

Stabilization of the Plate Current in Vacuum Tube Power Amplifier Using Cathode Resistor

S. Zheng

October 2003

Collider Accelerator Department
Brookhaven National Laboratory

U.S. Department of Energy

USDOE Office of Science (SC)

Notice: This technical note has been authored by employees of Brookhaven Science Associates, LLC under Contract No. DE-AC02-98CH10886 with the U.S. Department of Energy. The publisher by accepting the technical note for publication acknowledges that the United States Government retains a non-exclusive, paid-up, irrevocable, world-wide license to publish or reproduce the published form of this technical note, or allow others to do so, for United States Government purposes.

DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or any third party's use or the results of such use of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof or its contractors or subcontractors. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

C-A/AP/#116
October 2003

**Stabilization of the Plate Current in Vacuum Tube Power
Amplifier Using Cathode Resistor**

S. Zheng, J. Keane, M. Meth, R. Spitz, A. Zaltsman



**Collider-Accelerator Department
Brookhaven National Laboratory
Upton, NY 11973**

Stabilization of the Plate Current in Vacuum Tube Power Amplifier Using Cathode Resistor

Sanbao Zheng, John Keane, Marvin Meth, Richard Spitz, and Alexander Zaltsman

I Introduction

Vacuum tube power amplifier (PA) is a major RF device extensively used in the BNL Collider/Accelerator facilities. Normally the PA operates within a feedback loop to control the cavity gap voltage. In some abnormal situations such as a detuned cavity, the gap voltage is low, and the closed-loop increases the gap voltage by driving the PA harder without considering the increase of plate current. In these cases, the plate current can run away to a dangerous value. Damage to the PA is possible since there is a time delay before the protection device shuts down the PA.

A possible solution to this problem is to introduce another feedback signal derived from the plate current to the closed-loop. This solution, however, is difficult to implement since it requires changing of the system configuration. The plate current is controlled not only by the driving power, but also by the conduction angle of the tube. Thus, for either class C, class B, or class AB operation, another solution is to increase the magnitude of the control grid bias as the current increases. A cathode resistor R_c (see Fig. 1) is used to realize this method. In this configuration, the cathode resistor essentially forms a negative feedback loop. When the plate current increases, the voltage across R_c increases and the control grid bias becomes more negative, thus the conduction angle becomes smaller and plate current is restrained. The calculations and experimental results for this cathode resistor solution are presented in this note.

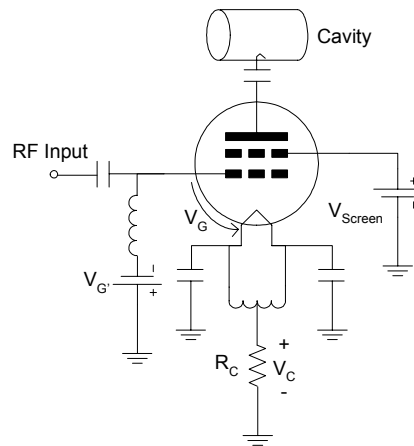


Fig. 1 Circuit configuration.

II Approximated calculations

The driving powers at different plate currents for the 4CW150000 tetrode tube with a 10Ω cathode resistor are calculated by an approximate method. Since the control grid bias is a function of the plate current, several iterations may be necessary during the calculation.

Assuming the screen voltage is 1500 volts, initial control grid bias is -400 volts, and the plate voltage is 14 kV, from the characteristic curve of the 4CW150000 the quiescent plate current is about 0.6 A. The characteristic curve also shows a cut-off control grid voltage of about -450 volts.

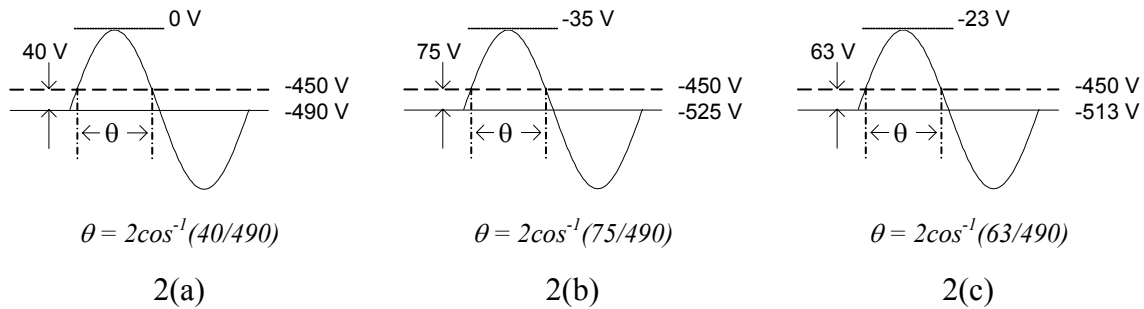


Fig. 2 The grid voltage waveforms used for plate current calculations.

As an initial calculation, assume the plate current I_{dc} to be 9 A, and thus the actual bias V_G is $V_G - V_C = -490$ volts. Also assume an input voltage V_g with a magnitude of 490 volts, thus the maximum grid voltage is $V_g + V_G = 0$. From the characteristic curve, the peak plate current I_m is 53 A. Under these assumptions, the grid voltage is shown in Fig. 2(a), where θ is the conduction angle of the tube. The value of θ can be calculated from the quantities given in the figure. Once this angle is known, a plot given in Page 447, reference [1] can be used to find the ratio of the dc plate current to the peak plate current $\beta = I_{dc}/I_m$. In the plot there is a parameter α , which is usually close to 3/2 for tubes with uniform plane electrodes. For the tube used in this note, $\alpha=2$ was found to be a reasonable value [2].

From Fig. 2(a), the conduction angle is found to be 170.6° . β is found to be 0.235 from the plot given in [1]. Therefore, $I_{dc} = \beta I_m = 12.5$ A, which is bigger than the initial assumption.

For the next iteration, assume $I_{dc} = 12.5$ A (the result from the first calculation). Repeat the above calculations. The resulted control grid voltage is shown in Fig. 2(b), and I_{dc} is found to be 10.1 A.

Interpolating I_{dc} by averaging the above two results one obtains a new plate current of 11.3 A. As a check, the calculation given in iteration 1 is performed again. It turns out that the result from this calculation agrees with the interpolated one.

The results of the calculation are given in table 1. So far only one point of the operation is calculated. Continuing this calculation with different values of V_G , the results for other points are also obtained. Assuming a grid load of 200Ω , the grid voltages are converted to driving power, and the final results are summarized in table 2.

Table 1. Summarization of the calculations with a grid swing of 490 Volts.

Iteration #	Assumed I_p (A)	I_m (A)	θ ($^\circ$)	β	I_{dc} (A)
1	9	53	170.6	0.235	12.5
2	12.5	45	162.4	0.225	10.1
3	11.3	50	164.7	0.226	11.3

Table 2. Calculated plate currents at different driving powers.

Drive power (W)	12.3	42.3	90.3	156.3	240.3	342.3	462.3	600.3
Plate current (A)	0.94	1.8	2.8	3.9	5.7	6.9	9.5	11.3

Using the results given in table 2, the operating characteristic given by the driving power vs. plate current is plotted in Fig. 3.

III Experimental results

Cathode resistors at different values are experimented in the RHIC 28 MHz PA, with a dummy load. The dummy load, which is comprised of a transmission line and a pure resistor, provide a load resistance of about 900Ω at resonance. The experimental results are shown in Fig. 4 to Fig. 5. Fig. 4 gives the comparisons between the results with a 10Ω cathode resistor and with no cathode resistor. As expected, the driving power needed is much higher when the cathode resistor is added to the PA, especially when the plate current is high. Fig. 5 gives a comparison of the results with different cathode resistors. It is evident that the driving power increases with the increase of the cathode resistance value. The efficiency of the PA also increases with the cathode resistance. This is because the PA operates closer to class C with the increase of the cathode resistance.

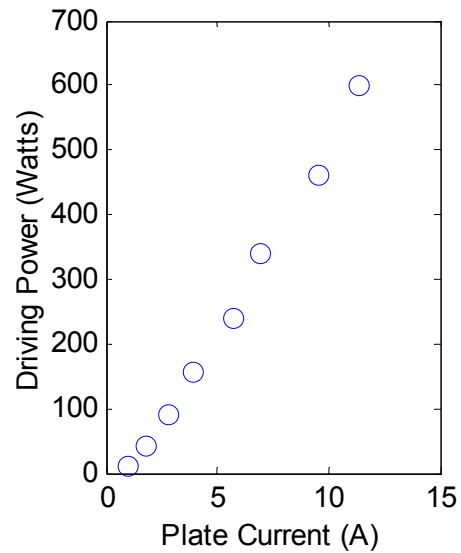


Fig. 3 Calculation result.

IV Summary

A cathode resistor can be used in a high power vacuum PA operating in class AB, B, or C to restrain the plate current from running away. The higher the cathode resistance, the better the current restraining effect. Calculations and experimental results are presented in this note. Experimental results show that, for different values of the cathode resistor, the output power of the PA is essentially the same for the same plate current.

Compromise needs to be made while choosing the cathode resistance since it changes the normal operation of the PA in two aspects: 1) Higher driving power is necessary for the same output; 2) The PA goes to class C operation and bigger harmonics may be produced.

V References

- [1] F. D. Terman, "Radio engineer's handbook," First edition, McGraw-hill book Company, 1943.
- [2] S. Zheng and J. Keane, "Modeling and Simulation of the Power Amplifier for the RHIC 28 MHz Accelerating Cavity," BNL note C-A/AP/97, 05/03.

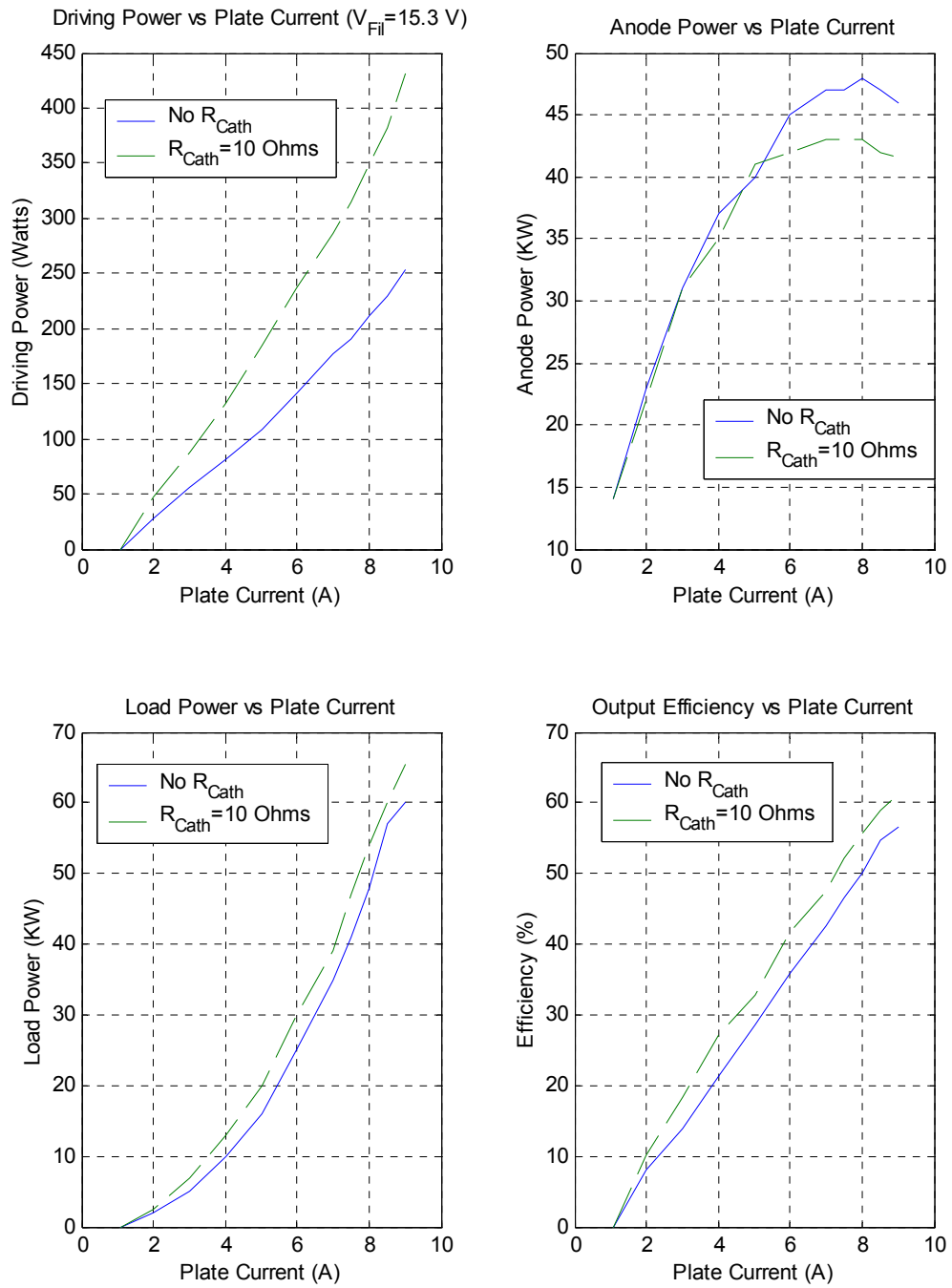


Fig.4 The experimental results of the PA with and without the cathode resistor.

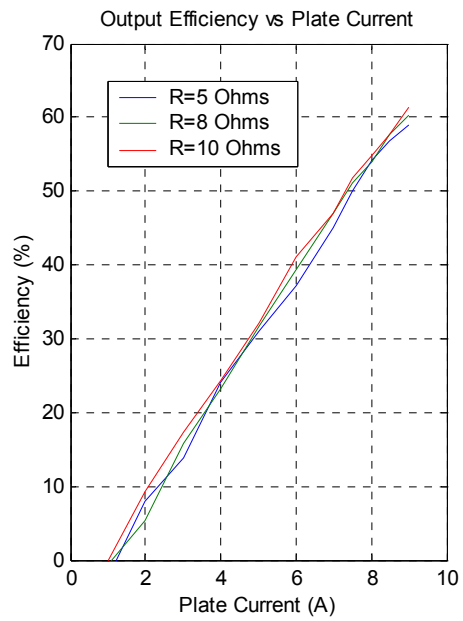
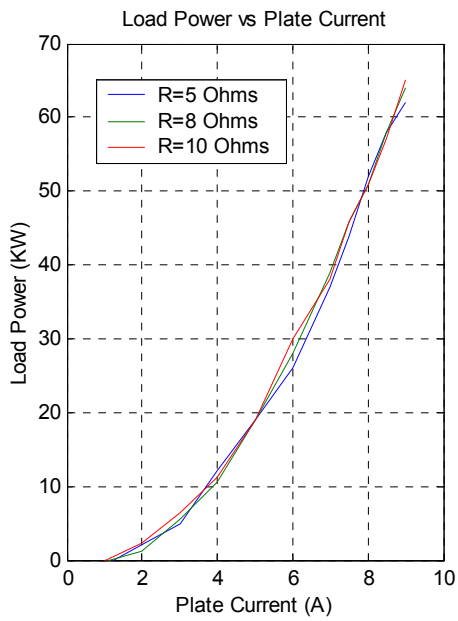
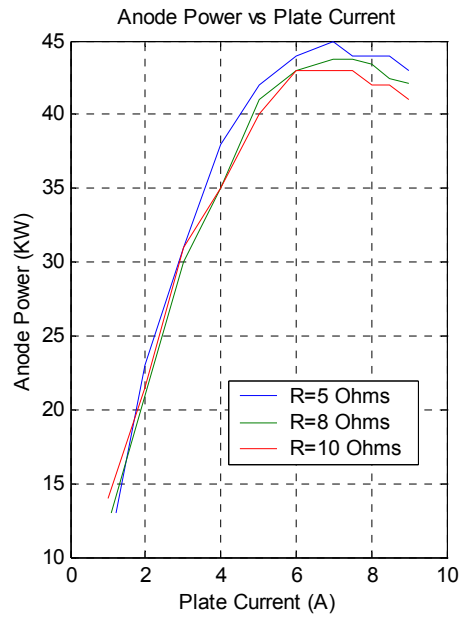
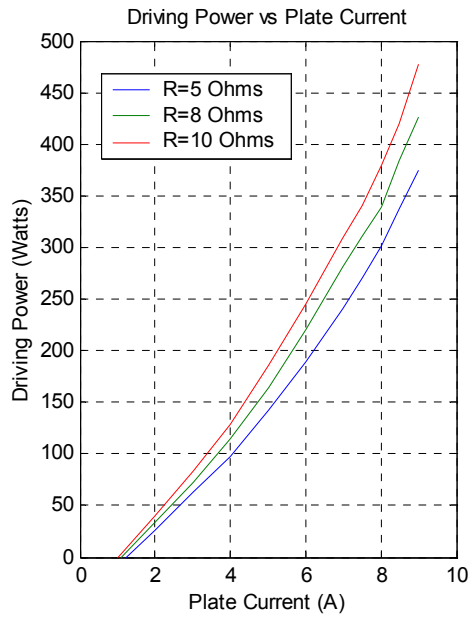


Fig.5 The experimental results of the PA with different cathode resistors.