

Implications of Unshielded Bellows in RHIC

M. Blaskiewicz

October 1999

Collider Accelerator Department
Brookhaven National Laboratory

U.S. Department of Energy

USDOE Office of Science (SC)

Notice: This technical note has been authored by employees of Brookhaven Science Associates, LLC under Contract No. DE-AC02-98CH10886 with the U.S. Department of Energy. The publisher by accepting the technical note for publication acknowledges that the United States Government retains a non-exclusive, paid-up, irrevocable, world-wide license to publish or reproduce the published form of this technical note, or allow others to do so, for United States Government purposes.

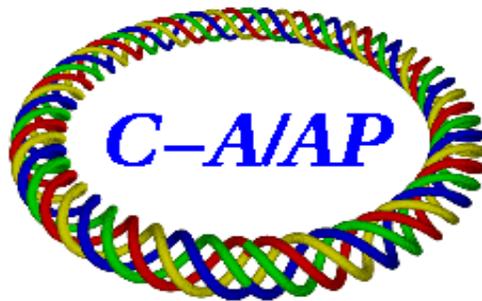
DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or any third party's use or the results of such use of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof or its contractors or subcontractors. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

C-A/AP/1
October 1999

Implications of Unshielded Bellows in RHIC

M. Blaskiewicz



**Collider-Accelerator Department
Brookhaven National Laboratory
Upton, NY 11973**

Implications of unshielded bellows in RHIC

Michael Blaskiewicz
CAD Brookhaven National Laboratory

Abstract

The implications of unshielded bellows in RHIC are discussed. It is found that unshielded bellows have a marginal impact on the impedance budget and will increase the heat load on the cryogenic system by about 10 watts.

1 Longitudinal Results

The model of the bellows used in the estimate is shown in Figure 1. The ABCI[1] simulations used a longitudinal bin size of $\Delta s = 0.25$ mm and a radial bin size of 1.0mm. This corresponds to a 10×10 grid in each bellows corrugation. The longitudinal and transverse wake potentials were calculated using a Gaussian pulse of rms length $\sigma_s = 1$ cm, which is short compared to the minimum length expected in RHIC; $\sigma_s \approx 10$ cm. The first meter of the longitudinal wake and the current pulse used are shown in Figure 2.

The Fourier transform of the wake potential is the impedance. The imaginary part of the longitudinal impedance (the longitudinal reactance) for the 24 and 30 corrugation bellows are shown in Figure 3 along with the impedance resulting from an inductance corresponding to $Z_{||}/n = 2$ m Ω . The numerically obtained curves are nearly straight lines below 2GHz, which agrees with measurements [2]. The real part of the longitudinal impedance (the longitudinal resistance) for the 24 and 30 corrugation bellows are shown in Figure 4. Note that the cutoff frequency for microwave propagation in a pipe of radius 3.4cm is 3.4GHz.

To estimate heating and dynamical effects two models of the beam will be used; a Gaussian pulse of rms length 10cm and a current pulse of the form

$$I(t) = I_p[1 - t^2/\hat{\tau}^2]^2$$

where $I = 0$ for $|t| > \hat{\tau}$ and $\hat{\tau}$ is chosen so that the rms length is 10cm. The second model is in fair agreement with observations of longitudinal spectra in the AGS.

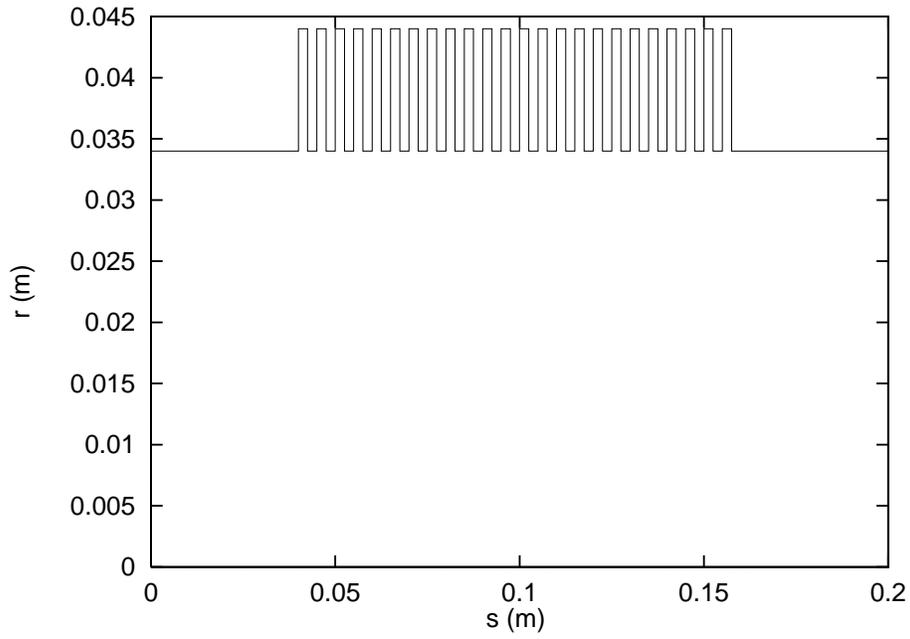


Figure 1: The geometry used in the ABCI calculations for 24 bellows corrugations. Simulations with 30 corrugations were also done.

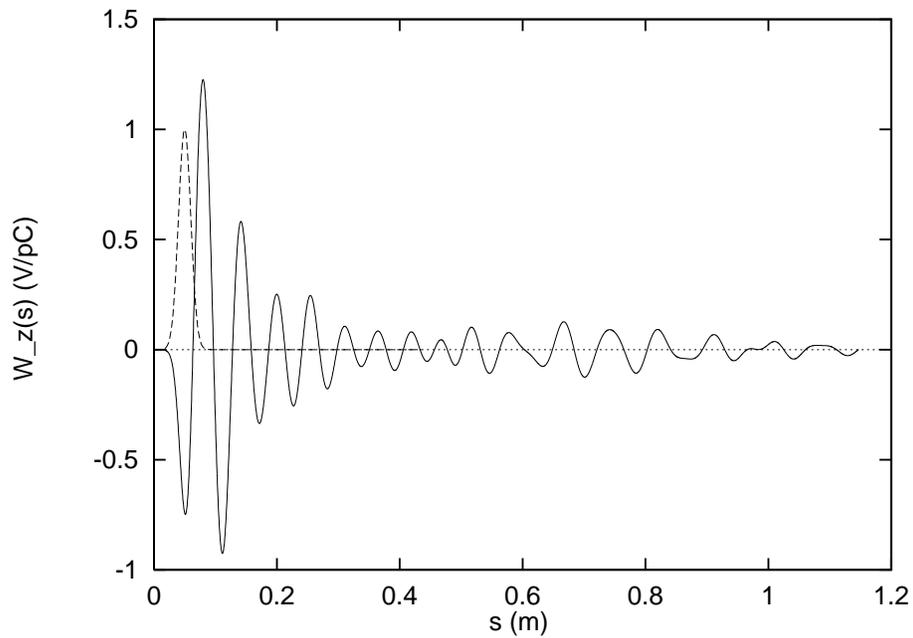


Figure 2: Current pulse and resulting longitudinal wake field for the geometry shown in Figure 1. The actual simulation went out to 10 meters of lag.

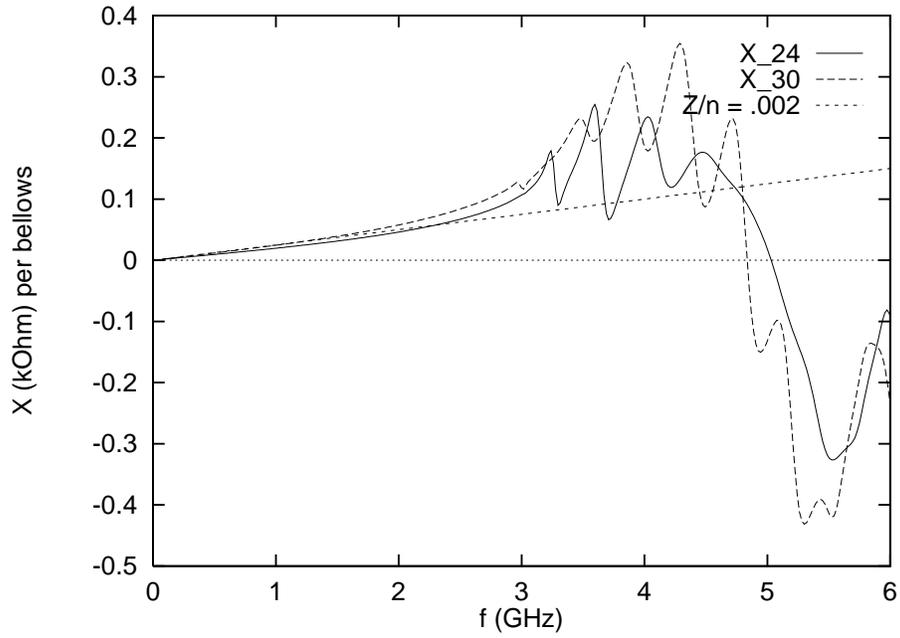


Figure 3: Longitudinal reactance for the 24 and 30 corrugation bellows models and a pure reactance with $Z_{\parallel}/n = 2 \text{ m}\Omega$.

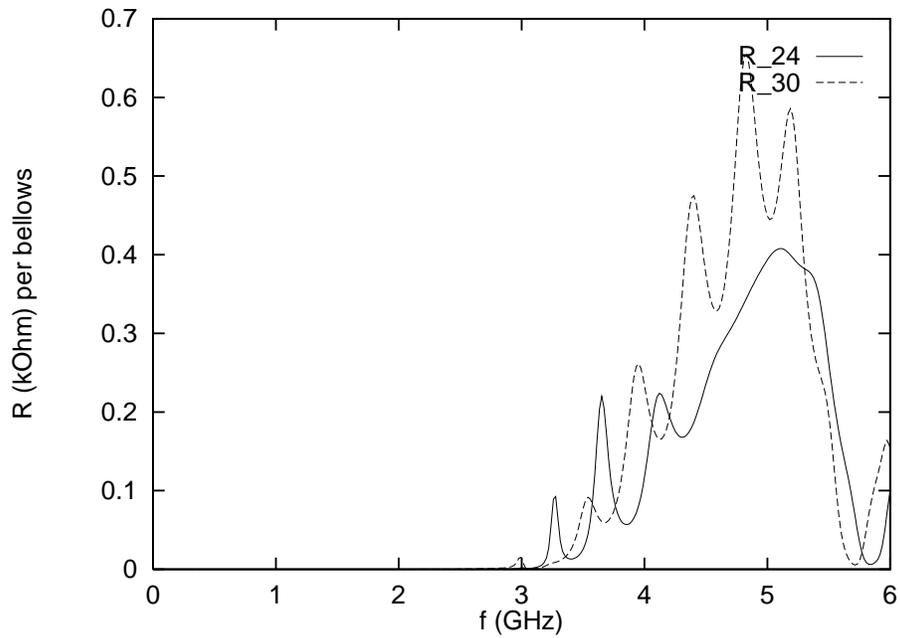


Figure 4: Longitudinal resistance for the 24 and 30 corrugation bellows models. The cutoff frequency for microwave propagation in a pipe of radius 3.4cm is 3.4GHz

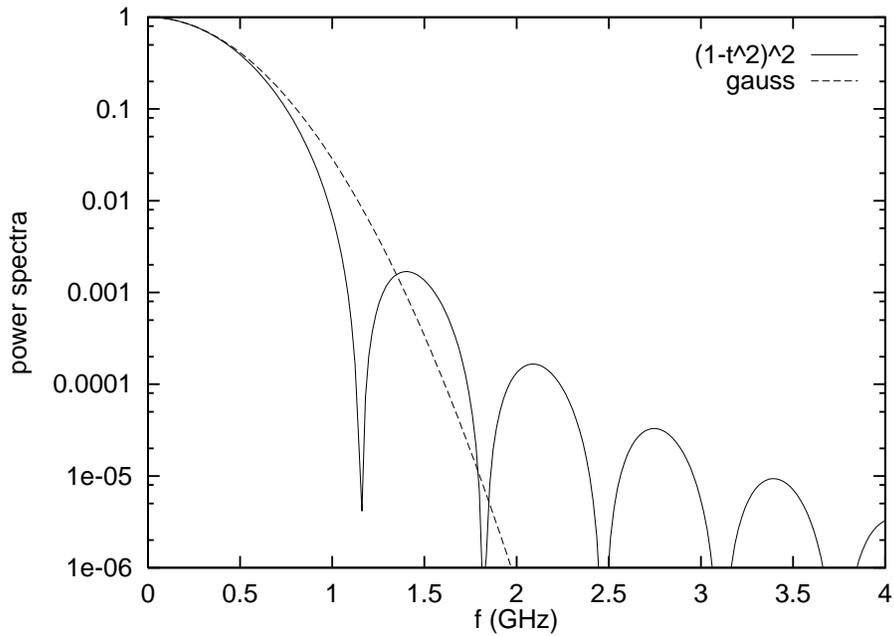


Figure 5: Power spectra for Gaussian current pulse and $I(t) = I_p[1 - t^2/\hat{\tau}^2]^2$. Both have a 10cm rms bunch length (1/3 ns rms duration).

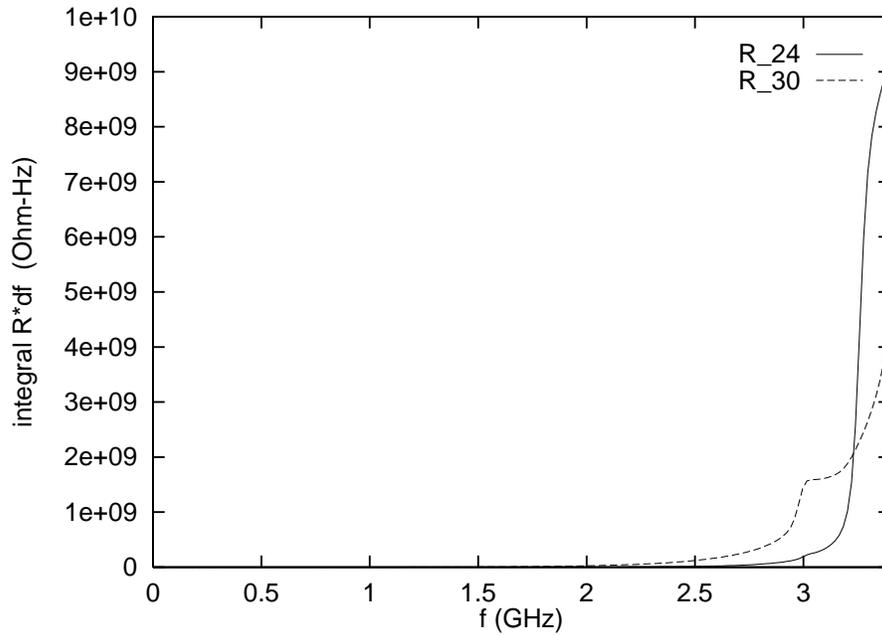


Figure 6: Integrals of resistance with respect to frequency used for estimating the R/Q values of trapped modes.

The absolute value squared of the Fourier transforms of these current pulses are shown in Fig 5. Note that the decay rate in frequency of the envelope of the solid line is essentially determined by how smoothly the pulse goes to zero in time.

Dynamical effects require that the bunch power spectra significantly overlap the impedance. Since both spectra are down by a factor of at least 10^4 by 2 GHz only frequencies below about 2 GHz are dynamically relevant. For longitudinal dynamics the bellows are pure inductors. The value of $Z_{||}/n = 2 \text{ m}\Omega$ corresponds to $Z_{||}/n = 0.2 \text{ }\Omega$ for 100 unshielded bellows per ring. Estimates of longitudinal microwave instability set a limit of $Z_{||}/n = 2 \text{ }\Omega$ and the stripline beam position monitors contribute $Z_{||}/n = 0.58 \text{ }\Omega$ [3]. It should be noted that a pure inductance with a parabolic current pulse is one of the few exactly solvable problems in instability theory. Starting with nearly matched initial conditions a pure inductance *never* causes instability [4]. The main dynamical effect of unshielded bellows will probably be seen around transition. The reactance and the longitudinal space charge impedance will cause a longitudinal mismatch across transition which may require some sort of active damping. This is not unforeseen and since the bellows are a small addition to the BPMs it is not an issue.

Heating effects are more subtle. The problem splits into two main parts. The first part involves the trapped modes with resonant frequencies below pipe cutoff. The simulation code reliably predicts the values of R_{sh}/Q for these modes. The values of R_{sh}/Q are found by integrating $R(f)$ with respect to frequency over the numerically induced line width. The values of these integrals for frequencies below pipe cutoff are shown in Figure 6. The maximum value of these integrals is $\approx 10\Omega\text{GHz}$. If this integral is ascribed to a single resonance then the parameters of the resonance satisfy $R_{sh}\omega_r/(4Q) = \text{integral}$, where ω_r is the angular frequency of the resonance. Setting $\omega_r = 2\pi \times 3\text{GHz}$ yields $R_{sh}/Q = 2.1\Omega$ and 0.32Ω for the 24 and 30 convolution cases, respectively. The quality factor for the resonance is estimated using the scaling $Q = r_{char}/\delta_{skin}(\omega_r)$, where r_{char} is the characteristic transverse dimension and $\delta_{skin}(\omega_r)$ is the skin depth evaluated at the resonant frequency [5]. Taking a resistivity of $70\mu\Omega\text{cm}$ [6] the resulting estimate is $Q \approx 2600$. If anything, this is an overestimate, which will overestimate the heating. Multiplying R_{sh}/Q by Q yields a shunt impedance of $R_{sh} = 5.5 \text{ k}\Omega$. In the worst case the resonant frequency will be a multiple of the bunching frequency. This is assumed since the code and its input are not reliable at this level. The resulting power dissipation is given by

$$P_{res} = 2I_{dc}^2 R_{sh} F_b(f_r),$$

where I_{dc} is the dc beam current and $F_b(f_r)$ is the form factor shown in Figure 5, evaluated at the resonant frequency. For 120 bunches with 2×10^{11} charges each $I_{dc} = 0.30\text{A}$. Using the envelope of the larger curve in Figure 5 gives $F_b(f_r) = 2 \times 10^{-5}$. The net power is $P_{res} = 20\text{mW}$.

Along with the power dissipated in the narrow band resonance there is the power

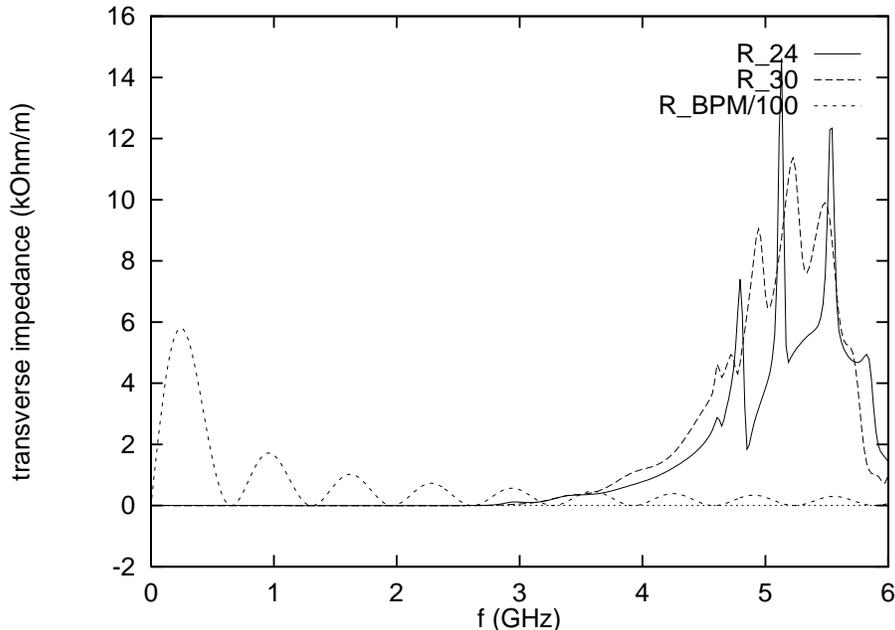


Figure 7: Transverse resistance versus frequency for the 24 and 30 convolution models. The transverse resistance of the stripline BPMs, divided by 100, is shown for comparison.

loss due to the broad band resistance. This contribution is given by

$$P_{bb} = 2f_b Q_b^2 \int_{f_{cut}}^{\infty} df F_b(f) R(f),$$

where f_b and Q_b are the bunching frequency and charge per bunch, respectively. Using the larger form factor in Figure 5 yields $P_{bb} = 12\text{mW}$. The net power dissipation per bellows is then $P_{tot} = 32\text{mW}$ which, for 200 bellows in all, yields a 6W load on the cryogenic system. There is a factor ~ 100 safety margin between this estimate and a noticeable load on the cryogenic system. It is interesting to note that this factor of 100 is just the increase in power one obtains by using an *unphysical* parabolic current pulse.

2 Transverse Results

Transverse impedance was estimated using the same input geometry as for the longitudinal impedance. The transverse resistance and reactance for the two bellows models are shown in Figures 7 and 8 respectively. For comparison purposes the transverse impedance of the stripline BPM system, normalized by the number of bellows, is also shown.

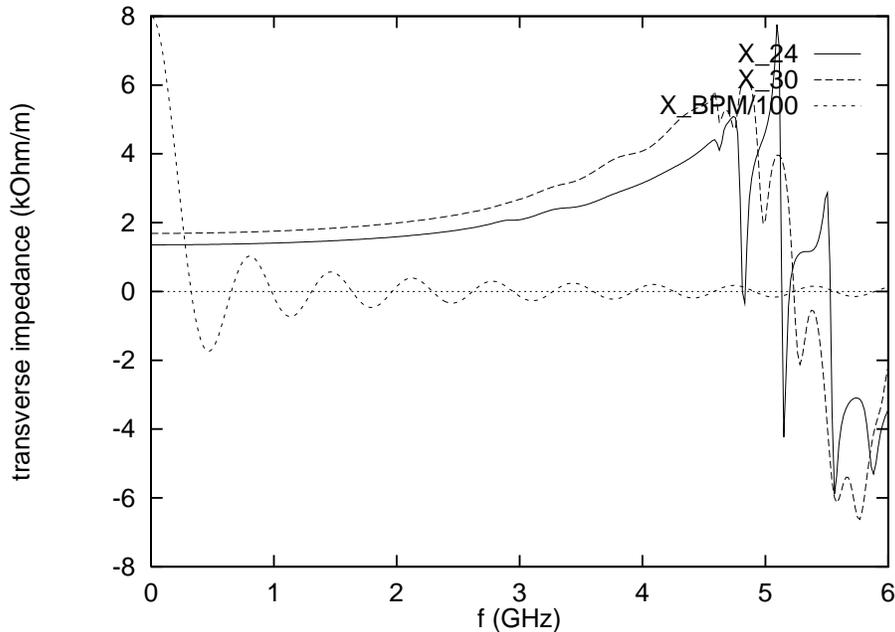


Figure 8: Transverse reactance versus frequency for the 24 and 30 convolution models. The transverse reactance of the stripline BPMs, divided by 100, is shown for comparison.

As in the longitudinal case, for dynamical purposes unshielded bellows introduce a pure reactance. For the 24 convolution case the contribution per bellows is $i1.4 \text{ k}\Omega/\text{m}$ which results in $i140 \text{ k}\Omega/\text{m}$ for 100 unshielded bellows per ring. The BPM contribution is 4 times larger at low frequencies. The frequency dependence of the BPM impedance is more dangerous than a pure reactance. As in the longitudinal case an exact solution exists for transverse stability with a pure reactance. The beam is always stable.

Heating due to the transverse modes will be present only if the closed orbit does not go down the center of the pipe. The heating due to the transverse mode will be comparable to the longitudinal mode heating for closed orbit distortions of order one centimeter. This is a large closed orbit distortion for high intensity operation so heating due to transverse modes will be negligible.

References

- [1] Y.H. Chin, User's Guide for ABCI Version 8.7, CERN SL/94-02 (AP) (1994).
- [2] Comparison of the Bellows Impedance Calculation with Measurement, V. Mane, RHIC/AP/7 (1993).

- [3] Collective Instabilities in RHIC, Editors S. Peggs and W.W. MacKay, RHIC/AP/36 (1994).
- [4] D. Neuffer, Stability of Self-Consistent Longitudinal Phase-Space Distribution Under Space Charge Perturbations, *Particle Accelerators* **11** p23 (1980).
- [5] J.D. Jackson, Classical Electrodynamics, pg 359, Wiley, (1975).
- [6] G. McIntyre private communication