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Coherent Instability in the Booster

S. Y. Lee

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Collider Accelerator Department

Brookhaven National Laboratory

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COHERENT INSTABILITY IN THE BOOSTER

Booster Technical Note
No. 19

S. Y. LEE, J. M. WANG, W. F. ZHAO

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HIGH ENERGY FACILITIES
Brookhaven National Laboratory
Upton, N.Y. 11973

Coherent Instability in the Booster

S.Y. Lee, J.M. Wang and X.F. Zhao Brookhaven National Laboratory

ABSTRACT

Longitudinal and transverse instability for the booster is evaluated. We found that the fast growth in the microwave region is not important. The slow growth of the head-tail mode can not be damped due to large space charge impedance at the low energy. Because of its small growth rate, the total growth is found to be maximum a few percent in the transverse phase space area.

1) Introduction

The coherent instability for a low energy booster is dominated by the space charge effect. To obtain the limitation of the booster performance and to evaluate the requirement of the correction elements in the booster, we shall concentrate in this paper to the collect effects. Section 2 discuss the single bunch phenomena and section 3 discuss the coupled bunch modes. The conclusion is given in section 4.

2) Single bunch collective effects.

In the single bunch collective effect we shall discuss the longitudinal motion as well as the transverse resistive wall instability. Table 1 list the relevant parameters in the booster performance for various ion spaces.

Т	Table 1		Booster Parameters in the coherent effect				
part.species	P	D	C	S	Cu	I	Au
A <q> N(10**9) beta(inj) gamma(inj) eps(10-6pi) epsn eta</q>		2 100 0.1768 1.01600 50 8.98148 -0.9253	50 6.36085	1.00505 50 5.03534			50 2.31748
space charge dnu(F/B)	 0.07681	0.02235	0.05929	0.05901	0.07813	0.08727	0.08289
@injection Trev(10^-6s) N(10^9)/mus Tfill(mus) <n>fill frev*2*pi</n>		3.28 30.4878 8.00843	0.5125	0.125 53.6 7.97942	8.60704 0.06875 68.3636 7.94275 730004.		
deltaE dE/E(^-3)	0.11763	3026.27 0.30710 35986.1 0.01902	0.06234 3063.24 0.30710 152261. 0.01351	0.05805 2878.64 0.30710 300171. 0.01002	0.05051 2520.38 0.30710 401347. 0.00682	2090.22 0.30710 508491. 0.00429	1792.21 0.30710 525129.
coastingbeam U=	-39790. 422.964	4.70375	-68 4 6.2 5.28 7 09	2.93800	2.08495	1.17289	-3510.9 0.59420 1.00004

2a) Microwave instability fast growth

The fast growth microwave instability can be estimated by the Keil-Schnell formula. The beam paticles are injected and extracted below transition energy. Table 2 lists the impedance limit of the booster, where

$$|Z_{\bullet}/n| < \frac{2\pi |n| \in A}{9e I_{P}} \left(\frac{\sigma_{P}}{P}\right)^{2}$$

$$|Zt/n| < \frac{4\sqrt{2\pi} |n| \in A}{9e I_{P} \overline{\beta}} \left(\frac{\sigma_{P}}{P}\right)^{2}$$

Table 2. Microwave instability limit

part.spices	P	D	C	S	Cu	I	Au
long(Ohm)	120.	24000	2.9E6	2.E7	9.E7	4.E8	2.E9
trans(MOhm/m)	97.	9.4E4	8.4E5	5.E6	2.E7	8.E7	3.E8

The total impedance of the booster ring can be calculated by using programs such as URMEL and TBCI of T. Weiland of DESY. K.Y. Ng of FNAL calculated the impedance of the booster ring to obtain Z/n=3.3 Ohms for the longitudinal motion and Z/n=.02MOhms for the transverse motion. We therefore conclude that the fast growth microwave instability will not be important in the booster.

2b) Slow growth collective effects

The coherent growth due to the resistive wall is related to the transverse coupling impedance, Zt

$$Z_{4} = -\frac{i}{e\beta I_{0}} \int \langle F_{y} \rangle dz = i R Z_{0} \left[\frac{1}{\beta^{2} \sqrt{2}} \left(\frac{1}{a^{2}} - \frac{1}{b^{2}} \right) - (1+i) \frac{\delta}{b^{3}} \right]$$

The coefficients for the dispersion relation, U+(1+i)V, is given by

$$U + (4+i)V = \frac{Ncr_0}{2\pi a^2 \alpha \beta \kappa} \left[-\frac{1-\kappa^2}{\gamma^2} + (1+i)\beta^2 \kappa^2 \frac{\mu \delta}{b} \right]$$

We shall solve the dispersion relation,

$$1 = \left[U + (HC) V \right] \int \frac{f(p) dp}{\omega - (n-Q) \Omega}$$

by using the Gaussian distribution in the momentum distribution. The result is given in Fig. 1, where we have used the normalized unit, i.e.

$$U'+(1+i)V'=\left[U+(1+i)V\right]/\Delta S'$$

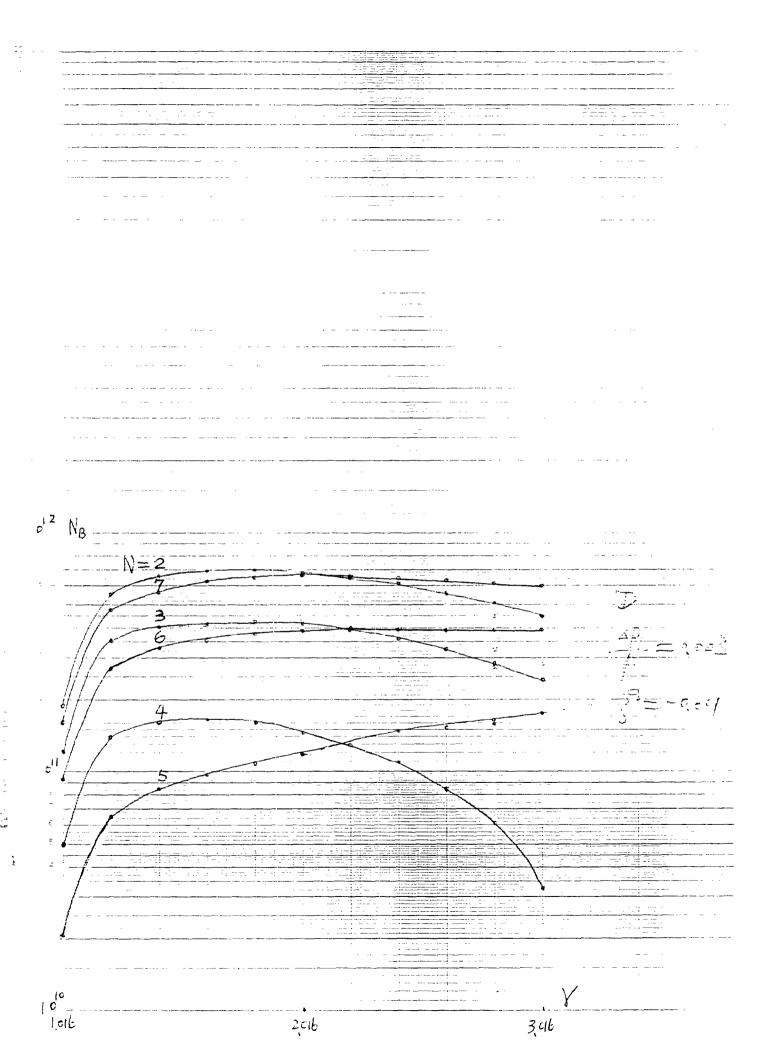
with

$$\Delta S = |(n - Q_0) \eta + Q'| \Omega_0 \frac{\Delta p}{p}$$

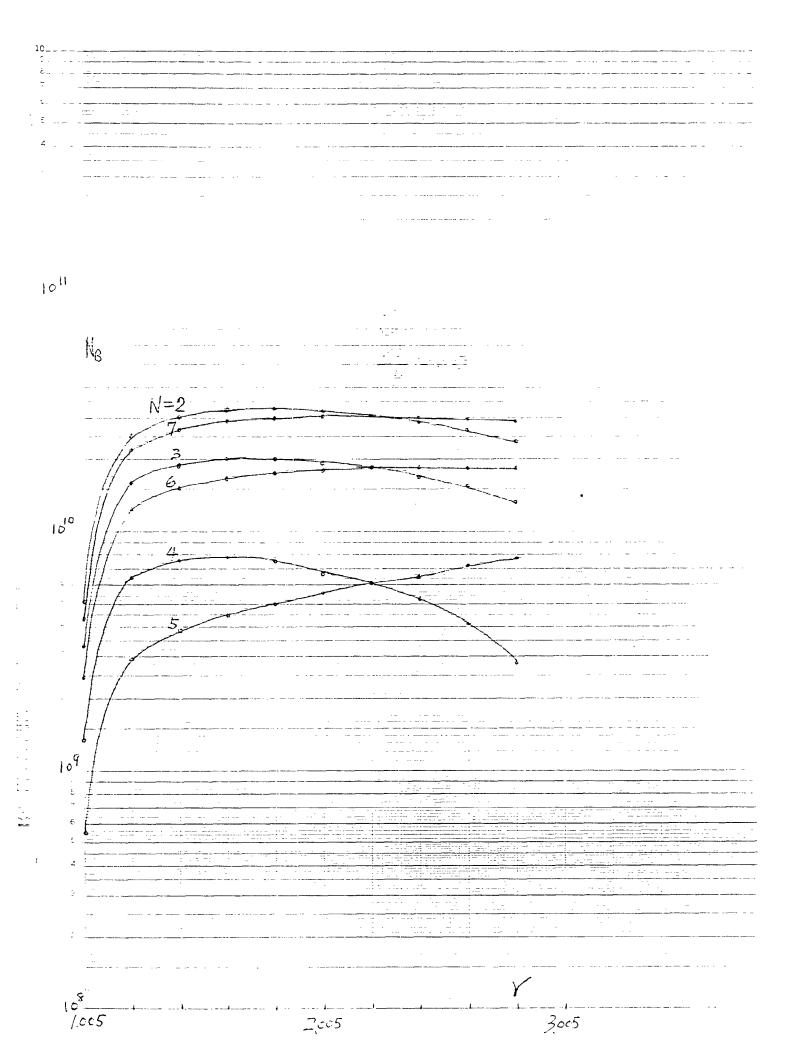
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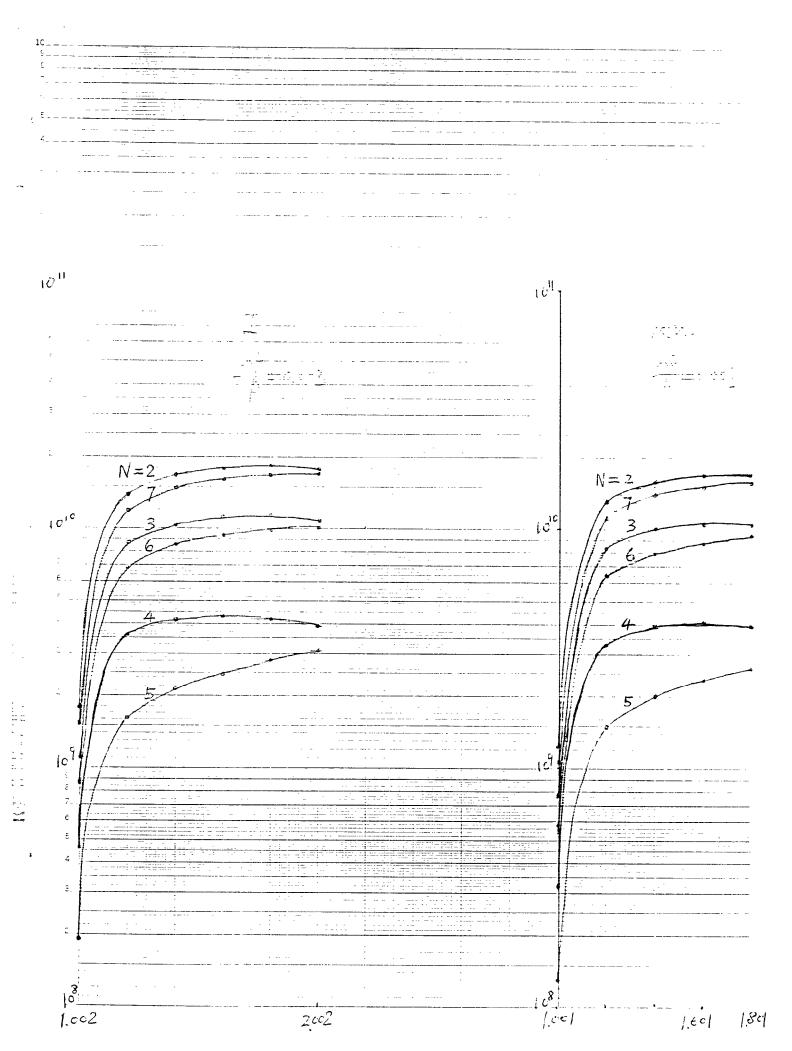
We observe that when the real part, U (corresponding to imaging part of the impedance) becomes very large. The landau damping becomes ineffective. The growth rate equals the resistive wall contribution. Table 1 lists the V component. The total growth of the transverse phase space is given by

where we have integrated the growth rate with the storage time in the booster. Figs. 2-6 show the instability limit as a function of the beam energy. At the low energy, the space charge impedance is large, we shall encounter instability irrespective of the Landau damping width. The Landau damping width, which induces mixing, shall be important in the dissipation of the growth into the phase space area. These damping width can be adjusted by the chromatic sextupoles. Since the total growth is of the order of a few percents. The transverse instability may not be important. Because of the slow growth, a feed back system shall still be considered to cure the head-tail mode.









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3) Couples bunch impedance in the rf detuning.

The booster shall be operated at h=3 harmonic mode, therefore there are possibly 3 coupled bunch mode in the booster. The eigenstate of the coupled bunch mode have the following coherent frequency shift,

$$\Delta\Omega = i \frac{q e \eta I_0 \omega_0^2}{2\pi E \omega_{sio}} \frac{1}{2^{a(a-1)!}} \hat{\theta}^{2a-2} Z_{eff} ; \hat{\theta} = rms bunch lougth$$

where $I_{\boldsymbol{o}}$ is the total average current and the effective impedance is given by

$$Z_{\text{eff}} = \sum_{n=-\infty}^{\infty} (nh+s) Z[(nh+s)\omega_0 + \Omega] e \qquad ; \Omega \simeq \alpha \omega_{so}$$

$$\frac{1}{h \hat{\theta} \geq 1} Z \cdot \frac{(\alpha-1)!}{\hat{\theta}^{2\alpha-1}}$$

Since the synchrotron frequency ω_s is a function of the synchrotron amplitude, the resulting frequency provides Landau damping for the coupled bunch motion,i.e.

$$1 = -i \frac{\eta \omega_0^3 h}{2\pi \rho \rho c} a \left[\frac{1}{2a_1} \right] Z_{eff} \int_0^{\infty} dr \frac{r^{2a} \psi_0'(r)}{\Omega - a \omega_s(r)}$$

where we have integrated the synchrotron amplitude in the dispersion integral. Assuming that all the nonlinearity of the synchrotron frequency is provided by the natural rf voltage,

$$V(t) = \hat{v} \sin (h\omega_0 t)$$

we obtain the limiting impedance to be

$$\left| \overrightarrow{E} \right| \leq \frac{2\pi E \omega_{sc}}{qe \eta I_0 \omega_0^2} \frac{2^{\alpha} a!}{\hat{\theta}^{2\alpha \cdot 2}} 0.32 Fa \frac{h^2}{16} \omega_{so} (2.5 \hat{\theta})^2$$

Table 3 shows that limit impedance of the booster for the stability of the copled bunch motion. The stability limit may be severe only in the case of proton beams, where \Zeff\<6000Ohm and \Zeff\<35MOhm is required to have stable coupled bunch motion for dipole mode and for quadrupole mode respectively.

Table 3 Impedance limit for the Coupled bunch mode instability

Coupled bunch instability							
-	P	D	C	S	Cu	I	Au
dOhmegaS Zmax/factor Zmax(a=1) Zrw/Zmax	1151.22 5825.34	1134339 5739921	2362859 1E+07	6643300 3E+07	1E+07 7E+07	693.060 3E+07 2E+08 0.00152	9E+07 4E+08
Mode factors a Fa' total factors	1 0.777 =5.06014	2 1.12 309.345	1.37	4 1.59 2369796	5 1.78 3E+08	6 1.96 4E+10	

4) Conclusion

In conclusion we have studied the possible coherent effects for the bunched beam in the booster. The transverse resistive wall instability can contribute at most a few percent of the phase space growth. The growth rate is much smaller than the synchrotron grequency. Thus these mode corresponds to the head tail instability, which can be controlled by the feed back system. We examine also the coupled bunch instability and calculate the preliminary effective impedance for the coupled bunch motion. The impedance shall be evaluated when the rf design is tested. Our conclusion is however that only the proton may be important to the coupled bunch motion.