

# The Start-to-End Simulation of Electron Beam in the RHIC E-cooling Facility (L-band option) with PARMELA

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## **Abstract**

The electron cooling facility has been proposed as a way to reduced the ion beam emittance and energy spread for the RHIC (Relativistic Heavy Ion Collider) to significantly enhance the luminosity. In a high energy electron cooling facilities like the one for RHIC, since the very higher beam quality is needed for the sufficient cooling rate, the traditional way to produce, accelerate and focus beam are hardly applicable. The new solutions include photo-injector for producing the high charge electron bunch with very low emittance, superconducting linac cavities for high current operations, strong cooler solenoid and beam transport to achieve specific beam parameters and make energy-recovery, etc. A start-to-end simulation has been performed with L-band (1.3GHz) gun and linac (TESLA cavity) to demonstrate the feasibility of such an unprecedented cooling facility from the beam production and transport point of view. The main results are, totally revised gun performance considering the crucial heating and RF power issues; workable scheme for merging high/low energy beam into linac with small bending angle dipole, septum magnet and rotation cavity; magnetized beam simulations, beam stretching and compressing, etc. It shows first time that such a design, with high charge beam, magnetized cathode, L-band super-conducting cavities and long transport lines, is feasible from the single bunch particle tracking point of view. The next step is to include real cooler solenoid sections (under design in the Magnet Division). The coherent synchrotron radiation effects is investigated in a separate study.

## Introduction

The RHIC(Relativistic Heavy Ion Collider) is a double ring hadron collider that can provide head-on collisions at energies up to 100GeV/u per beam for very heavy ions, normally gold(  $^{197}\text{Au}^{79+}$ ) and 250GeV/u per beam for protons. Luminosity requirements for the heaviest ions are in  $10^{26} \sim 10^{27} \text{ cm}^{-2}\text{s}^{-1}$  range. By now ( year 2002) the achieved luminosity with Au-Au collisions at 100 GeV/u per beam is  $5 \times 10^{26} \text{ cm}^{-2} \text{ s}^{-1}$ . In near future the RHIC luminosity can be possibly enhanced by another factor of 3~6 with lower beta functions at IP and more bunches. The further physics goals require a higher luminosity. The limiting factor is then the large beam sizes initially determined by the injector machine and later by the Intra-Beam Scattering (IBS) effect. In order to reach that luminosity the beam sizes must be reduced by the beam cooling technique. On the other hand the concept of Electron-Ion Collider (EIC), a proposed machine complex that could provide electron-ion collision, needs even smaller beam dimensions.

Table 1, Nominal Beam Parameters for RHIC E-cooling (Ion beam)  
(05/2002)

Energy	100	GeV/nucleon
No of bunches	120	
Bunch repetition rate	9.4	MHz
Particles per bunch	$10^9$	
Revolution frequency	78.2	kHz
Tunes	28.2/29.2	
Normalized emittance (95%) (start)	15	pi.mm.mrad
Bunch length	30	cm
Solenoid length	30	meter
Solenoid field	1.0	Tesla
Beta-function at cooler	60	meter
Solenoid error level	$8 \times 10^{-6}$	

Electron cooling has been proved to be a very effective way to reduce the beam dimensions both transversely and longitudinally in the low energy accelerators with kinetic energy less than 1 GeV/nuclon (corresponding to 500 KeV electron beam). In those traditional electron cooling schemes the solenoid fields accompany the electron beam from the cathode to the beam dump. While the solenoid provides the tight focusing to confine the beam the angular momentum of the beam is also kept low since the beam has never had a chance to experience the end fields of solenoid or like.

Due to the fact that the cooling rate is inversely proportional the fifth power of ion beam energy the RHIC electron cooling needs to push all the parameters to their limits to obtain the reasonable cooling time for the luminosity upgrades. Table 2 shows the parameters of electron beam according to a recent study of electron cooling simulations.[2]

Table 2, Beam Parameters of Electron beam required by the Cooling

Energy	55	MeV
Particles per bunch	$3 \times 10^{10}$	
Charge per bunch	10	nc
Ratio of cooler/circumference	0.0078	
Average current	47	mA
Beta function at cooler	$\sim 5$	meter
Transverse temperature	$\sim 330$	eV
Energy spread	$10^{-4}$	
Bunch length	$\sim 30$	cm

Among these beam parameters some are unprecedented, for example,  $\sim 100$  mA(cw) current for a 55 MeV linac. The newly proven Energy Recovery Linac(ERL) technique will be adopted to save the tremendous electric power. Still for the electron source, i.e., RF gun, which can not utilize the ER technique, is having the thermal problems due to the very high RF power therefore its peak field at cathode is limited. Consequently the beam performance in the gun is greatly deterred. From single bunch point of view, the low emittance and very small energy spread are also difficult for such a high bunch charge. On the other hand, the multi-bunch effects including Higher-Order-Modes (HOM), Beam-Break-Up(BBU) and other issues for the linac are also very tough and need through and separate investigations. Another uncertain issue is so-called magnetization of the beam. For high energy electron cooling facilities (hadron beam energy is above 10 GeV, corresponding electron beam energy is above 5 MeV), it is very difficult to employ a continuous solenoid field as the electron beam acceleration (especially superconducting radio frequency cavities) and the necessary long beam decompression/compression transport line can hardly be surrounded by the solenoids. The main point of transport of electron beam from the cathode to the cooler solenoid with discrete optical elements is the effect of end field of the solenoid. An analytical study was carried out [2]. Under assumptions: 1, the angular momentum dominated beam, 2, negligible energy spread, 3, linear dynamics only. It concluded that, 1, beam must be magnetized at the cathode, 2, angular momentum can be maintained through the beam line with proper matching with optical elements then eliminated while enter the cooler solenoid. Since the field strength of cooler solenoid required by the RHIC electron cooling is very strong, a rigorous simulation is vital, especially in the sense of addressing the issues the existing theory does not cover.

## 1, General layout

The electron beam facility consists of following major components:

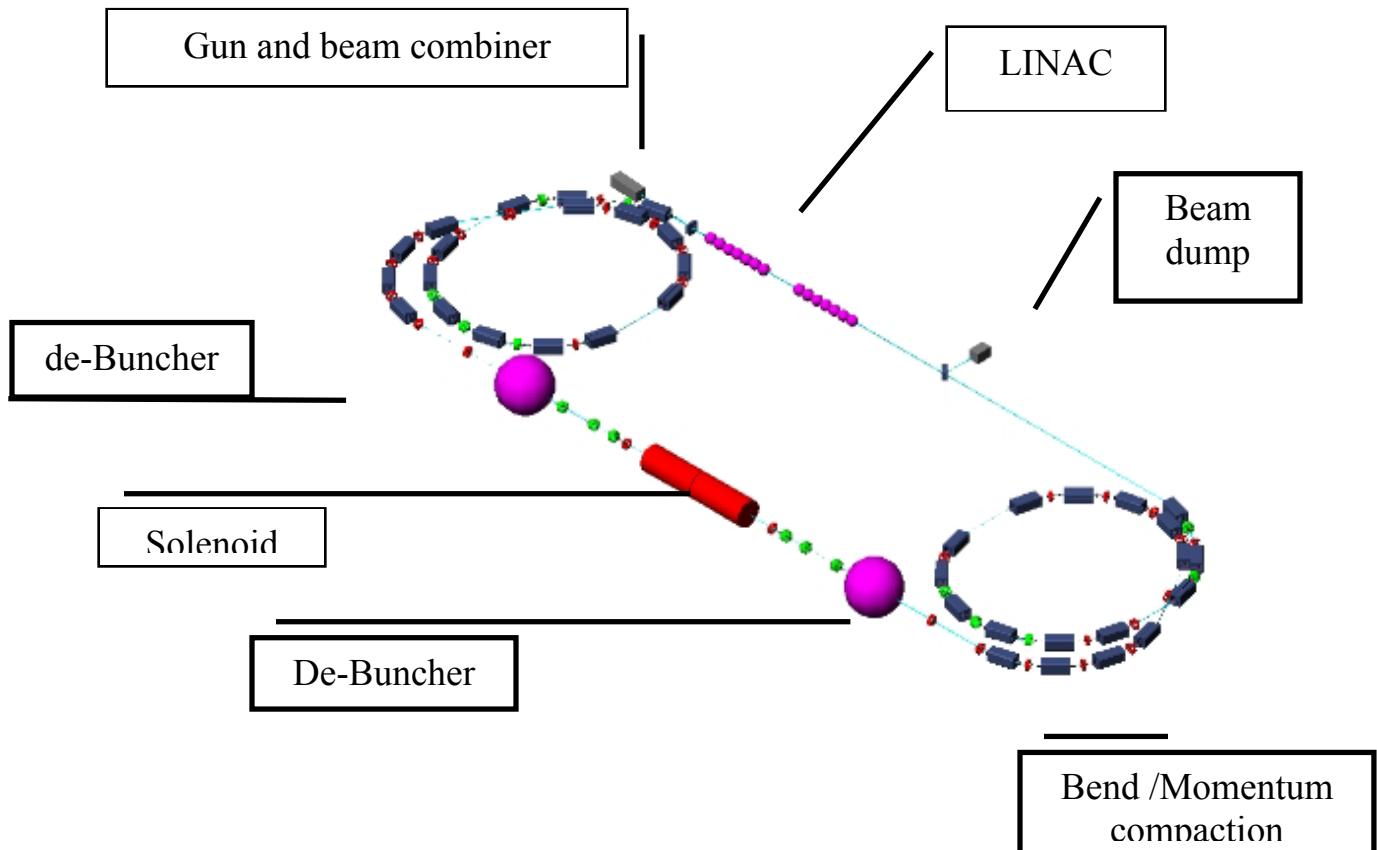
- 1, photo-cathode RF gun and a bunching cavity
- 2, beam merging system
- 3, superconducting linac including focusing coils
- 4, transport line 1: beam stretcher including rotation cavity

5, cooler solenoid(under design)

6, transport line 2: beam compressor including rotation cavity

7, beam dump

Plot 1 shows a schematic layout of RHIC electron cooling facility. The design is still far from a frozen version.



Plot 1, Sketch of electron beam facility for e-cooling

## 2, L-band(1.3 GHz) RF Gun (photo-injector)

In a linear accelerator the electron source plays a crucial role in determining the quality of the beam. For RHIC electron cooling facility the RF photo-injector has been chosen since it is well suitable for producing the low emittance(a few tens mm mrad), short(about 10ps) and intense(10nc/bunch) electron beam.

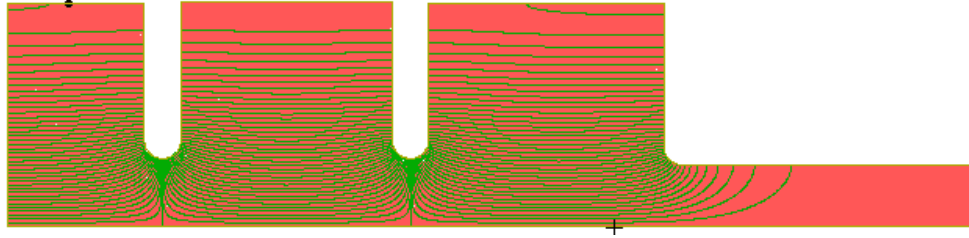
### 1, Choice of frequency

At the time this study was performed, the 1.3 GHz frequency was assumed for the gun mainly because the 1.3 GHz TESLA 9-cell cavity was chosen as the acceleration cavity for the linac. The same frequency will simplify the system designs and operations.

## 2, Geometry of the gun

A 2.5 cell structure is adopted to obtain enough energy at the exit of the gun. Plot 1 shows the gun shape and the electric field calculated by SUPERFISH.

The radius of cavity is 9.1 cm. The iris radius is 2.75 cm. The total length of gun is about 39 cm. The field shown in the plot is the TE01 mode which has its highest field on the cathode. The field flatness among cells is better than 1 percent.



Plot 2, Geometry and Field Distribution of 1.3GHz RF Gun

## 3, Determine the peak electric field in the RF gun

The electric field in the RF gun will dictate the electron beam performance. It is one of the most important parameters in the design of RF guns. The space charge effect in an intense electron bunch can cause fast blow-up in both transverse and longitudinal dimensions. When laser incidents on the photo-cathode, the photo-electrons are produced promptly. As electrons escape from the cathode surface with quite low energies the space charge effect is particularly dangerous. The one of the main cues for this is to accelerate electrons to the high energy as quickly as possible. Therefore a high electric field gradient on the cathode is absolutely favorable.

In a previous study[3] of RF photo-injector the field gradient was set to 25 MV/m and a transverse emittance of about 10 mm mrad was achieved for 5nc bunch charge. Later on more detailed calculations in the gun thermal issues showed that the power dissipated with 25 MV/m field gradient on the cathode might be too high. Table 3 gives the results from SUPERFISH simulations.

**Table 3, Major issue for a cw gun: high dissipated power**

Field (MV/m)	15	20	25
Diss. power (kw)	773	1373	2140
Ave. power den. (w/cm <sup>2</sup> )	293	520	810
Max. power den. (w/cm <sup>2</sup> )	359	638	937

\* 120°C operating temperature.

The preliminary thermal studies showed that the average power density should better be lower than 300 w/cm<sup>2</sup>. So the field gradient at the cathode is chosen to be 15 MV/m. As a matter of fact, this change results in great degeneration of beam performance.



Table 4, main parameters in optimization of gun performance

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Frequency: 1.3GHz
Number of cells: 2 ½ cell
Cathode radius: ~ 0.9 cm
Laser pulse length: ~ 10 ps
Initial RF phase: ~ 15 degree
Magnetic field at cathode: 0~100 Gs
Gradient at cathode: 15 MV/m
Energy at exit: ~ 2.35 MeV
External field: 3 solenoid coils

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#### 4, Solenoid coils for transverse focusing and beam magnetization

The function of solenoid coils around the gun is mainly to keep electron bunch tightly when its energy is still very low since otherwise the space charge force in an intense beam( a few nc charge/bunch with about 10 ps length) totally destroy the electron beam before it is accelerated to high energy.

In case of RHIC electron cooler the solenoid coils have another purpose: to produce adequate magnetization for the electron beam. The detailed studies are reported in a separated paper[5]. Plot 3 shows the layout and field distribution of solenoid coils around the gun.

#### 5, Results in RF gun simulations

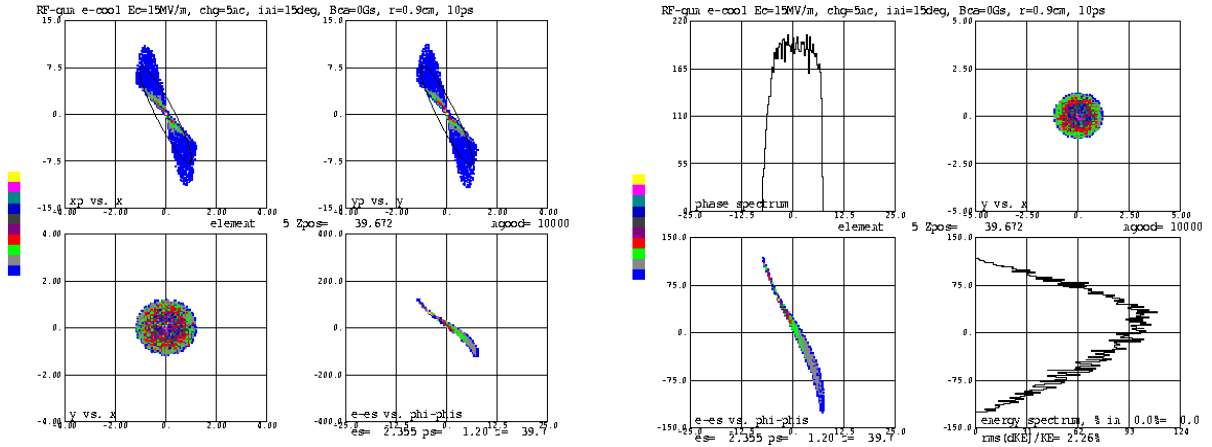
The simulations show that the overall gun performance depends on many parameters. One can hardly give the simple rule or correlations about those dependences. Basically, for a gun with high charge and low field gradient at cathode one has to enlarge the laser spot size even though it will cause increase in initial beam emittance.

Table 5, Performance of 1.3G Hz RF gun with zero magnetic field at cathode

Major parameters	Unit	Exit of RF-gun	Entrance of linac
Beam energy	MeV	2.35	2.35
Trans. emittance	mm.mrad	35	15
Long. emittance	KeV.deg	32.3	72.1
Energy spread	%	2.2	4.3

Table 5 shows the parameters primarily optimized for the transverse emittance. Basically 15 pi mm.mrad is the lowest value one can get with the current setup. In the case of magnetized beam as the contribution of magnetization on the transverse emittance becomes dominate. When beam merging scheme is included into simulation the trade-

off between transverse and longitudinal emittance is made to minimize the effect of the bending magnet on the beam quality.



Plot 3, left: transverse phase space at gun exit, right, longitudinal phase space at gun exit.

Plot 3 shows the transverse and the longitudinal phase spaces of the beam at the gun exit.

## 2, Magnetizing beam at cathode

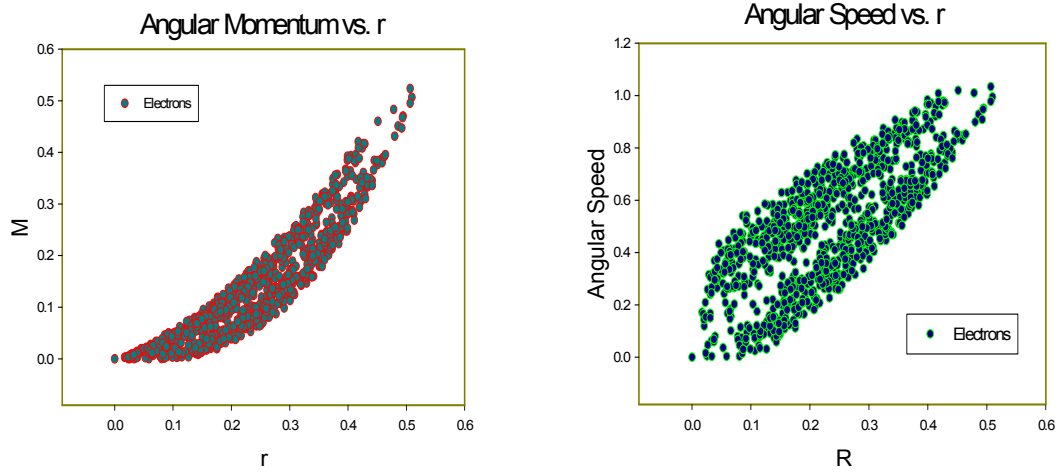
For a high energy electron cooling facility like e-cooler at the RHIC, it is very difficult to employ a continuous solenoid field as the electron beam acceleration (especially superconducting RF cavities) and the necessary long beam decompression/compression transport line can hardly be surrounded by the solenoids. The main point of transport of electron beam from the cathode to the cooler solenoid with discrete optical elements is the effect of end field of the solenoid. An analytical study was carried out [3]. Under assumptions: 1, the angular momentum dominated beam, 2, negligible energy spread, 3, linear dynamics only. It concluded that, 1, beam must be magnetized at the cathode, 2, angular momentum can be maintained through the beam line with proper matching with optical elements then eliminated while enter the cooler solenoid. Since the field strength of cooler solenoid required by the RHIC electron cooling is very strong, a rigorous simulation is vital, especially in the sense of addressing the issues the existing theory does not cover.

The detailed studies on the simulations of magnetized beams are summarized in another paper[5]. Here we just give a general description of magnetized beam and its application in L-band case.

If a bunch of electrons without any collective angular momentum pattern (just as most common electron beams) is simply injected into cooler solenoid, electrons will acquire some amount of angular momentum due to the transverse magnetic component in the end fields of the solenoid.

$$M = mr^2\dot{\theta}$$

Consequently the electrons get extra transverse temperatures and the angular momentum will result in modulation in transverse beam sizes in a longitudinal magnetic field. To eliminate or minimize the angular momentum the electron bunch needs to be ‘magnetized’, i.e., to be given certain amount of angular momentum in a specific pattern before it goes through the cooler solenoid.



Plot 4, left, angular momentum of magnetized beam, right, angular speed

Before talking about the global matching of the magnetization of the beam, a direct consequence of a finite longitudinal magnetic field is the increase of the transverse beam emittance. The principle can be described by the Busch's theorem (which is also the simplest case of the matching of the magnetized beam),

$$\dot{\phi} = -\frac{e}{2\pi\gamma m_e r^2(s)}[\Phi(s) - \Phi_{cathode}]$$

Assuming the matched electron and ion beam sizes and 1T cooler solenoid, the required field at cathode is about 100 Gauss for 10 mm radius beam spot size. Therefore the estimated contribution of this field is given by,

$$\mathcal{E}_{mag} = \frac{\Phi}{2\pi B \rho}$$

The effects of this extra emittance on beam transport can only be evaluated via particle tracking. The last section will show the overall beam emittance and envelope along the beam line.

### 3, Low- and High-Energy beam merging system

The principle of an Energy Recovery Linac(ERL) is to re-inject the ‘used’ electron beam into the same linac to give back its energy to the linear accelerator system by setting the RF phase opposite to that when it is accelerated. A beam merging system is needed to adequately guide low- and high-energy beams into the linear accelerator without damaging the beam quality.

Since there is a big difference in energy between two beams, 2~3 MeV vs. 55 MeV, it is then possible that one could use a common bending magnet to bring two beams to the axis of the linac. The natural choice is that with a single dipole the low energy beam is bent by a large angle while the high energy beam is injected with a much smaller angle. But the simulation showed that such a big bending is quite harmful for the low energy beam. More sophisticated schemes such as achromat or other matching sections are also considered and calculated but the side effects of large bending angle dipoles can hardly overcome at this low energy and high bunch charge. Therefore a scheme was proposed that the low energy beam is bent by a minimum angle(1~3 degrees) while the high energy beam is brought into by a septum magnet. See plot 6.

The criterion in design of beam merging system is like following:

$$D = D\text{-low} + D\text{-high} + D\text{-septum} + M$$

D: distance between centers of high- and low-energy beam

D-low: 100% beam size (radius) of the low energy beam

D-high: 100% beam size (radius) of the high energy beam

D-septum: minimum thickness of the septum magnets

M: margin for other considerations, e.g., orbit jitter and so on.

In our case:

Table 6, Beam separation calculations

	Amount	Definition
D-low	5 mm	100% beam size (radius) of the low energy beam
D-high	3 mm	100% beam size (radius) of the high energy beam
D-septum	10 mm	minimum thickness of the septum magnets
M	5+5 mm	margin for other considerations, e.g., orbit jitter and so on.
D	28 mm	distance between centers of high- and low-energy beam

The bending angle of the dipole and the distance between the exit of septum magnet fulfill the following relationship:

$$D = L \times \sin(A) \text{ (when } A \text{ is small, say, a few degrees)}$$

D: distance between centers of high- and low-energy beam, same as above definition

L: distance between the exit and the entrance of dipole

A-dipole: bending angle of the dipole before the linac.

Table 7, Different combinations of distance and bending angles(D=28mm)

L (meter)	0.5	1.0	1.5
A-dipole (degree)	3.3	1.6	1.1

Table 8, Different combinations of distance and bending angles(D=35mm)

L (meter)	0.5	1.0	1.5
A-dipole (degree)	4.0	2.0	0.7

In our design, the modest distance and bending angle, say, 2 degree and 1 meter, are chosen to avoid side effects on the transverse and longitudinal quality of the low energy beam.

The design of the septum magnet is preliminarily estimated by 2-D magnetic calculation code POISSON. It shows that with 10 mm thickness and 4000 Gausses field strength on the high energy beam side (inside septum magnet), the magnetic field leakage on the low energy beam side is negligible.

The length and bending angle of the septum magnet are determined by:

D2: total distance between high- and low energy beams,

$D2 = 100\% \text{ beam size of high energy beam} + \text{orbit margin} + \text{high energy beam pipe}$   
 $+ \text{outer radius of solenoid coil at the end of the gun} - D$

$D2 = L\text{-septum} \times \sin(A)$

Table 9, preliminary estimation of D2

The 100% beam size(radius) of high energy beam	3 mm
Orbit safe margin	10 mm
High energy beam pipe	5 mm
Outer radius of solenoid coil or bunching cavity	~ 90 mm*
D	~ 35 mm
Total	73 mm

\* estimated as the same as the gun cavity inner radius, this is a rough estimation.

Detailed design is yet to be done.

The estimated total length of septum magnet is about 30 cm. The bending angle is about 15~20 degrees. If the outer size of solenoid coil at the end of the gun is larger or smaller than the preliminary estimation the length or the field strength needs adjusting.

There is a bunch cavity just next to the gun exit for optimizing the longitudinal phase space of the beam and it does not provide any acceleration or de-acceleration to the center beam energy. This cavity can be the same frequency as the gun's or with higher frequency to reduce the voltage. On the other hand the optimized energy spread will help to minimize the effect of the dipole. Simulations show that, with above setup, both transverse and longitudinal parameters can fulfill the requirements even without a double dipole achromat.

A booster immediately installed after gun can significantly enhance the beam quality according to our simulation. In fact this is the way adopted in many of electron linac facilities.

### 3, Superconducting Linac

1.3 GHz 9-cell TESLA superconducting cavity has been a great success in recent decades in providing high gradient acceleration for the low and high energy electron linear

accelerators. The choice of 1.3 GHz system is mainly because it is a proven technology and a commercial product. Nevertheless the major applications of the 1.3 GHz 9-cell TESLA cavity have been in pulsed working mode. To work properly in the cw working mode in RHIC e-cooling facility some efforts need to be made to address some high current issues. Some parallel studies have been conducted to investigate the high current and multi-bunch issues[5]. From beam transport point of view, the most relevant issue is single bunch effect, i.e., RF focusing and space charge effect.

In our simulations the field gradient of 9-cell cavity is set to about 13~15 MV/m. Each 9-cell cavity structure is about 1.06 m long. Four cavities can provide up to about 55 MeV total energy gain. One solenoid coil in the middle of the linac is enough for the transverse focusing. Transverse emittance is maintained through the linac as expected. No third harmonic de-acceleration cavity is assumed in L-band simulation as the beam energy spread has already good enough ( $1.5E-3$ ).

#### **4, De-compressor and Compressor**

The purpose of the compressor and decompressor in arcs is following:

- 1, optimize the energy spread before beam enters cooler solenoid to maximize the cooling rate.
- 2, before beam enters the cooler solenoid, adjust(lengthen) the bunch length to partially match the ion bunch length (typically a few tens centimeters) and to mitigate the space charge effect(de-compressor). After the cooler solenoid, adjust(shorten) the bunch length to re-enter the lianc for the energy recovery(compressor).

The lattice design of the arc is done by Jorg Kewisch. The optics of compressor and de-compressor is same. The bunch lengthening parameter  $R_{56}$  of each arc was matched to 100m initially. Later on a more moderate value(30m) was chosen to alleviate problems caused by large dispersions. Each arc is an achromat and has symmetric structure. In each end of arc there are enough quadrupole variables to match the twiss parameters to the linac and the cooler.

#### **5, Cavities for longitudinal phase rotation**

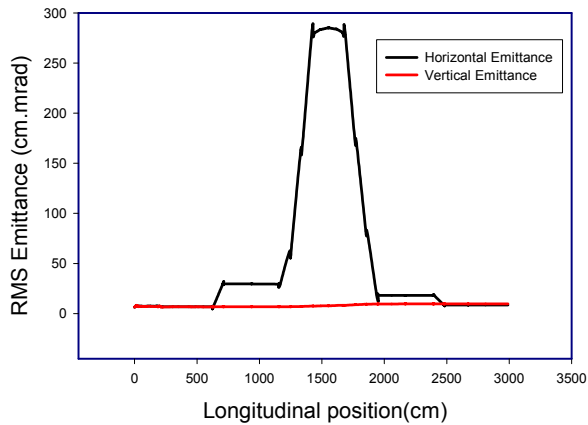
To minimized the energy spread of electron beam a widely used scheme is adopted in our beam line. The electron bunch is first lengthened, i.e., stretched in the longitudinal phase space by the arc, then rotated by a RF field to get a flattened energy spread. Several cavities with different frequencies range from 200 MHz to 1.3 GHz are used in our simulations. The voltage needed to right rotation is inversely proportional to the RF frequency. No significant difference is found in terms of beam performance.

#### **6, Summary: overall simulation results and matching of magnetized beam**

Simulations have shown that,

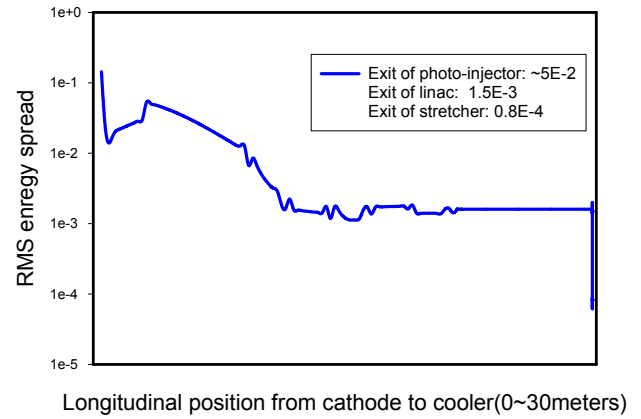


# RHIC e-cool, magnetized beam transport (photo-injector, linac, stretcher) Transverse emittance preservation

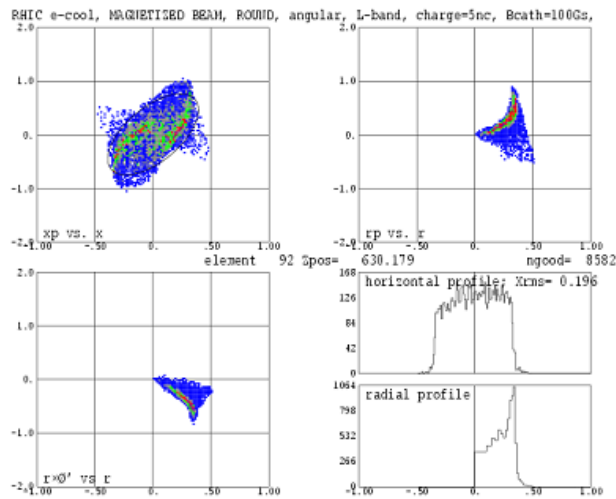


Plot 6, Hori./verti. beam emittances

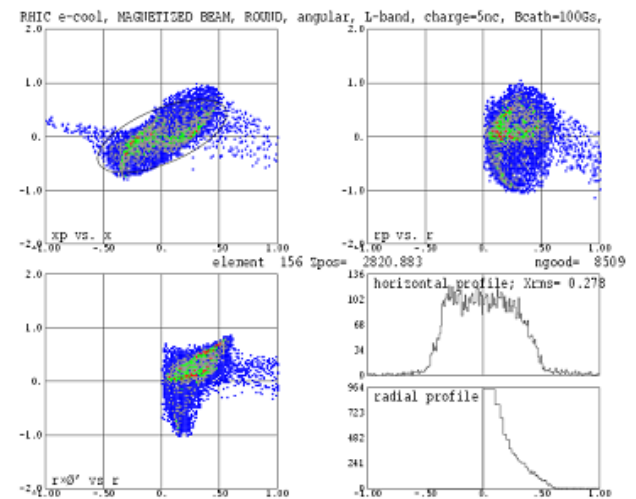
# RHIC e-cool, magnetized beam transport optimization of beam energy spread



Plot 7, energy spread from cathode to cooler



Plot 8, magnetization at linac exit



Plot 9, magnetization at entrance of the cooler



## **7, Higher charge(current) case**

A recent cooling simulation shows that a higher bunch charge, say, 10nc, may be needed to get decent cooling rate. This is big challenge for a L-band gun with limited field gradient at the cathode. One may have to go to lower frequency RF system which allows a bigger spot size and bunch length. However, the short wavelength of L-band system permits us to think about the bunch train scheme, i.e., using a few 5nc electron bunches to cool a 30~150 cm ion bunches. The bunch spacing of L-band can be as close as about 23 cm. For a 30cm ion bunch, one put 2 consecutive 5nc electron bunches at same time. Nevertheless high average current issues can be another limiting factor for L-band system. This needs some dedicated studies[5].

## **8, Acknowledgment**

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