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# Gain-Bandwidth Product of Power Grid Tubes and Application to AGS Power Amplifier Driver

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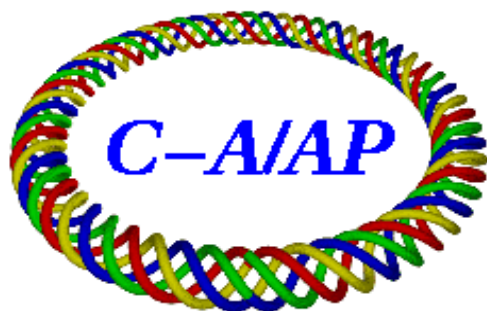
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## **Introduction:**

The driver for the AGS power amplifier is basically a two-stage feedback amplifier. Each stage consists of four Eimac 4CX350AC tubes connected in parallel, for a total of eight tubes. The second or output stage drives a tuned transformer. The first or input stage is a RC coupled amplifier. The loading of the first stage is due to the input capacitance of the second stage plus its own output capacitance. The loading of the preamplifier driver is the input capacitance of the first stage.

The two-stage driver is a wide band rf feedback amplifier. For stability the phase shift of each stage must be limited, requiring a wide bandwidth. To achieve both high gain and wide bandwidth requires that the tubes have a large transconductance ( $g_m$ ) and a small value of capacitance ( $C_{in} + C_{out}$ ). This can be expressed as a figure of merit [1]

defined as  $\frac{1}{2\pi} \frac{g_m}{C_{in} + C_{out}}$ .

## **Figure of Merit:**

The figure of merit is a measure of the gain-bandwidth product of the stage and is expressed in units of frequency, cycles per second, or

herz. The division of the figure of merit between gain and bandwidth is in the value of the load resistance. The above definition is for an amplifier with a two-terminal coupling network. For an amplifier with a four-terminal coupling network the figure of merit is defined as

$$\frac{1}{2\pi} \frac{g_m}{C}. \text{ Where } C \text{ is either } C_{in} \text{ or } C_{out}, \text{ which ever is the larger.}$$

A survey of the figure of merit for tubes varying in anode dissipation from 19 to 300,000 watts is given in Table I. These tubes were in common use at one time or are presently used in the AGS complex.

<b>Tube Type</b>	<b><math>g_m</math> (<math>\mu</math> mho)</b>	<b><math>C_{in}</math> (<math>\mu</math> <math>\mu</math> F)</b>	<b><math>C_{out}</math> (<math>\mu</math> <math>\mu</math> F)</b>	<b>Figure of Merit (Mhz)</b>
6L6 (19 Watts)	5,700	10	12	41
807 (25 Watts)	6,000	11	7	53
814 (50 Watts)	4,000	13.5	13.5	24
4W300B	12,000	15.7	4.5	95
4CX350AC	24,000	23.6	5.6	131
4CX1500B	30,000	85	12.8	47
4CW2000A	37,000	81.5	11.8	63
4CW150,000E	250,000	370	60	93
4CM300,000G	600,000	800	84	108

Table I  
Figure of Merit of Beam Power Tetrodes  
Two Terminal Coupling

Discussion:

Examination of Table I reveals that the 4CX350AC has the highest value of gain-bandwidth product of any available tube. Replacement of the 4CX350AC in the driver by any other tube type would require the employment of a larger number of tubes and or a more complex circuit arrangement.

Paralleling of identical tubes does not affect the gain-bandwidth product of the composite. Nor does it affect the phase characteristics of the composite. A parallel arrangement of identical tubes is characterized by a single (first order) dominant pole with an asymptotic roll-off of 6 db/octave and a maximum phase shift of  $90^\circ$ .

A series arrangement of N identical tubes has a reduced bandwidth as compared to a single tube. It is characterized by an  $N^{\text{th}}$  order dominant pole with an asymptotic roll-off of 6N db/octave and a limiting phase shift of 90N-degrees. A string of three or more identical stages should not be employed in a feedback amplifier due to its excessive phase shift; greater than  $180^\circ$ .

A series arrangement of three or more stages can be employed provided that one stage has a bandwidth significantly smaller than the other stages. The full gain-bandwidth product of the remaining stages is not utilized, reverting to the reduced gain-bandwidth product of the modified stage.

#### References:

- [1] Terman F.E., Radio Engineer's Handbook; 1943; Page 433.