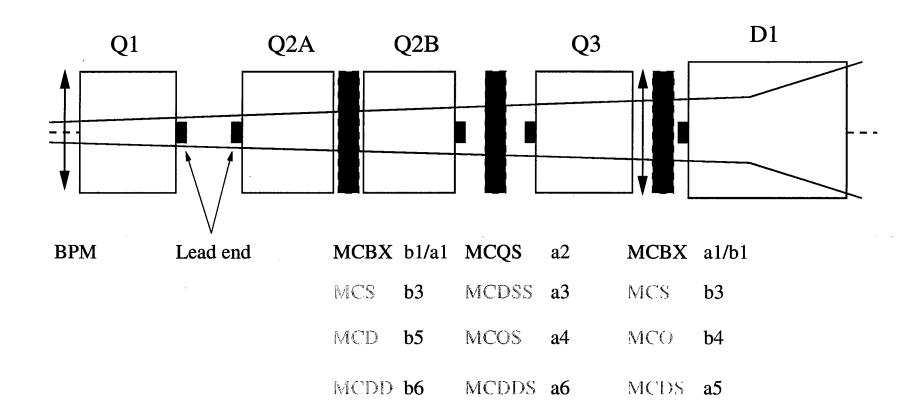
#### \* IR Correctors

- based on bench multipole measurements (assuming 5% rms error)
- limited by space and available strengths

#### towards the IP



#### towards the IP



#### Comparison of IR correction efficiency

### (FNAL v1.1)

Case	$\overline{\mathrm{DA}\left(\sigma_{xy}\right)}$	Min. DA	$\Delta\nu_{max}\ (10^{-3})$	layers
0	$10.7 \pm 1.7$	$8\sigma_{xy}$	1.9±1.1	0
1	$10.7 \pm 1.3$	$9\sigma_{xy}$	$2.1 \pm 1.0$	1
2	$12.5 \pm 1.9$	$9\sigma_{xy}$	$1.9 \pm 1.5$	1
3	$13.3 \pm 1.6$	$10\sigma_{xy}$	$1.0 \pm 0.7$	2
4	$13.6 \pm 1.5$	$11\sigma_{xy}$	$0.5 \pm 0.3$	3
5	$14.1 \pm 1.5$	$11\sigma_{xy}$	$0.5 \pm 0.4$	3

case 0:  $b_1, a_1, a_2$ 

case 1: case 0 plus  $b_3$ ,  $a_3$ ,  $b_4$ 

case 2: case 0 plus  $b_6$ ,  $b_6$ ,  $a_6$ 

case 3: case 0 plus  $b_3$ ,  $b_4$ ,  $b_6$ ,  $a_3$ ,  $a_4$ ,  $a_6$ 

case 4: case 0 plus  $b_3$ ,  $b_4$ ,  $b_5$ ,  $b_6$ ,  $b_6$ ,  $a_3$ ,  $a_4$ ,  $a_5$ ,  $a_6$ 

case 5: case 0 plus  $b_3$ ,  $b_4$ ,  $b_5$ ,  $b_6$ ,  $b_{10}$ ,  $a_3$ ,  $a_4$ ,  $a_5$ ,  $a_6$ 

- nonlinear corrections are activated in IP1 and 5 only.
- assume 10% rms measurement error.
- for zero measurement error, add  $\sim 0.5\sigma_{xy}$
- numbers of layers are for nonlinear multipoles  $(n \ge 3)$

# IR corrector strength used for compensation:

# (FNAL v1.1)

order	Integrated	Field $B_n$ at 17 mm	Field $B_n$ at 17 mm
	$\operatorname{strength}$	$(\text{mean} \pm \text{SD})$	(mean + 6  SD)
	$[\mathrm{unit}{\cdot}\mathrm{m}]$	[T]	[T]
$b_3$	$5.6 \pm 4.5$	$0.0038 \pm 0.0031$	0.022
$a_3$	$13.0 \pm 10.5$	$0.0088 \pm 0.0071$	0.051
$b_4$	$7.0 \pm 4.1$	$0.0048 \pm 0.0028$	0.022
$a_4$	$10.8 \pm 8.3$	$0.0073 \pm 0.0056$	0.041
$b_5$	$2.3 \pm 2.0$	$0.0016 \pm 0.0014$	0.010
$a_5$	$2.4 \pm 2.3$	$0.0016 \pm 0.0016$	0.011
$b_6$	$5.4 \pm 1.9$	$0.0038 \pm 0.0013$	0.012
$a_6$	$3.5 \pm 3.1$	$0.0024 \pm 0.0021$	0.011
$b_{10}$	$0.5 \pm 0.3$	$0.00034 \pm 0.00020$	0.0015

#### Note:

- assume  $L_m = 0.5$  m magnetic length
- bi-polar, individually powered

# from A. Ijspert

Calculation takes account of 4.5 T from MCBX															
Program d:\excell\fields\nedesign:*** Design of a flested magnet At hipporty   100															
	Input parame		6		3		6		3		10	5	4		
Magnet type		n					3900000		88		6.3E+12	66000	2240		
Integrated gradient BI/R^(n-1)	Tm/m^(n-1)		4300000				37	40			37	41	43		
Coil inner radius	mm	R1	37	41.5			39.5				40.5	42.5	44.5		
Coil outer radius	mm	R2	41	43.5			2600				2600	2600	2600		
NoTi crit. current at 5T and 4.2 K	A/mm2	jc	2600				1.9	1.9			1.9	1.9	1.9		
Bath temperature	K	T	1.9	1.9	1.9 1.6	<u> </u>	1.6	1.6			1.6	1.6	1.6		
Copper/Supercond. ratio		r	1.6				0.6		<del> </del>		0.6	0.6	0.6		
Filling fact.(*B/Bpeak evt.)		ff	0.6	0.6			0.6	0.4			0.4	0.4	0.4		
Working point load line		wp	0.4		0.4		25	25	1		25	25	25		
Nominal current	Α	1	25	25	25		25	25		-					
	Output parai	meter	s:		10100		4577.000	1559	1667		1547.306	1674.4	1670.4		
Current density NbTi	A/mm2	j	1464.39				1577.966	0.5692			0.588928	<del>                                     </del>	0.3806		
Field at R1	T	В	0.72929			<u></u>	0.537025	8893.8			4.53E+12		4786.5		
Gradient (B/R^n-1)	T/m^(n-1)	g	1.1E+07				7744371 200				200				
Iron inner radius	mm	R3	200				470				470	<del></del>			
Iron outer radius	mm	R4	470				503.5916				1390.252				
Magnetic length	mm	Lm	408.859				517.3727	494.48			1398.73				
Coll length	mm	Lc	423.164				70.28301	106.05			280.3578				
Magnetic energy	J	W	142.965								0.897145				
Inductance	Н	L	0.45749				0.224906				202.7507	202.62	264.77		
Number of turns/coil		N	367.855				242.9765			-	0.042008				
Wire cross-section (metal)	mm2	Α	0.04439	0.0402	0.0359		0.041192	0.0417	0.039	<u> </u>	0.042000	3.0000		-	

using dipole

for 92

@ 13 mm R.

#### IR corrector strength used for compensation:

(KEK v1.1)

order	Integrated	Field $B_n$ at 17 mm	Field $B_n$ at 17 mm
	$\operatorname{strength}$	$(\text{mean} \pm \text{SD})$	(mean + 6  SD)
	$[\mathrm{unit}{\cdot}\mathrm{m}]$	[T]	[T]
$b_{10}$	$21 \pm 2$	$0.014 \pm 0.001$	0.015

#### Note:

- assume  $L_m = 0.5$  m magnetic length
- bi-polar, individually powered
- for  $n \leq 6$ , the FNAL (mean + 6 SD) value is adequate

#### Is this $b_{10}$ strength achievable?

- According to A. Ijspert, in 3-layer (nonlinear) configuration all except  $b_{10}$  can be made
- ullet The  $b_{10}$  needed for KEK is 28 times achievable value

# Comparison of IR correction efficiency

# (KEK v1.1)

Case	$\mathrm{DA}\left(\sigma_{xy}\right)$	Min. DA	layers
0	$8.7 \pm 0.9$	$7\sigma_{xy}$	0
1	$9.4 \pm 1.2$	$8\sigma_{xy}$	3
2	$14.3 \pm 1.1$	$11\sigma_{xy}$	3

case 0:  $b_1, a_1, a_2$ 

case 1: case 0 plus  $b_3$ ,  $b_3$ ,  $b_4$ ,  $b_5$ ,  $b_6$ ,  $a_3$ ,  $a_4$ ,  $a_5$ ,  $a_6$ 

case 2: case 0 plus  $b_3$ ,  $b_4$ ,  $b_5$ ,  $b_6$ ,  $b_{10}$ ,  $a_3$ ,  $a_4$ ,  $a_5$ ,  $a_6$ 

- nonlinear corrections are activated in IP1 and 5 only.
- assume 5% rms measurement error.
- numbers of layers are for nonlinear multipoles  $(n \ge 3)$

#### \* Discussions

- ullet Comparing with FNAL quads, KEK quad field error further reduces DA by about  $2\sigma_{xy}$
- KEK field error gives DA (mean  $\pm$  SD:  $8.2 \pm 0.9 \ \sigma_{xy}$ ; min.  $6.5\sigma_{xy}$ ) about  $4\sigma_{xy}$  lower than the CERN target (mean  $12\sigma_{xy}$ , min.  $10\sigma_{xy}$ )
- Leading impact is from  $b_{10}$ ; secondly from  $b_6$
- Local corrections using multipoles not higher than  $b_6/a_6$  gives limited improvement ( $\sim 1\sigma_{xy}$ );  $b_{10}$  correctors are needed to meet the target
- Local corrections with  $b_{10}$  can meet the target; needed  $b_{10}$  strength is 0.015 [T] at 17 [mm] (L=0.5 [m]), or integrated gradient  $BL/R^9$  at  $6.3 \times 10^{13}$  [T/m<sup>8</sup>] 28 times achievable value in a 3-layer (nonlinear) configuration
- $\bullet$  Global map/resonance correction may improve situation in the absence of  $b_{10}$  correctors, but the operation is likely to be challenging and less robust in practice