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MESB Design Notes: I. Tolerances on the uniformity of ? Bd in D1 and D2

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EP&S DIVISION TECHNICAL NOTE
No. 59
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MESB Design Notes: I. Tolerances on the Uniformity of $\int Bd\ell$ in D1 and D2.

ABSTRACT- It is found that $\int Bd\ell$ in D1 must be uniform within 0.2% over a 10-inch region up to 6.6 Gev/c (15.4 KG) and within 0.2% over an 8" region from 6.6 to 9.3 Gev/c (21.8 KG), in order to hold aberrations in the y coordinate at the mass slit to a tolerable level. D2 is less critical since there is a nearby sextupole in the beam to use for correction, if an extra power supply can be found for it.

~~MESB Notes~~

~~Aberrations at Mass slit due to D1 + D2~~

Theory

If ~~the~~ $\int B dl$ of a bending magnet ~~has a~~ has a quadratic variation with x (horizontal coordinate):

$$\int B dl = A_0 \left(1 + \frac{\epsilon x^2}{x_0^2}\right) \qquad (1)$$

where ϵ is the fractional change in $\int B dl$ at $x = x_0$, then the fringe focusing in the vertical plane has an x-dependence given by[1]:

$$\frac{1}{f} = \frac{\alpha^2}{L}\left(1 + \frac{2 L \epsilon x}{\alpha x_0^2}\right)$$

where α = bend angle (radians), L = length. We care only about the variation about the central value:

$$\Delta \frac{1}{f} = \alpha \epsilon \frac{2x}{x_0^2} \qquad (2)$$

(For reference, I note that such an aberration can be simulated by a sextupole magnet in various beam programs. In particular, Fox's program ~~Beam~~ BEAM has the sextupole focal length in the form

$$\frac{1}{f} = \frac{G}{1313 P} 2x \qquad \text{(units: kG/inch, inches, GeV/c)}$$

where G is the sextupole "gradient". Since $\alpha = \int B dl / 1313 P$,

(1) M. L. Good, ANL-6611 (1962); C. T. Murphy, U. of Mich. Bubble Chamber Note 42/65 (1965)

where B is the bending ~~m~~ magnet field,

$$G = \frac{\epsilon}{x_0^2} \int B\,dl \qquad (3)$$

~~five~~ gives a relationship between a measured value of ϵ and the input "gradient" value which simulates the effect.)

The variation in f, Eq. (2), induces a variation in $\bar{y}_b' = dy/dz$ at the bending magnet:

$$\Delta \bar{y}_b' = y_b \Delta\left(\frac{1}{f}\right)$$

which may be related to the effective target ~~B~~ broadening, Δy_t by

$$\Delta y_t = b \, \Delta \bar{y}_b' \qquad (4)$$

where b is the "upper right hand corner" element of the transfer matrix, T_{tb}, from the target to the bending magnet:

$$T_{tb} = \begin{pmatrix} a & b \\ c & d \end{pmatrix}$$

Let $\bar{y}_t'$ = angle of a ray at the target. Then $y_b = b\,\bar{y}_t'$. Eq. (4) then ~~then~~ can be written in a number of forms:

$$\boxed{\Delta y_t = b^2 \, \bar{y}_t' \, \Delta\left(\frac{1}{f}\right)} = \frac{y_b^2}{\bar{y}_t'} \Delta\left(\frac{1}{f}\right) = b \, y_b \, \Delta\left(\frac{1}{f}\right) \qquad (5)$$

This may be related to the broadening at the mass slit (the first focus), Δy_m, and the slope at the mass slit, $\bar{y}_m'$, by multiplying by the magnification (and note $\bar{y}_m' = \bar{y}_t' / m_v$):

$$\boxed{\Delta y_m = b^2 m_v^2 \, y_m' \, \frac{\alpha \epsilon \, 2 x_b}{x_0^2}} \qquad (6)$$

Summarizing the notation, Δy_m is the change of position of a ray at the mass slit which has slope y_m' and which passed through the bending magnet at x_b; b is the transfer matrix element defined in Eq. (4); m_v is the magnification, y_t / y_m; α is the bend angle (radians); x_0 is the position in the bending magnet where $\int B dl$ differs by the fraction ϵ from its central value.

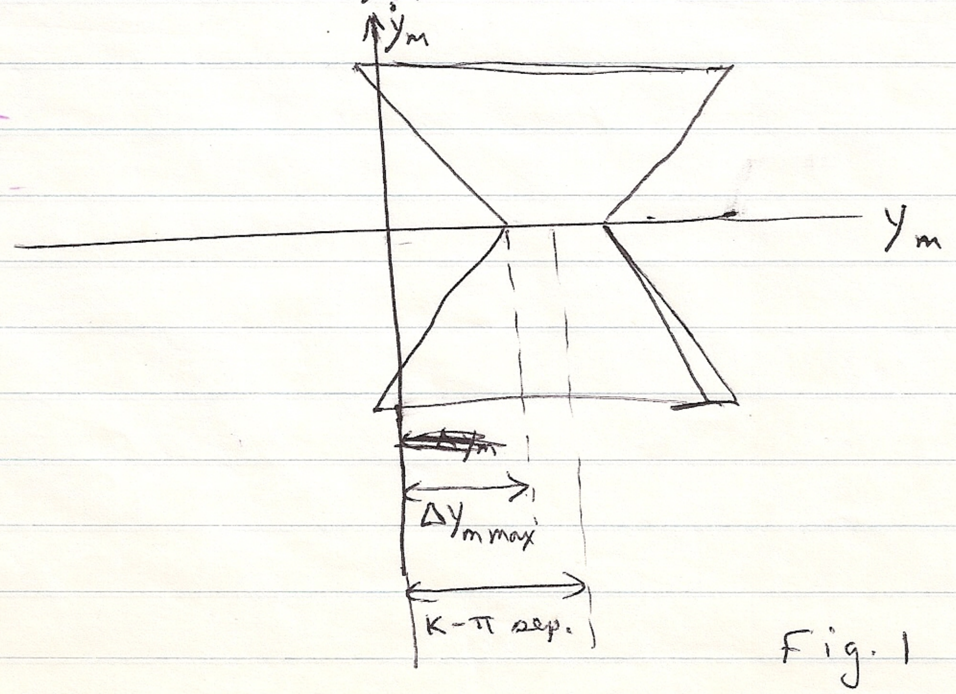
Data and examples

Table I shows input data for Eq. (6) for 5 modes of MESB. The value of $x_{b\,max}$ includes half of the total sagitta (1.4") of the beam in D1 and D2. The bend angle, α, is $8° = 0.14$ rad in all cases. The K–π separation listed for each mode is the separation at the nominal momentum limit of that mode, i.e., the momentum at which the K–π separation is twice the geometrical image width (except mode 4W, where the ratio is 1.5). (These momenta are 4, 6, and 6.6 GeV/c for modes 1, 3, and 4, respectively.) Values of $(\Delta y_m)_{max}$ are listed under the assumption that $\epsilon = 0.2\%$ at $x_0 = 5''$, an apparently arbitrary case. In fact, this case is the maximum tolerable non-uniformity in D1, as will be shown in the next section. The ratio of $(\Delta y_m)_{max}$ to the K-π separation is also listed and is 0.8 for mode 4W ~~1W~~ and slightly less for other modes, ~~Thus mode 1W is the mode most sensitive to~~ considering only D1.

The same ratio is usually considerably smaller for D2. ~~Furthmore~~ Furthermore, D2 has a nearby sextupole magnet which can be used to correct the aberration. Therefore D2 is of no concern, unless it has aberrations ~~which are very large in~~ which are of higher order than sextupole and are very large.

<u>A criterion for maximum allowable non-uniformity in D1</u>

As can be seen from Eq. (6), the non-uniformity of D1 will produce a phase space plot for pions at the mass slit which has the qualitative appearance of Fig. 1 (ignoring all other aberrations).



(this fig. is in the text.)

Fig. 1

~~This shape is reminiscent of that of the chromatic aberration~~

This shape is qualitatively the same as that shown in Fig. 15 of EP+S 72-1, a shape which results from the unremovable chromatic aberrations. The mass slit has been shaped to as to ~~roughly~~ roughly cover this shape (see separate report). Thus a reasonable criterion for the maximum acceptable non-uniformity in D1 seems to be that the aberration be no worse than ~~chrom~~ the chromatic aberration. Comparing ΔY_{max} (line 8, Table I) with ΔY_{max}, chromatic (line 4) we see that the criterion is met for mode 3 and slightly exceeded for modes 1 and 4. To be more exact, I display in Figs. 2 and 3 the actual phase space plots for modes 1E and 4W. Fig. (a) shows the shape derived from the Monte Carlo in BEAM, including chromatic aberration but assumed no aberration from D1. In the Monte Carlo, a 4" target was assumed; the momentum bites were 3% for mode 1 and 1½% for mode 4. The effective shape of the mass slit is shown as a dotted line (assuming that the mass slit is 40" long and has a slope of 0.6 mrad). Fig. (b) shows the phase space derived from Eq. (6) with $\epsilon = 0.2\%$ at $x_0 = 5"$, i.e., resulting from D1 aberrations alone. The mass slit is supposed to intercept any pion to the right of the dotted line. We see that Mode 1E is predicted to have some leak through. However, these hand-calculated phase spaces cannot be taken literally, since chromatic effects and clipping by collimators has been ignored. Hence Monte Carlos were run with a sextupole added at the end of D1, with G given by Eq. (3) ($\epsilon = 0.2\%$, $x_0 = 5''$). The resulting phase space plots (computer print out) are shown in Fig. 4; both chromatic and D1 aberrations are now correctly included. The number of ~~particles~~ π's which leak thru the mass slit is $\approx 1\%$ or less.

Details: Momentum dependence and the ~~sg~~ sagitta question

The criterion that $\epsilon = 0.2\%$ at $\pm 5''$ is dictated by modes 1 and 4. Mode 1 is ~~supposed to work up to 6 GeV ($\bar{p}$'s)~~ to separate $\bar{p}$'s up to 6 GeV/c; Mode 4 is supposed to make a cleaner K beam at 6 GeV/c (with a loss of flux), or perhaps can be used to extend the momentum limit for K^- to 6.6 GeV/c. (15.4 kG).

Above 6.6 GeV/c, neither mode 1 nor mode 4 will be used to separate masses. Mode 3 will be adequate to separate π^+ from p up to the momentum limit of 9.3 GeV/c. If anybody tries to separate $\bar{p}$ from π^- at 9 GeV/c, the loss of flux caused by switching to mode 4 is intollerable.

Thus we can demand that above 6.6 GeV/c, the D1 non-uniformity must satisfy mode 3, which has a looser tolerance (see Table I). For equal chromatic and D1 aberrations, one can allow $\epsilon \leq 0.32\%$ at $x_0 = 5''$; since only $\pm 4''$ are used in mode 3, this criterion is better stated as $\epsilon \leq 0.20\%$ at $x_0 = \pm 4''$.

~~If these criteria cannot be met without the addition of pole face windings~~ The ~~situation~~ phase space plots under this condition for mode 3W are shown in Figs. 5(a) (Monte Carlo, no D1 aberration), ~~and~~ 5(b) (hand calculation of aberrated D1), and 6 (Monte Carlo including chromatic and D1 aberration).

The maximum x-values assumed included and extra 0.7" in all modes, corresponding to the half sagitta of the path of the particle through D1. If a curved $\int B dl$ coil is used, or if a model can be used to calculate $\int B dl$ along curved paths, the tolerances are loosened slightly: at 6.6 GeV/c, $\epsilon \leq .18\%$ at $x = \pm 4.5''$; at 9.3 GeV/c, $\epsilon \leq .18\%$ at $x_0 = \pm 3.5''$.

If these tolerances cannot be achieved without the addition of pole face windings, it would of course be desirable to design the windings to achieve ϵ values about one-half as large as those stated above.

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Table I - Aberrations from non-uniformities in $\int B dl$ for D1 + D2

	Mode				
	1W (MPS)	1E	3W	3E	4W
m_V	2.13	2.41	0.62	0.61	1.00
y'_m max	1.8 mr	1.6	1.9	1.9	1.2
K-π separation	0.17"	0.19"	0.049"	0.049"	0.060"
ΔY_{max}, chromatic	0.09"	0.71	0.040	0.042	0.040
At D1:					
b	340"	325	645	620	645
x_{max} {includes ½ sagitta}	5.3"	5.2	4.2	4.0	4.1
$(\Delta y_m x_0^2/\epsilon)_{max}$	1400 in^3	1440	320	305	540
ΔY_m max *	0.11"	0.12	0.025	0.024	0.044
ΔY_m max / K-π sep.	0.65	0.64	0.51	0.49	0.73
At D2:					
b	200"	163"	520	645	372
x_{max}	4.7"	3.7	3.3	1.8	2.3
$(\Delta y_m x_0^2/\epsilon)_{max}$	1500" in^3	260	175	190	105
ΔY_m max *	0.12"	0.02"	0.014	.008	.0085
ΔY_m max / K-π sep.	0.70	.10	.29	.16	.14

* if $\epsilon = \frac{1}{5}\%$ at $x_0 = .5$"

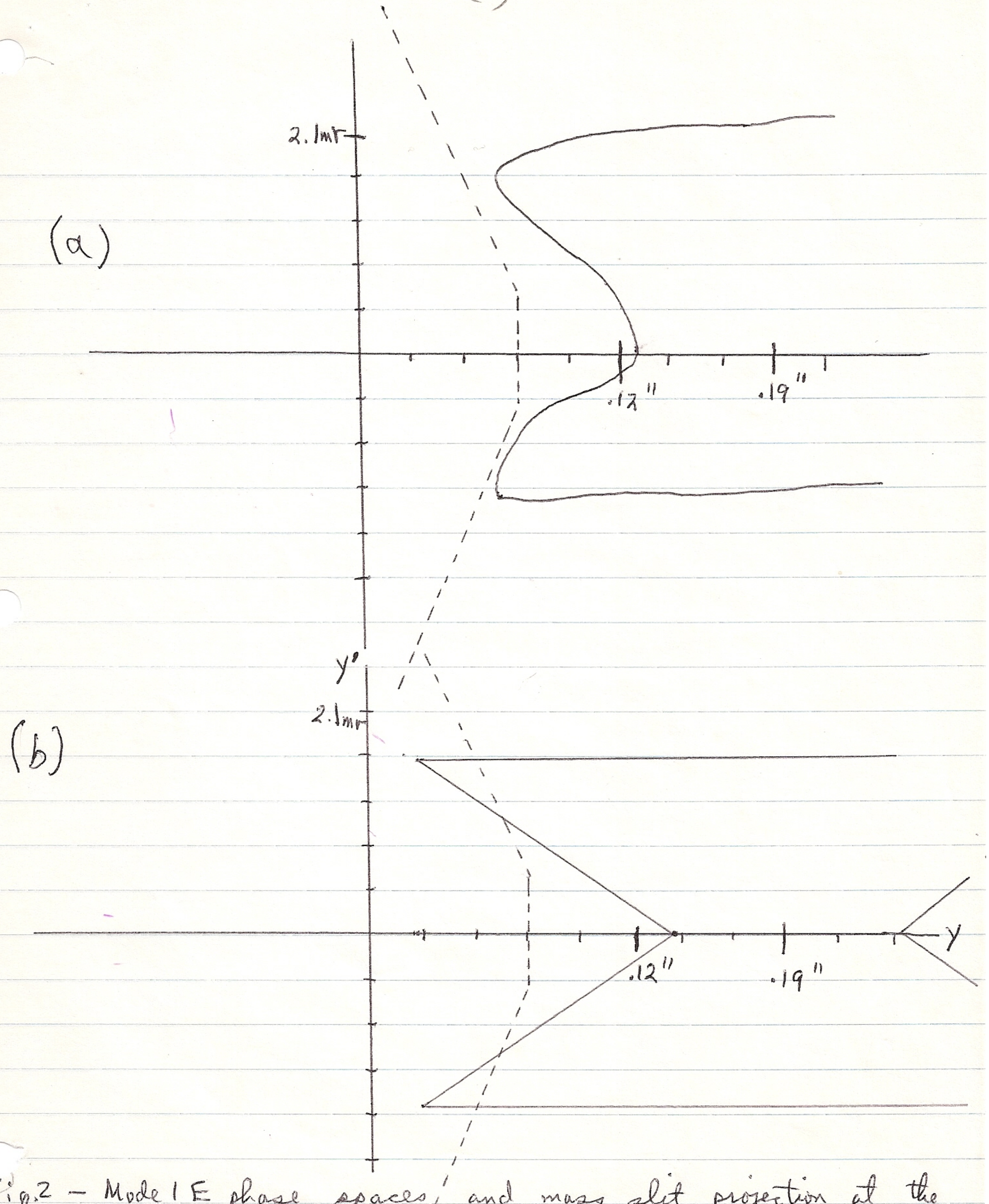
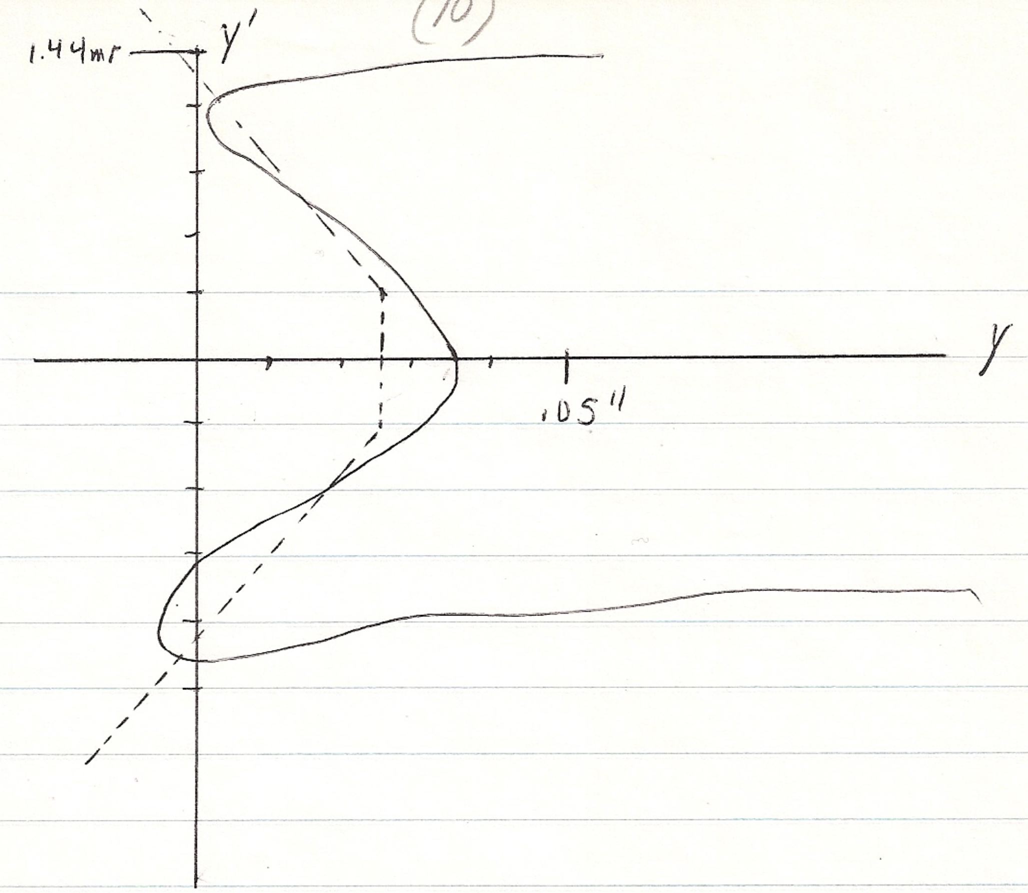


Fig.2 – Model E phase spaces, and mass slit projection at the mass slit.

(a)



(b)

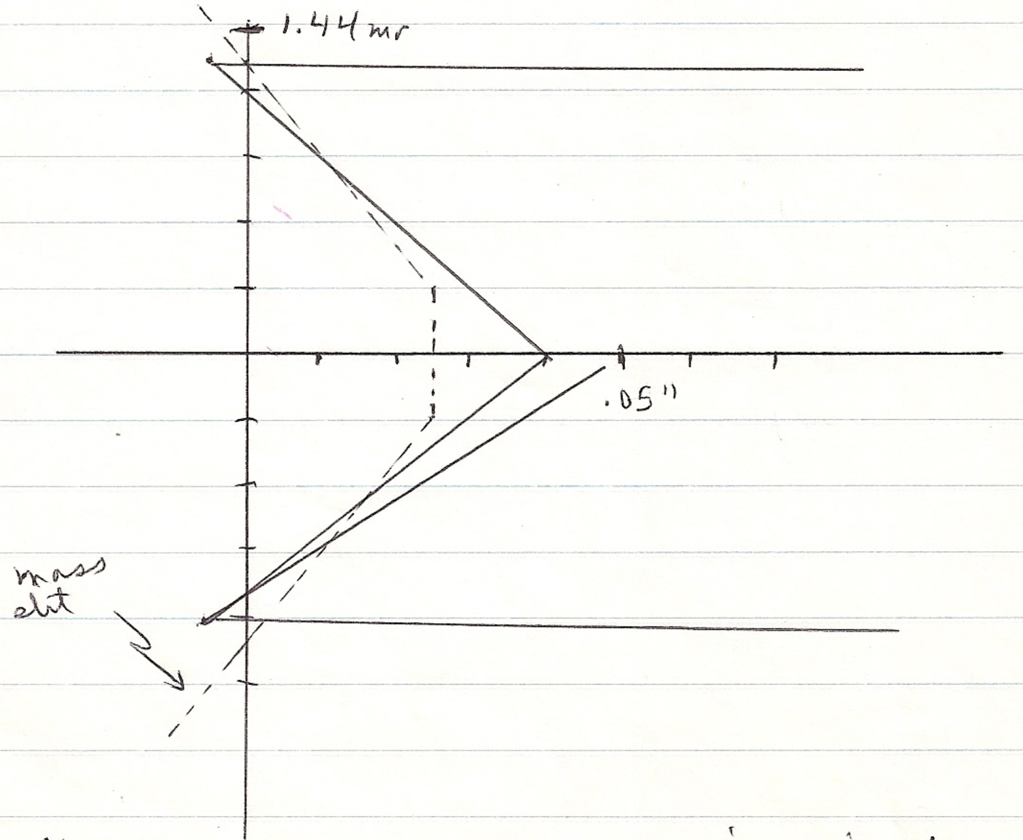


Fig. 3 – Mode 4 W phase spaces and mass slit projections

Mode E 1 (11)

	XMAX	DXMAX	YMAX	DYMAX	K1	K2	K3	K4	X1	DX1	Y1	DY1
ASS	4.00000	.10000	.23769	.00228	3	5	3	4	.001	.02000	.020	.00380

0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	0	0	2
0	0	0	0	0	0	0	0	0	0	0	2	2	11	2	0	0	17
0	0	0	0	0	0	0	0	0	1	2	4	9	6	6	1	2	31
0	0	0	0	0	0	0	0	0	1	5	7	12	16	9	12	1	63
0	0	0	0	0	0	0	0	0	2	8	8	19	19	16	5	4	81
0	0	0	0	0	0	0	0	1	4	9	8	28	23	26	15	3	117
0	0	0	0	0	0	1	0	1	6	10	14	19	27	32	20	8	138
0	0	0	0	0	0	0	2	1	3	4	13	16	27	24	28	23	141
0	0	0	0	0	0	0	1	1	3	7	8	21	25	36	27	16	145
0	0	0	0	0	0	0	0	0	1	1	3	10	28	24	23	34	124
0	0	0	0	0	0	0	0	0	0	3	2	6	26	22	20	27	106
0	0	0	0	0	0	0	0	0	0	1	3	7	20	29	40	26	126
0	0	0	0	0	0	0	0	0	0	0	0	2	11	18	31	30	92
0	0	0	0	0	0	0	0	0	0	0	0	4	6	19	16	30	75
0	0	0	0	0	0	0	0	1	0	1	1	1	8	15	18	11	56
0	0	0	0	0	0	0	0	0	1	4	2	4	5	8	9	6	39
0	0	0	0	0	0	0	0	0	0	4	0	3	2	3	6	4	22
0	0	0	0	0	0	0	0	0	0	2	3	1	1	1	0	1	9
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	1	3	5	22	61	78	164	262	291	271	226	.888 = UP/TOTAL

3.0 % leak thru

0	0	0	0	0	0	0	0	0	0	0	0	0	3	1	2	1	7
0	0	0	0	0	0	0	0	0	2	4	5	8	6	7	2	3	37
0	0	0	0	0	0	0	1	0	6	9	9	7	7	13	4	8	64
0	0	0	0	0	0	1	2	0	6	6	15	19	23	19	12	15	118
0	0	0	0	0	0	0	0	3	4	10	13	14	15	20	19	11	109
[illegible]	[illegible]	[illegible]	[illegible]	0	0	0	0	1	1	6	6	17	25	26	23	17	122
[illegible]	[illegible]	[illegible]	0	0	0	0	0	0	0	1	4	8	26	35	21	9	104
0	0	0	0	0	0	0	0	0	0	0	3	19	29	31	27	21	130
0	0	0	0	0	0	0	0	0	0	0	0	12	31	26	29	20	118
0	0	0	0	0	0	0	0	0	0	0	0	5	15	23	27	34	104
0	0	0	0	0	0	0	0	0	0	0	0	13	17	25	28	22	105
0	0	0	0	0	0	0	0	0	0	4	5	11	23	20	32	26	121
0	0	0	0	0	0	0	0	0	1	6	3	9	13	19	21	14	86
0	0	0	0	0	0	0	0	0	0	6	5	9	14	16	10	16	76
0	0	0	0	0	0	0	0	1	1	4	4	7	7	8	9	8	49
0	0	0	0	0	0	0	0	0	1	2	4	4	8	2	5	0	26
0	0	0	0	0	0	0	0	0	0	3	2	2	0	0	0	0	7
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	1	3	5	22	61	78	164	262	291	271	225	.888 = UP/TOTAL

.93 (CENTRAL RAY Y)/WAIST= 1.125 YMAX,YMIN= .313 .120 YMIN/GEOM.IMAGE HT =
TO MASS= .370 NTHIT= 3192 KILLK= 334 NK= 1474 KOUT/KIN= .815 NPI= 900
TR 0 9 22 39 56 75 92 126 106 124 145 141 138 117 81 63
AM

	Q2		D1	SEXD	DRF1	Q3	ENTR		SEP1	WALL	STOP	SEP2	EXIT
0	0	0	0	0	0	16	84	0	7	16	165	70	403
	SEX1		PLIM		SEX2	DRF4	D2	DD2		Q6		MASS	
	0	0	1250	0	0	31	0	0	415	45	0	425	

MESB, MODE E1 ** 1 ** **SMALL BENDS, DATE= 03/28/73

Fig. 4 (a)

'S JPRINT XMAX DXMAX YMAX DYMAX K1 (12) K2 K3 K4 X1 DX1 Y1
MASS MASS 4.00000 .10000 .09975 .00144 3 5 3 4 .001 .02000 .020

0	0	0	0	0	0	0	0	0	0	1	0	1	1	0	3	1	1	0	8
0	0	0	0	0	0	0	1	1	1	2	2	2	4	4	5	4	2	3	31
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0	0	0	0	0	0	0	0	1	1	1	2	10	25	33	35	26	14	6	154
0	0	0	0	0	0	0	0	0	0	3	2	13	16	30	35	30	19	7	155
0	0	0	0	0	0	0	0	0	2	2	3	6	19	21	24	18	20	6	121
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0	0	0	0	0	0	0	0	0	0	1	1	4	10	14	9	10	10	5	64
0	0	0	0	0	0	0	0	0	0	1	0	1	8	5	7	2	1	3	28
0	0	0	0	0	0	0	0	0	0	0	0	1	3	0	0	1	1	0	6
0	0	0	0	0	0	0	3	6	18	40	73	199	403	549	484	419	248	124	.611 =

0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	1	1	2	5	2	5	7	5	9	4	41
0	0	0	0	0	0	0	1	1	4	4	9	20	19	31	18	18	15	8	148
0	0	0	0	0	0	0	0	0	3	6	12	8	20	24	25	19	19	18	154
0	0	0	0	0	0	0	0	1	3	4	7	13	23	35	13	16	11	11	137
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0	0	0	0	0	0	0	0	0	0	1	5	16	24	40	21	27	13	8	155
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0	0	0	0	0	0	0	0	0	0	0	0	10	29	41	45	37	10	0	172
0	0	0	0	0	0	0	0	0	0	0	0	4	49	37	35	48	8	0	181
0	0	0	0	0	0	0	0	0	0	0	0	3	41	35	48	36	8	0	171
0	0	0	0	0	0	0	0	0	0	0	0	6	28	40	42	36	10	2	164
0	0	0	0	0	0	0	0	0	0	0	1	12	21	62	44	27	15	9	191
0	0	0	0	0	0	0	0	0	0	1	5	10	26	33	33	23	24	7	162
0	0	0	0	0	0	0	0	0	1	4	7	19	16	22	36	26	20	11	162
0	0	0	0	0	0	0	0	0	1	4	6	16	21	32	21	24	19	14	158
0	0	0	0	0	0	0	0	1	4	8	6	14	19	24	27	13	19	18	153
0	0	0	0	0	0	0	1	3	1	3	2	8	10	10	9	2	6	3	58
0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	1
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	3	6	18	40	73	199	403	549	484	419	248	124	.507 =

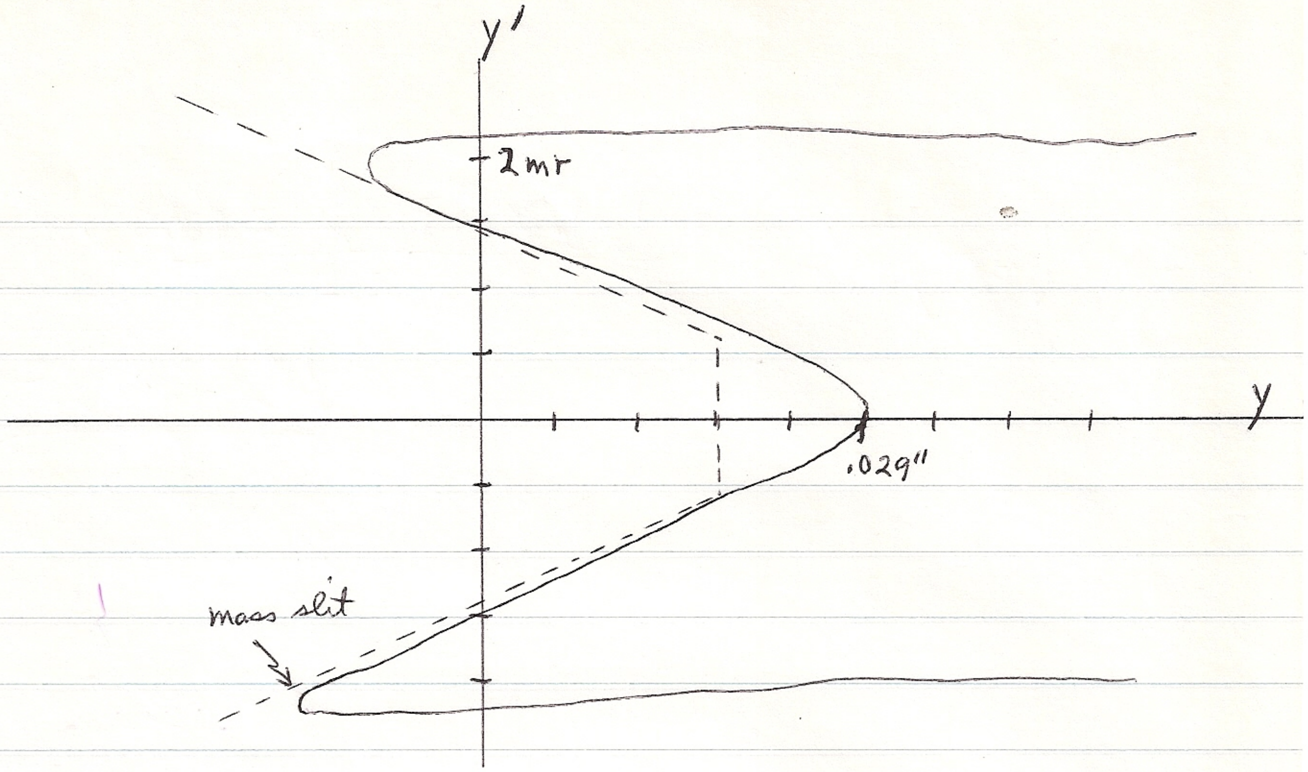
1% leak thru

= .048 (CENTRAL RAY Y)/WAIST= 1.253 YMAX,YMIN= .085 .036 YMIN/GEOM,IN
MISSION TO MASS= .540 NTHIT= 2345 KILLK= 1291 NK= 1364 KOUT/KIN= .514 NPI= 6700
TUM DISTR 6 28 64 82 121 155 154 211 208 219 244 219 209 193 1
S IN BEAM

RT	Q1		Q2		D1	SEXD	DRF1	Q3	ENTR		SEP1	WALL	STOP	SEP
	74	83	0	0	0	0	0	0	37	0	0	0	0	122
		SEXT		PLIM	DR64	DRF3	D2	DD2		Q6	DRF4		MAS2	MAS
	0	0	0	0	0	0	0	0	0	0	0	0	0	89

B E A M MPS 4** 4 ** DATE= 03/

Fig. 4 (b) Mode 4 W



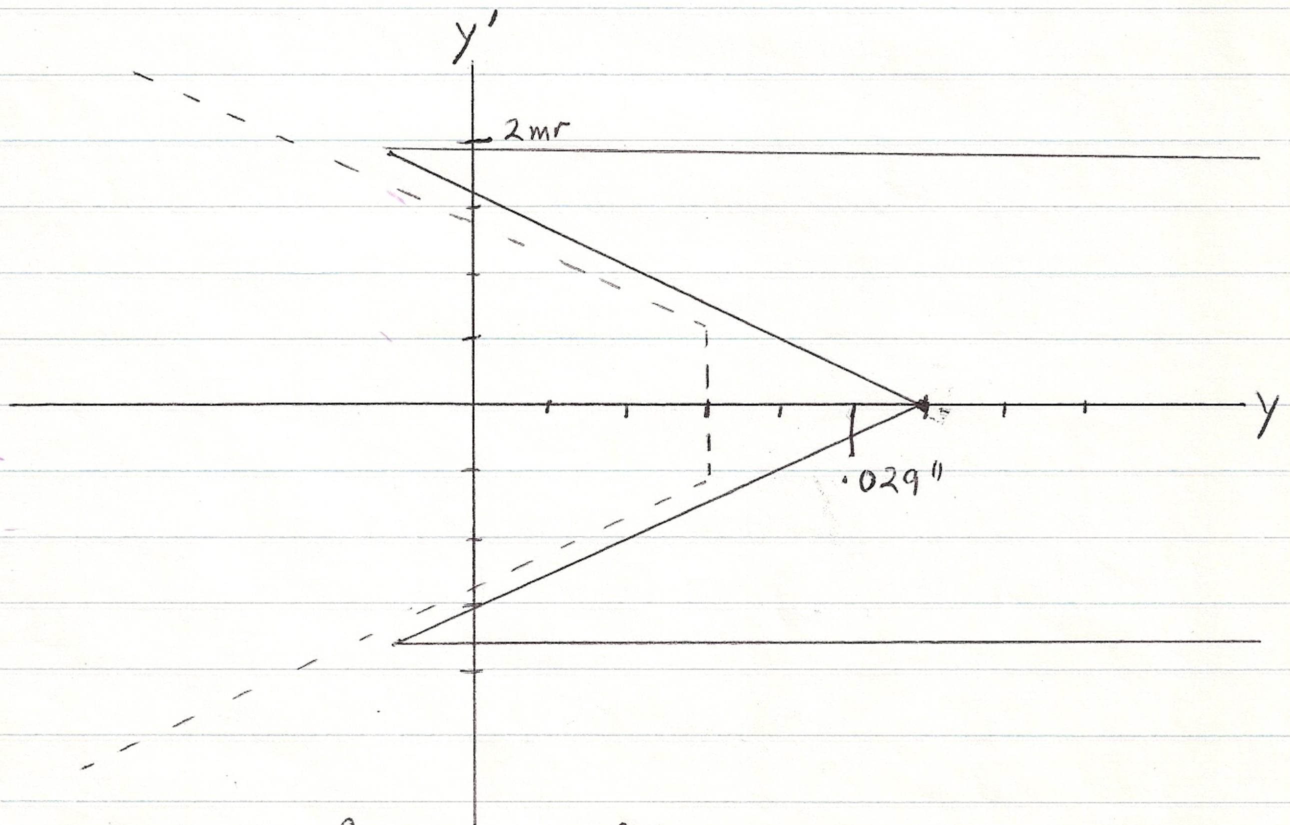


Fig. 5. Mode 3 W phase space plots

(14)

JPRINT		XMAX	DXMAX	YMAX	DYMAX	K1	K2	K3	K4		X1	DX1	Y1
MASS	MASS	4.00000	.10000	.06169	.00233	3	5	3	4		.001	.02000	.020

0	0	0	0	0	0	1	0	0	1	0	1	0	0	1	0	2	0	2	8
0	0	0	0	1	1	1	0	1	1	1	3	1	2	4	9	7	6	7	45
0	0	0	0	0	0	0	0	3	5	2	2	1	7	10	8	9	20	11	78
0	0	0	0	0	0	0	2	0	4	0	2	5	8	7	21	20	15	13	97
0	0	0	0	0	0	0	0	1	1	2	6	5	9	23	25	27	21	28	148
0	0	0	0	1	0	1	0	0	2	3	5	9	13	16	30	33	34	24	171
0	0	0	0	1	0	2	2	3	1	2	9	10	12	24	38	34	35	26	199
0	0	0	0	0	0	0	1	4	2	4	6	12	13	18	41	30	37	31	199
0	0	0	0	0	0	0	2	1	1	4	6	8	11	20	28	32	27	33	173
0	0	0	0	0	1	0	0	2	4	4	6	6	12	20	19	47	29	36	186
0	0	0	0	0	0	0	1	1	3	4	3	6	8	10	33	34	31	32	166
0	0	0	0	0	1	0	0	1	1	0	2	7	11	14	23	36	29	34	159
0	0	0	0	0	0	0	1	0	1	2	4	11	10	24	27	39	39	28	186
0	0	0	0	0	0	0	0	1	4	0	5	6	10	13	26	34	34	32	165
0	0	0	0	0	0	0	0	0	2	3	4	3	11	11	25	28	39	35	161
0	0	0	0	0	0	0	2	1	2	2	1	6	9	14	23	22	33	19	134
0	0	0	0	0	0	0	0	0	1	1	0	5	5	5	21	24	24	32	118
0	0	0	0	0	0	0	0	0	1	0	2	1	6	11	9	18	18	16	82
0	0	0	0	0	0	0	0	0	0	0	1	1	0	9	13	10	15	8	57
0	0	0	0	0	0	0	0	0	1	0	1	0	1	3	1	2	0	4	13
0	0	0	0	3	3	5	11	19	38	34	69	103	158	257	420	488	486	451	.672 =

y′

mass slit

2.33 mr

1.6% leak thru

0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	1	1	3	0	2	3	1	6	0	17
0	0	0	0	1	1	1	3	2	6	7	7	8	11	16	14	20	15	14	126
0	0	0	0	0	0	2	1	6	10	5	9	17	12	20	14	16	20	15	147
0	0	0	0	0	0	1	2	1	4	5	12	9	14	21	17	22	13	14	135
0	0	0	0	0	0	0	0	2	4	1	7	14	19	29	27	20	22	23	168
0	0	0	0	0	0	0	0	0	0	0	4	11	16	24	26	34	29	29	173
0	0	0	0	0	0	0	0	0	0	1	0	3	9	20	40	37	34	32	176
0	0	0	0	0	0	0	0	0	0	0	0	0	3	17	42	47	60	43	212
0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	55	62	49	62	232
0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	36	43	54	43	178
0	0	0	0	0	0	0	0	0	0	0	0	0	5	16	37	39	46	48	191
0	0	0	0	0	0	0	0	0	0	0	3	0	7	17	25	51	49	39	191
0	0	0	0	0	0	0	0	0	0	3	5	6	9	18	25	24	23	17	130
0	0	0	0	0	0	0	0	1	2	4	7	9	19	19	14	28	22	24	149
0	0	0	0	0	0	1	0	0	2	4	4	8	15	14	23	22	18	26	137
0	0	0	0	0	0	0	1	4	7	1	8	9	12	12	16	15	16	15	116
0	0	0	0	1	1	0	4	3	2	2	2	6	7	6	6	7	10	7	64
0	0	0	0	1	1	0	0	0	1	0	0	0	0	0	0	0	0	0	3
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	3	3	5	11	19	38	34	69	103	158	257	420	488	486	451	.592 =

y

0.0617"

```
      .040 (CENTRAL RAY Y)/WAIST=          1.332 YMAX,YMIN=        .073      .033 YMIN/GEOM.I
ISSION TO MASS= .690 NTHIT=  1590 KILLK=  700 NK=  2710 KOUT/KIN=  .795 NPI= 11300
UM DISTR        13   57   82  118  134  161  165  186  159  166  186  173  199  199
 IN BEAM
T  Q1             Q2              D1    SEXD   DRF1   Q3             SEP1   WALL   SEP2  EXIT
   73    87    0     0     0     0     0     0     0     1     34    639   132    79
1        PLIM             SEX2   DRF3   D2     DD2           Q6                       MASS
   9    452    0     0     0     0     0    10    13     0     0     0    865
     MESB, MODE MPS 3 ** 3 **  CRAM IT AL IN 12 INCH TARGET                          DATE= 03
```

Fig. 6