



BNL-105146-2014-TECH

Booster Technical Note No. 99; BNL-105146-2014-IR

Booster survey and linear lattice parameters with program MAD

Z. Parsa

November 1987

Collider Accelerator Department
Brookhaven National Laboratory

U.S. Department of Energy

USDOE Office of Science (SC)

Notice: This technical note has been authored by employees of Brookhaven Science Associates, LLC under Contract No. DE-AC02-76CH00016 with the U.S. Department of Energy. The publisher by accepting the technical note for publication acknowledges that the United States Government retains a non-exclusive, paid-up, irrevocable, world-wide license to publish or reproduce the published form of this technical note, or allow others to do so, for United States Government purposes.

DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or any third party's use or the results of such use of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof or its contractors or subcontractors. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

*BOOSTER SURVEY and
LINEAR LATTICE PARAMETERS
with PROGRAM MAD*

AD

*Booster Technical Note
No. 99*

*Zohreh Parsa
November 1987*

*ACCELERATOR DEVELOPMENT DEPARTMENT
Brookhaven National Laboratory
Upton, N.Y. 11973*

BOOSTER SURVEY
AND
LINEAR LATTICE PARAMETERS
WITH
PROGRAM MAD

Zohreh Parsa

Accelerator Development Department
Brookhaven National Laboratory
Upton, New York 11973

ABSTRACT

This note describes the coordinates of AGS Booster in the Booster centered frame of reference, with program MAD. The results agree with and confirm our earlier calculation. The linear lattice parameters for $\Delta(P)/P = -.01$ to $.01$ in increments of $.002$ are also included.

TABLE OF CONTENTS

- I. INTRODUCTION
- II. BOOSTER SURVEY WITH MAD
- III. COORDINATE SYSTEM CONVENTIONS
- IV. CONCLUSION
- V. REFERENCES

FIGURE 1 (a, b, c)	; REFERENCE COORDINATE CONVENTIONS.
FIGURE 2	; LAYOUT OF THE BOOSTER AND ITS SUPERPERIODS.
TABLE I	; DEFINITION AND MAGNITUDE OF THE ELEMENTS AND PARAMETERS.
TABLE II	; LATTICE PARAMETERS FOR $\Delta(P)/P = 0$.
TABLE III	; SURVEY OF THE AGS - BOOSTER.
TABLE IV a-k	; LATTICE FUNCTIONS FOR THE AGS BOOSTER WITH $\Delta(P)/P = -.01$ TO $.01$ with .002 increments.

I. INTRODUCTION

This note includes the results of the Booster Survey obtained with program MAD [1] (versions [2] 4.03 and 6 produced same results).

In Table I, we present the definition of the ring elements inputed into program MAD, (with lengths in meters).

In Table II, linear lattice parameters with $\Delta(P)/P = 0$ are summarized and in Table III, the results of the MAD program Survey (for the Booster is given. This table (III), show the coordinates of an on axis point of the downstream end of that element when viewed in clockwise direction.

Table IV, gives the lattice functions for the Booster, calculated with program MAD6, for $\Delta(P)/P = -.01$ to $+.01$ in increments of .002.

II. BOOSTER SURVEY WITH MAD

Coordinates of the AGS Booster in the Booster centered reference system, was generated with program MAD. The values listed in Table III correspond to the coordinates of an on - axis point of the downstream end of that element when viewed in a clockwise direction. Assuming the magnets have sharp edges where the field becomes zero. These coordinates (given in Table III) agrees with and confirm our previous results [3], we obtained using a CDC - version of the Geometry program [4].

In the present calculation (shown in Table I) we used thick lens sextupoles of length .1 m; whereas in reference [3] thin lens sextupoles of zero length were assumed.

Figures 1 and 2 are also included showing the conventions used in program MAD (e.g. coordinates and angles given in Table III), and in the layout of the Booster lattice (e.g relative positions of magnets and Booster superperiods) respectively.

The transformation from the Booster centered reference system to the AGS and BNL grids are discussed and tabulated in subsequent note [5].

III. COORDINATE SYSTEM CONVENTIONS

Figure 1 shows the Global reference coordinates as follows:

X (displacement of the local origin in the X direction),
 Y (displacement of the local origin in the Y direction),
 Z (displacement of the local origin in the Z direction).

Where X is the East (E) and -Z is the North (N) direction.

θ (THETA in Table III) is the azimuth angle (i.e. the rotation angle about the global Y axis, between the projection of the reference orbit onto the (Z,X) plane, and the global Z axis).

ϕ (PHI) is the elevation angle and ψ (PSI) is the roll angle about the local s axis (see Figure 1 (c)). For more detail of MAD conventions see the MAD program manual [1].

IV. CONCLUSION

The coordinates of the Booster were generated using program MAD. The result obtained agreed with and confirms our previous calculation given in the Booster Design Manual. The transformations from the Booster center-ed reference system to AGS and BNL grids and the coordinates of the apex of the dipoles and centers of the quadrupoles and sextupoles are generated and given in the subsequent note [5].

V. REFERENCES

1. F. C. Iselin, CERN, Geneva, Switzerland, Principal author of program MAD (versions 4 and 6).
2. Available in BNLDAG::DUA0:[PARSA1.MAD] DIRECTORY.
3. Z. Parsa, Booster Technical Note No. 27 and Booster Desing Manual.
4. Originally was designed for ISABEL (E. Courant). Now modified for the Booster (I refer to it as) BSTGEO.FOR (VAX version), and a version we use for the RHIC coordinate calculation, (will be referred to as) GEOMETRY.FOR (also VAX version).
5. Z. Parsa, AGS Booster Geometry and Coordinates, Booster Technical Note; November 1987, (No 100).
6. E. Courant, Z. Parsa, Booster Lattice, Booster Technical Note No. 1; January 1986.

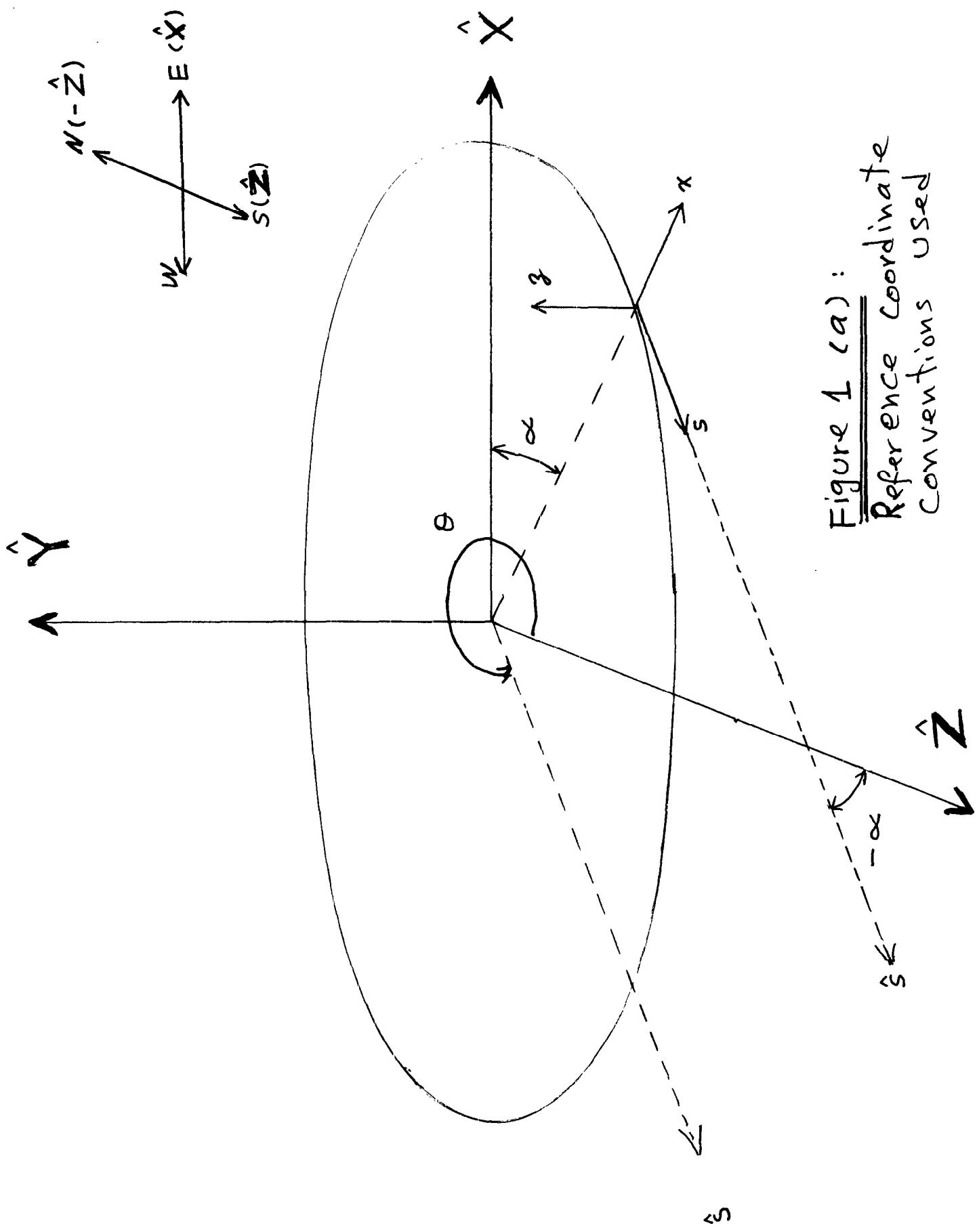


Figure 1 (b and c):
Local and Global
Coordinate Conventions
Used.

Page 6

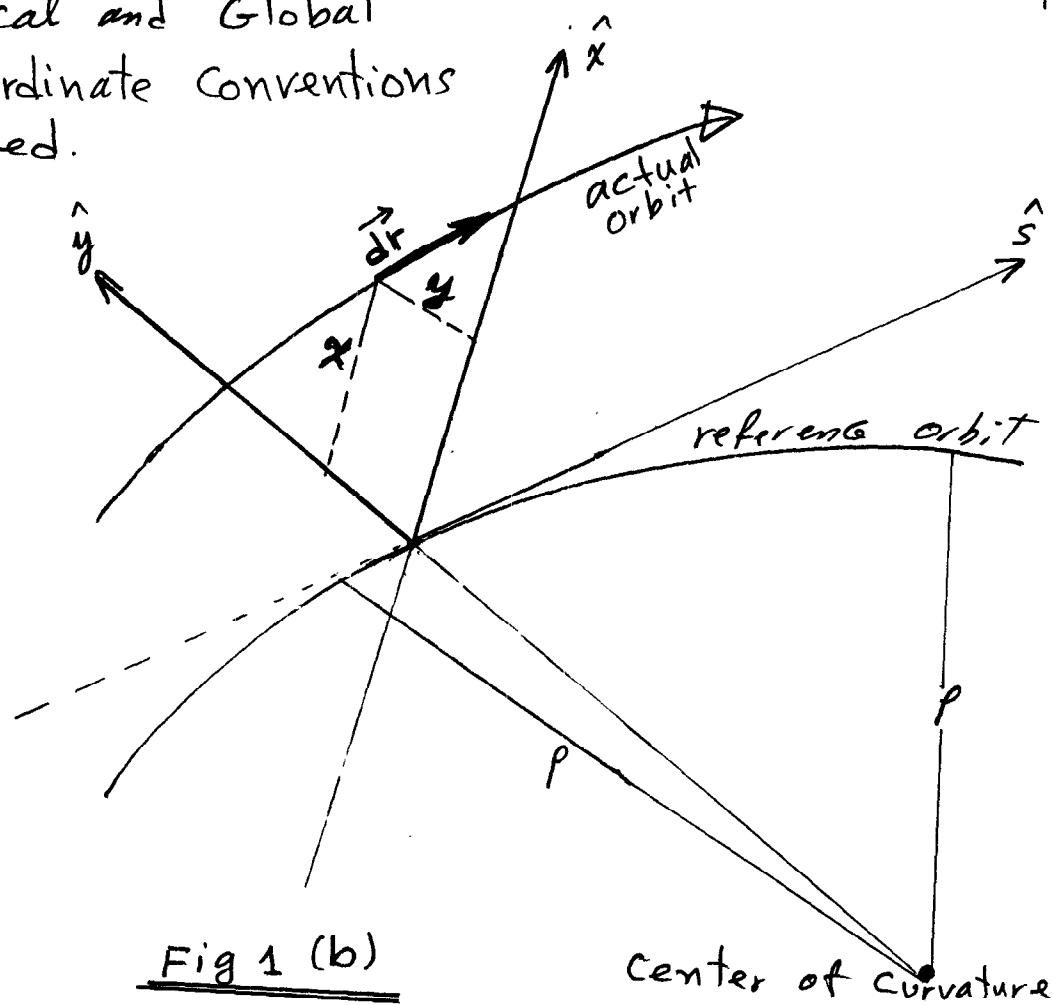


Fig 1 (b)

center of curvature

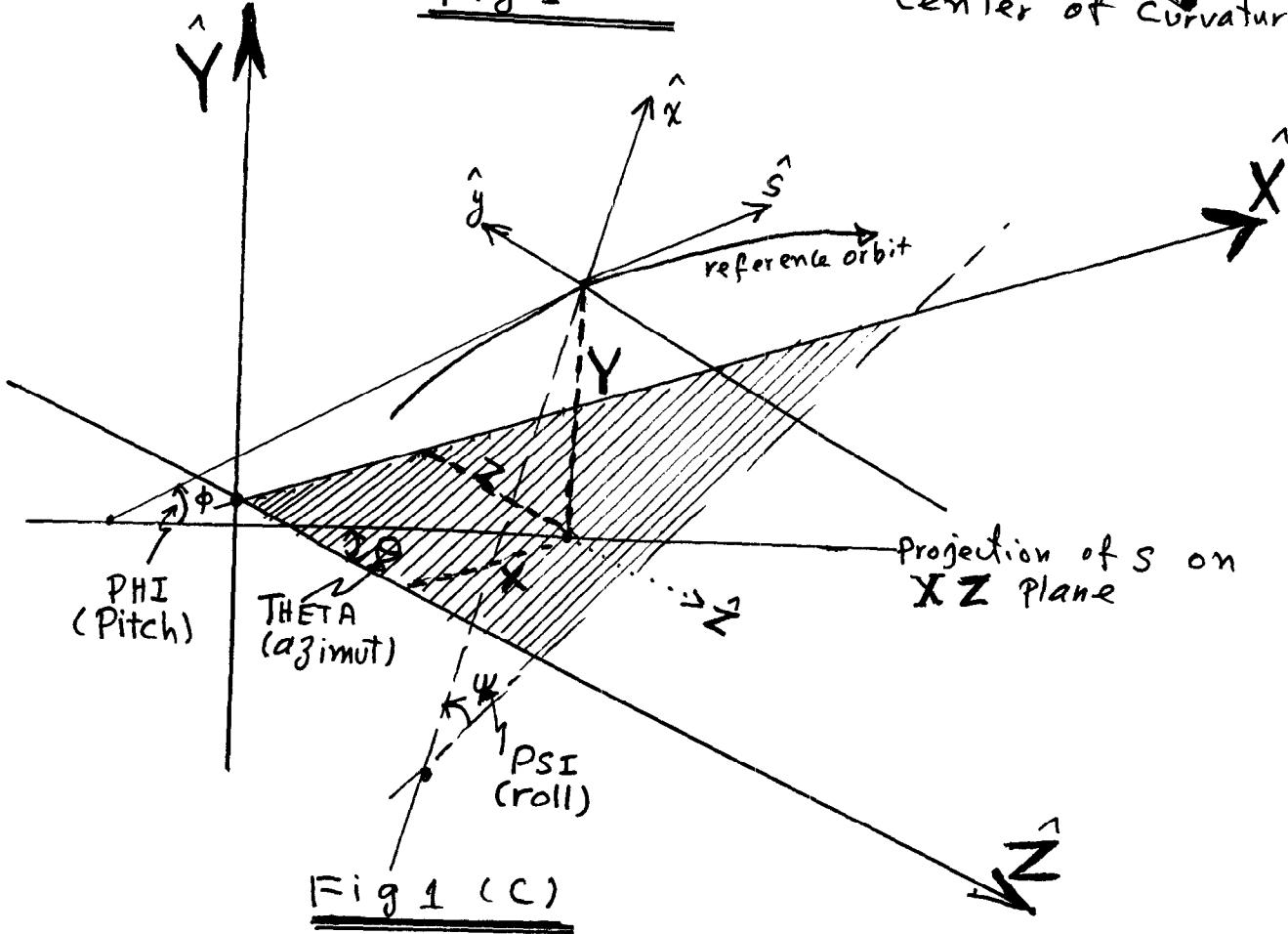


Fig 1 (c)

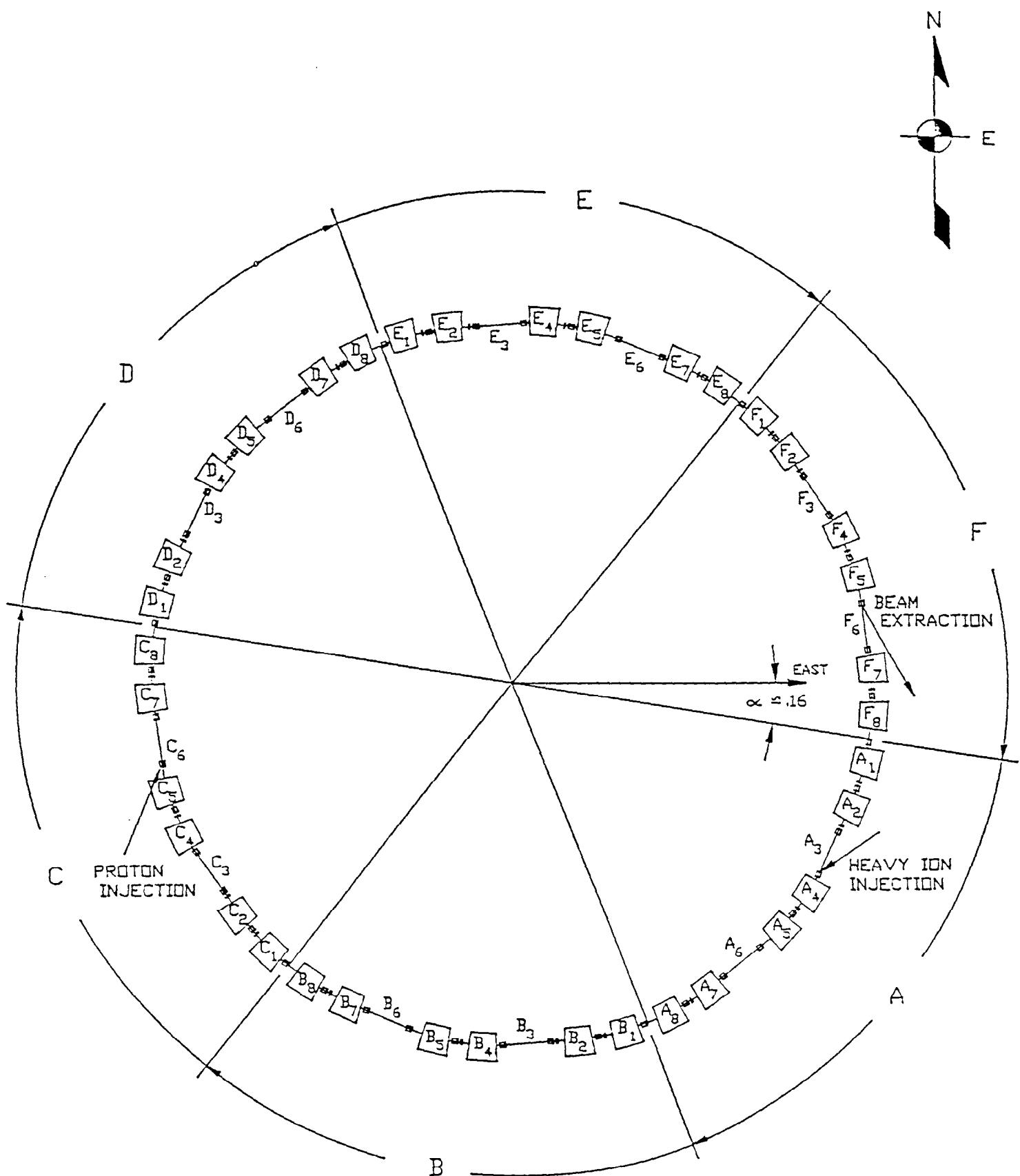


Fig. 2 Layout of the AGS Booster showing the relative position of magnets (e.g. Dipole Apex locations) and labeling convention of the Booster Superperiods. (A to F, with the Beam in the Clockwise direction).

TABLE I
DEFINITION AND MAGNITUDE OF THE ELEMENTS AND PARAMETERS

TABLE I

AGS BOOSTER LATTICE FOR SURVEY ZOHREH PARSA
INPUT STREAM TO PROGRAM MAD (SHOWING THE DEFINITION AND MAGNITUDE OF THE ELEMENTS AND
PARAMETER DEFINITIONS)

```

BR := 2.14962
TH := 1.174532925199
SF := 1.36066306
SD := -8.105988
SV := .11164764
GF := -558211184119
GD := -575416218362
LQ := .251875

DRIFT SPACES
S2H : DRIFT,L=.25
S1 : DRIFT,L=.1
S3 : DRIFT,L=.3
S3H : DRIFT,L=.35
S5H : DRIFT,L=.55
S10 : DRIFT,L=1.
S32H : DRIFT,L=3.25
S37 : DRIFT,L=3.7

```

BENDING MAGNET WITH EDDY CURRENT SEXTUPOLES

BEND : \$BEND,L=2.4,ANGLE=TH,K2=SV

QUADRUPOLES

```

QF : QUADRUPOLE,L=LQ,K1=GF
QD : QUADRUPOLE,L=LQ,K1=GD

```

SEXTUPOLES (CHROMATICITY CORRECTING AND EDDY CURRENT)

```

SXF : SEXTUPOLE,L=.1,K2=SF
SXD : SEXTUPOLE,L=.1,K2=SD

```

THE KICKERS

CT : DRIFT,L=.1

```

HCDF : LINE=(QD,S3,BEND,S5H,CT,SXF,S2H,QF)
HCFD : LINE=(QF,S3,BEND,S5H,CT,SXD,S2H,QD)
HCDFL : LINE=(QD,S3,BEND,S5H,CT,S3H,QF)
HCDFLM : LINE=(QD,S3,BEND,S10,QF)
HCFDL : LINE=(QF,S3,BEND,S5H,CT,S3H,QD)
HCFDLM : LINE=(QF,S3,BEND,S10,QD)
HCDFO : LINE=(QD,S32H,CT,S3H,QF)
HCFDO : LINE=(QF,S32H,CT,S3H,QD)
HCDFOM : LINE=(QD,S37,CT,S3H,QF)
HCFDOM : LINE=(QF,S37,QD)

```

SUPERPERIODS

```

B4SA : LINE=(HCDF,HCFD,HCDF0,HCFD,HCDFLM,HCFD0,HCDF,HCFDL)
B4SC : LINE=(HCDF,HCFD,HCDF0,HCFD,HCDFLM,HCFD0,HCDF,HCFDL)
B4SF : LINE=(HCDF,HCFD,HCFD0,HCFD,HCDFL,HCFD0,HCDF,HCFDL)
B4S : LINE=(HCDF,HCFD,HCDF0,HCFD,HCDFL,HCFD0,HCDF,HCFDL)

```

TABLE II

LATTICE PARAMETERS FOR $\Delta(P)/P = 0$

TABLE II

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
DELTA(P)/P = 0.000000

"MAD" VERSION: 6.01/03 RUN: 21-NOV-8 10:18:00

PAGE 1

ELEMENT SEQUENCE	HORIZONTAL			VERTICAL		
	DIST [M]	BETAX [M]	ALFAX [M]	MUX [CO]	PX(CO) [MM]	DX [MM]
BEGIN RING	1	0.0000	0.0000	0.0000	0.540-0.015	13.644
55 QD	9	33.882	3.642	0.814	0.546-0.064	13.157
56 S3	7	34.182	3.789	0.802	0.565-0.064	12.041
57 BEND	7	36.582	9.447	0.826	0.918	0.812
58 S5H	6	37.132	11.154	0.888	0.960	0.860
59 CT	8	37.232	11.486	0.897	1.045	0.229
60 SXF	3	37.332	11.825	0.898	1.068	0.229
61 S2H	5	37.582	12.700	0.900	1.090	0.229
62 QF	9	37.834	13.158	0.905	1.185	0.229
63 QF	10	38.086	12.705	0.906	1.180-0.102	3.853
64 S3	8	38.386	11.665	0.913	1.150-0.102	4.247
65 BEND	8	40.786	5.266	0.954	1.098	0.059
66 SSH	7	41.436	4.326	0.981	1.000	0.059
67 CT	9	41.436	4.178	0.984	1.136	0.059
68 SXD	3	41.536	4.038	0.988	1.142	0.059
69 S2H	6	41.786	3.720	0.592	1.157	0.059
70 QD	10	42.037	3.575	-0.011	1.193	0.229
71 QD	11	42.289	3.731	-0.615	1.021	0.229
72 S32H	3	45.539	11.627	-1.815	1.103	0.000
73 CT	10	45.639	11.993	-1.852	1.104	0.000
74 S3H	4	45.989	13.335	-1.981	1.108	0.000
75 QF	11	46.241	13.866	-0.102	1.111	0.000
76 QF	12	46.493	13.435	1.791	1.114	0.000
77 S3	9	46.793	12.389	1.697	1.118	0.000
78 BEND	9	49.193	5.820	1.012	1.163	0.000
79 S5H	8	49.743	4.812	0.821	1.180	0.000
80 CT	11	49.843	4.651	0.786	1.183	0.000
81 SXD	4	49.943	4.498	0.751	1.187	0.000
82 S2H	7	50.193	4.144	0.664	1.196	0.000
83 QD	12	50.445	3.976	0.008	1.206	0.000
84 QD	13	50.697	4.135	-0.646	1.216	0.000
85 S3	10	50.997	4.553	-0.749	1.227	0.000
86 BEND	10	53.397	9.894	-1.453	1.285	0.000
87 S5H	9	53.947	11.588	-1.627	1.293	0.000
88 CT	12	54.047	11.916	-1.658	1.294	0.000
89 S3H	5	54.397	13.115	-1.768	1.299	0.000
90 QF	13	54.649	13.546	0.079	1.302	0.000

TABLE II (CONTINUES)

"MAD" VERSION: 6.01/03 RUN: 21-NOV-8 10:18:00
 LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING", ZOHREN PARSA
 $\Delta(P)/P = 0.00000$

POS.	ELEMENT NO.	SEQUENCE NAME	DIST [M]	I [M]	HORIZONTAL [L]	MUX [L2P1]	X(CO) [MM]	PX(CO) [MM]	DX [MM]	DPX [MM]	I [1]	BETAY [M1]	ALFAY [L1]	MUY [L2P1]	Y(CO) [MM]	DY [MM]	DPY [MM]	VERTICAL [L1]
91	QF	14	54.901	13.038	1.915	1.305	0.000	0.000	2.894-0.435	3.853	-0.603	1.319	0.000	0.000	0.000	0.000	0.000	
92	S32H	4	58.151	4.371	0.752	1.376	0.000	0.000	1.481-0.435	11.508	-1.752	1.400	0.000	0.000	0.000	0.000	0.000	
93	CT	13	58.251	4.224	0.716	1.379	0.000	0.000	1.437-0.435	11.862	-1.788	1.401	0.000	0.000	0.000	0.000	0.000	
94	S3H	6	58.601	3.767	0.598	1.393	0.000	0.000	1.285-0.435	13.157	-1.912	1.406	0.000	0.000	0.000	0.000	0.000	
95	QD	14	58.852	3.624	-0.018	1.404	0.000	0.000	1.198-0.255	13.644	0.000	1.409	0.000	0.000	0.000	0.000	0.000	
96	QD	15	59.104	3.785	-0.628	1.415	0.000	0.000	1.156-0.085	13.157	1.912	1.412	0.000	0.000	0.000	0.000	0.000	
97	S3	11	59.404	4.195	-0.739	1.427	0.000	0.000	1.130-0.085	12.041	1.806	1.416	0.000	0.000	0.000	0.000	0.000	
98	BEND	11	61.804	9.644	-1.509	1.488	0.000	0.000	1.118-0.075	5.413	0.956	1.464	0.000	0.000	0.000	0.000	0.000	
99	S5H	10	62.354	11.407	-1.695	1.497	0.000	0.000	1.159-0.075	4.467	0.762	1.481	0.000	0.000	0.000	0.000	0.000	
100	CT	14	62.454	11.749	-1.729	1.498	0.000	0.000	1.167-0.075	4.319	0.727	1.485	0.000	0.000	0.000	0.000	0.000	
101	SXF	4	62.554	12.098	-1.763	1.499	0.000	0.000	1.175-0.075	4.177	0.691	1.489	0.000	0.000	0.000	0.000	0.000	
102	S2H	8	62.804	13.001	-1.848	1.503	0.000	0.000	1.193-0.075	3.853	0.603	1.499	0.000	0.000	0.000	0.000	0.000	
103	QF	15	63.056	13.477	-0.017	1.506	0.000	0.000	1.191-0.093	3.703	0.000	1.509	0.000	0.000	0.000	0.000	0.000	
104	QF	16	63.308	13.018	-1.816	1.509	0.000	0.000	1.47-0.258	3.853	-0.603	1.528	0.000	0.000	0.000	0.000	0.000	
105	S3	12	63.608	11.959	1.717	1.512	0.000	0.000	1.97-0.075	4.247	-0.709	1.532	0.000	0.000	0.000	0.000	0.000	
106	BEND	12	66.008	5.405	0.986	1.566	0.000	0.000	0.647-0.094	9.687	-1.558	1.593	0.000	0.000	0.000	0.000	0.000	
107	S5H	11	66.558	4.431	0.785	1.578	0.000	0.000	0.596-0.094	11.508	-1.752	1.601	0.000	0.000	0.000	0.000	0.000	
108	CT	15	66.658	4.278	0.749	1.582	0.000	0.000	0.586-0.094	11.862	-1.788	1.603	0.000	0.000	0.000	0.000	0.000	
109	S3H	7	67.008	3.798	0.621	1.596	0.000	0.000	0.554-0.094	13.157	-1.912	1.607	0.000	0.000	0.000	0.000	0.000	
110	QD	16	67.260	3.642	0.009	1.607	0.000	0.000	0.540-0.015	13.644	0.000	1.610	0.000	0.000	0.000	0.000	0.000	
END	RING	1	201.780	3.642	0.009	4.820	0.000	0.000	0.540-0.015	13.644	0.000	4.830	0.000	0.000	0.000	0.000	0.000	
TOTAL LENGTH =			201.780000	QX,	=	4.820000	QY,	=	4.829999				4.829999					
ALFA			0.419701E-01	BETAX(MAX)	=	0.001048	BETAY(MAX)	=	-0.001678				-0.001678					
GAMMA(CTR)	=		4.881238	DX(MAX)	=	13.865707	DY(MAX)	=	13.644032				13.644032					
XCO(MAX)	=			XCO(MAX)	=	2.951449	YCO(MAX)	=	0.000000				0.000000					
XCO(R.M.S.)	=			XCO(R.M.S.)	=	0.000000	YCO(R.M.S.)	=	0.000000				0.000000					

TABLE III

SURVEY OF THE AGS - BOOSTER

**AGS BOOSTER LATTICE FOR SURVEY
SURVEY OF BEAM LINE "RING",**
TABLE III GIVES THE SURVEY, WITH X0=31.86063, Z0=5.55399, THETA0=-.161765

"MAD" VERSION: 6.01/03 RUN: 21-NOV-8 10:18:00

PAGE 1**ZOHREH PARSA****TABLE III**

POS. NO.	ELEMENT NAME	SEQUENCE SUM(L)	ARC M	POSITIONS			Z M	I RAD	ANGLES RAD
				I M	X M	Y M			
BEGIN RING				0.0000000	31.860630	0.0000000	5.553990	-0.161765	0.0000000
1 QD	1	0.251875	0.251875	0.0000000	31.820063	0.0000000	0.0000000	-0.161765	0.0000000
2 S3	1	0.551875	0.551875	0.0000000	31.771745	0.0000000	6.098660	-0.161765	0.0000000
3 BEND	1	2.951875	2.951875	0.0000000	31.180978	0.0000000	8.421673	-0.336298	0.0000000
4 S5H	1	3.501875	3.501875	0.0000000	30.999481	0.0000000	8.940863	-0.336298	0.0000000
5 CT	1	3.601875	3.601875	0.0000000	30.966482	0.0000000	9.035262	-0.336298	0.0000000
6 SXF	1	3.791875	3.791875	0.0000000	30.933482	0.0000000	9.129660	-0.336298	0.0000000
7 S2H	1	3.951875	3.951875	0.0000000	30.850984	0.0000000	9.365656	-0.336298	0.0000000
8 QF	1	4.203750	4.203750	0.0000000	30.767866	0.0000000	9.603342	-0.336298	0.0000000
9 QF	2	4.455625	4.455625	0.0000000	30.684749	0.0000000	9.841187	-0.336298	0.0000000
10 S3	2	4.755625	4.755625	0.0000000	30.585750	0.0000000	10.124382	-0.336298	0.0000000
11 BEND	2	7.155625	7.155625	0.0000000	29.600572	0.0000000	12.309517	-0.510831	0.0000000
12 S5H	2	7.705625	7.705625	0.0000000	29.331676	0.0000000	12.789303	-0.510831	0.0000000
13 CT	2	7.805625	7.805625	0.0000000	29.282786	0.0000000	12.876537	-0.510831	0.0000000
14 SXD	1	7.905625	7.905625	0.0000000	29.233895	0.0000000	12.963771	-0.510831	0.0000000
15 S2H	2	8.155625	8.155625	0.0000000	29.111670	0.0000000	13.181856	-0.510831	0.0000000
16 QD	2	8.407500	8.407500	0.0000000	28.988528	0.0000000	13.401576	-0.510831	0.0000000
17 QD	3	8.659375	8.659375	0.0000000	28.865585	0.0000000	13.621296	-0.510831	0.0000000
18 S32H	1	11.909375	11.909375	0.0000000	27.276453	0.0000000	16.456397	-0.510831	0.0000000
19 CT	3	12.009375	12.009375	0.0000000	27.227563	0.0000000	16.543631	-0.510831	0.0000000
20 S3H	1	12.359375	12.359375	0.0000000	27.055644	0.0000000	16.848949	-0.510831	0.0000000
21 QF	3	12.611250	12.611250	0.0000000	26.933305	0.0000000	17.068669	-0.510831	0.0000000
22 QF	4	12.863125	12.863125	0.0000000	26.810163	0.0000000	17.288396	-0.510831	0.0000000
23 S3	3	13.163125	13.163125	0.0000000	26.663492	0.0000000	17.550991	-0.510831	0.0000000
24 BEND	3	15.563125	15.563125	0.0000000	25.313836	0.0000000	19.530955	-0.685364	0.0000000
25 S5H	3	16.113125	16.113125	0.0000000	24.965711	0.0000000	19.956759	-0.685364	0.0000000
26 CT	4	16.213125	16.213125	0.0000000	24.902415	0.0000000	20.034178	-0.685364	0.0000000
27 SXD	2	16.313125	16.313125	0.0000000	24.839120	0.0000000	20.11197	-0.685364	0.0000000
28 S2H	3	16.563125	16.563125	0.0000000	24.680881	0.0000000	20.305144	-0.685364	0.0000000
29 QD	4	16.815000	16.815000	0.0000000	24.521456	0.0000000	20.500143	-0.685364	0.0000000
30 QD	5	17.066875	17.066875	0.0000000	24.362030	0.0000000	20.695142	-0.685364	0.0000000
31 S3	4	17.366875	17.366875	0.0000000	24.172144	0.0000000	20.927398	-0.685364	0.0000000
32 BEND	4	19.766875	19.766875	0.0000000	22.499019	0.0000000	22.643803	-0.859897	0.0000000
33 S1g	1	20.766875	20.766875	0.0000000	21.741244	0.0000000	22.296319	-0.859897	0.0000000
34 QF	5	21.018750	21.018750	0.0000000	21.550379	0.0000000	23.460671	-0.859897	0.0000000
35 QF	6	21.270625	21.270625	0.0000000	21.359514	0.0000000	23.625024	-0.859897	0.0000000
36 S32H	2	24.520625	24.520625	0.0000000	24.896745	0.0000000	25.745700	-0.859897	0.0000000

TABLE III (CONTINUES)

AGS BOOSTER LATTICE FOR SURVEY,
SURVEY OF BEAM LINE "RING",
A ZOHREH PARSA

"MAD" VERSION: 6.01/03 RUN: 21-NOV-8 10:18:00
PAGE 2 P

POS. NO.	ELEMENT NAME	SEQUENCE SUM(L)	C E ARC M	I 1	X M	Y M	Z M	POSITIONS			I 1	THETA RAD	ANGLES RAD	PSI RAD
								I 1	I 1	I 1				
37	CT	5	24.620625	24.620625	18.820968	0.000000	25.810951	-0.859897	0.000000	0.000000	-0.859897	0.000000	0.000000	
38	S3H	2	24.970625	24.970625	18.555746	0.000000	26.639332	-0.859897	0.000000	0.000000	-0.859897	0.000000	0.000000	
39	QD	6	25.222500	25.222500	18.364882	0.000000	26.203684	-0.859897	0.000000	0.000000	-0.859897	0.000000	0.000000	
40	QD	7	25.474375	25.474375	18.174017	0.000000	26.368037	-0.859897	0.000000	0.000000	-0.859897	0.000000	0.000000	
41	S3	5	25.774375	25.774375	17.946685	0.000000	26.563791	-0.859897	0.000000	0.000000	-0.859897	0.000000	0.000000	
42	BEND	5	28.174375	28.174375	16.000927	0.000000	27.563585	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	
43	S5H	4	28.724375	28.724375	15.528163	0.000000	28.244644	-1.034430	0.000000	0.000000	-1.034430	0.000000	0.000000	
44	CT	6	28.824375	28.824375	15.442006	0.000000	28.295746	-1.034430	0.000000	0.000000	-1.034430	0.000000	0.000000	
45	SXF	2	28.924375	28.924375	15.356249	0.000000	28.346847	-1.034430	0.000000	0.000000	-1.034430	0.000000	0.000000	
46	S2H	4	29.174375	29.174375	15.141356	0.000000	28.474601	-1.034430	0.000000	0.000000	-1.034430	0.000000	0.000000	
47	QF	7	29.426250	29.426250	14.924852	0.000000	28.603314	-1.034430	0.000000	0.000000	-1.034430	0.000000	0.000000	
48	QF	8	29.678125	29.678125	14.708347	0.000000	28.732026	-1.034430	0.000000	0.000000	-1.034430	0.000000	0.000000	
49	S3	6	29.978125	29.978125	14.450476	0.000000	28.885331	-1.034430	0.000000	0.000000	-1.034430	0.000000	0.000000	
50	BEND	6	32.378125	32.378125	12.291208	0.000000	29.925981	-1.208963	0.000000	0.000000	-1.208963	0.000000	0.000000	
51	S5H	5	32.928125	32.928125	11.776821	0.000000	30.120676	-1.208963	0.000000	0.000000	-1.208963	0.000000	0.000000	
52	CT	7	33.028125	33.028125	11.683296	0.000000	30.156075	-1.208963	0.000000	0.000000	-1.208963	0.000000	0.000000	
53	S3H	3	33.378125	33.378125	11.355958	0.000000	30.279971	-1.208963	0.000000	0.000000	-1.208963	0.000000	0.000000	
54	QD	8	33.630000	33.630000	11.120393	0.000000	30.369132	-1.208963	0.000000	0.000000	-1.208963	0.000000	0.000000	
55	QD	9	33.881875	33.881875	10.884827	0.000000	30.458293	-1.208963	0.000000	0.000000	-1.208963	0.000000	0.000000	
56	S3	7	34.181875	34.181875	10.604252	0.000000	30.564490	-1.208963	0.000000	0.000000	-1.208963	0.000000	0.000000	
57	BEND	7	36.581875	36.581875	8.297081	0.000000	31.214378	-1.383495	0.000000	0.000000	-1.383495	0.000000	0.000000	
58	S5H	6	37.131875	37.131875	7.756700	0.000000	31.316792	-1.383495	0.000000	0.000000	-1.383495	0.000000	0.000000	
59	CT	8	37.231875	37.231875	7.658449	0.000000	31.335413	-1.383495	0.000000	0.000000	-1.383495	0.000000	0.000000	
60	SXF	3	37.331875	37.331875	7.560198	0.000000	31.354034	-1.383495	0.000000	0.000000	-1.383495	0.000000	0.000000	
61	S2H	5	37.581875	37.581875	7.314570	0.000000	31.400586	-1.383495	0.000000	0.000000	-1.383495	0.000000	0.000000	
62	QF	9	37.833750	37.833750	7.067100	0.000000	31.447487	-1.383495	0.000000	0.000000	-1.383495	0.000000	0.000000	
63	QF	10	38.085625	38.085625	6.819631	0.000000	31.494388	-1.383495	0.000000	0.000000	-1.383495	0.000000	0.000000	
64	S3	8	38.385625	38.385625	6.524877	0.000000	31.550250	-1.383495	0.000000	0.000000	-1.383495	0.000000	0.000000	
65	BEND	8	40.785625	40.785625	4.139005	0.000000	31.789628	-1.558028	0.000000	0.000000	-1.558028	0.000000	0.000000	
66	S5H	7	41.335625	41.335625	3.589950	0.000000	31.796650	-1.558028	0.000000	0.000000	-1.558028	0.000000	0.000000	
67	CT	9	41.435625	41.435625	3.489958	0.000000	31.797927	-1.558028	0.000000	0.000000	-1.558028	0.000000	0.000000	
68	SXD	3	41.535625	41.535625	3.389967	0.000000	31.799204	-1.558028	0.000000	0.000000	-1.558028	0.000000	0.000000	
69	S2H	6	41.785625	41.785625	3.139987	0.000000	31.802396	-1.558028	0.000000	0.000000	-1.558028	0.000000	0.000000	
70	QD	10	42.037500	42.037500	2.888132	0.000000	31.805612	-1.558028	0.000000	0.000000	-1.558028	0.000000	0.000000	
71	QD	11	42.289375	42.289375	2.636278	0.000000	31.808827	-1.558028	0.000000	0.000000	-1.558028	0.000000	0.000000	
72	S32H	3	45.539375	45.539375	0.613457	0.000000	31.850322	-1.558028	0.000000	0.000000	-1.558028	0.000000	0.000000	
73	CT	10	45.639375	45.639375	-0.713449	0.000000	31.851599	-1.558028	0.000000	0.000000	-1.558028	0.000000	0.000000	

TABLE III (CONTINUES)

AGS BOOSTER LATTICE FOR SURVEY
SURVEY OF BEAM LINE "RING",
ZOHREH PARSA"MAD" VERSION: 6.01/03 RUN: 21-NOV-8 10:18:00
PAGE 3

POS. NO.	ELEMENT NAME NO.	SEQUENCE			POSSITIONS			ANGLES		
		SUM(L) M	ARC M	X M	Y M	Z M	I RAD	PHI RAD	PSI RAD	
74	S3H	4	45.989375	45.989375	-1.063420	0.000000	31.856067	-1.558028	0.000000	
75	QF	11	46.241250	46.241250	-1.315275	0.000000	31.856283	-1.558028	0.000000	
76	QF	12	46.493125	46.493125	-1.567129	0.000000	31.862499	-1.558028	0.000000	
77	S3	9	46.793125	46.793125	-1.867105	0.000000	31.866329	-1.558028	0.000000	
78	BEND	9	49.193125	49.193125	-4.257411	0.000000	31.687925	-1.732561	0.000000	
79	S5H	8	49.743125	49.743125	-4.800231	0.000000	31.599342	-1.732561	0.000000	
80	CT	11	49.843125	49.843125	-4.898925	0.000000	31.583236	-1.732561	0.000000	
81	SXD	4	49.943125	49.943125	-4.997620	0.000000	31.567130	-1.732561	0.000000	
82	S2H	7	50.193125	50.193125	-5.244356	0.000000	31.526864	-1.732561	0.000000	
83	QD	12	50.445000	50.445000	-5.492943	0.000000	31.486297	-1.732561	0.000000	
84	QD	13	50.696875	50.696875	-5.741529	0.000000	31.445730	-1.732561	0.000000	
85	S3	10	50.996875	50.996875	-6.307613	0.000000	31.397412	-1.732561	0.000000	
86	BEND	10	53.396875	53.396875	-8.360625	0.000000	30.806646	-1.907094	0.000000	
87	S5H	9	53.946875	53.946875	-8.879816	0.000000	30.625149	-1.907094	0.000000	
88	CT	12	54.046875	54.046875	-8.974214	0.000000	30.592149	-1.907094	0.000000	
89	S3H	5	54.396875	54.396875	-9.304608	0.000000	30.476651	-1.907094	0.000000	
90	QF	13	54.648750	54.648750	-9.542374	0.000000	30.399334	-1.907094	0.000000	
91	QF	14	54.900625	54.900625	-9.780139	0.000000	30.310416	-1.907094	0.000000	
92	S32H	4	58.150625	58.150625	-12.848084	0.000000	29.237933	-1.907094	0.000000	
93	CT	13	58.250625	58.250625	-12.942482	0.000000	29.204934	-1.907094	0.000000	
94	S3H	6	58.680625	58.680625	-13.272876	0.000000	29.089436	-1.907094	0.000000	
95	QD	14	58.852500	58.852500	-13.510641	0.000000	29.006318	-1.907094	0.000000	
96	QD	15	59.104375	59.104375	-13.748407	0.000000	28.923201	-1.907094	0.000000	
97	S3	11	59.404375	59.404375	-14.031602	0.000000	28.824202	-1.907094	0.000000	
98	BEND	11	61.804375	61.804375	-16.216737	0.000000	27.839024	-2.081627	0.000000	
99	S5H	10	62.354375	62.354375	-16.696524	0.000000	27.570128	-2.081627	0.000000	
100	CT	14	62.454375	62.454375	-16.783757	0.000000	27.521238	-2.081627	0.000000	
101	SXF	4	62.554375	62.554375	-16.870991	0.000000	27.472348	-2.081627	0.000000	
102	S2H	8	62.804375	62.804375	-17.089076	0.000000	27.350122	-2.081627	0.000000	
103	QF	15	63.056250	63.056250	-17.308796	0.000000	27.226980	-2.081627	0.000000	
104	QF	16	63.308125	63.308125	-17.528517	0.000000	27.103838	-2.081627	0.000000	
105	S3	12	63.608125	63.608125	-17.790218	0.000000	26.957167	-2.081627	0.000000	
106	BEND	12	66.008125	66.008125	-19.771082	0.000000	25.607511	-2.256160	0.000000	
107	S5H	11	66.558125	66.558125	-20.196886	0.000000	25.259386	-2.256160	0.000000	
108	CT	15	66.658125	66.658125	-20.274305	0.000000	25.196090	-2.256160	0.000000	
109	S3H	7	67.008125	67.008125	-20.545271	0.000000	24.974556	-2.256160	0.000000	
110	QD	16	67.260000	67.260000	-20.740270	0.000000	24.815131	-2.256160	0.000000	

AGS BOOSTER LATTICE FOR SURVEY
 SURVEY OF BEAM LINE "RING",
 ZOHREH PARSA

TABLE III (CONT'UES)

 "MAD" VERSION: 6.01/03 RUN: 21-NOV-8 10:18:00
 PAGE 4

POS. NO.	ELEMENT NAME	ELEMENT OCC. NO.	SEQUENCE SUM(L)			POSITIONS			ANGLES		
			M	ARC M	I	X M	Y M	Z M	THETA RAD	PHI RAD	PSI RAD
111	QD	17	67.511875	67.511875	-20.935268	0.000000	24.655705	-2.256160	0.000000	0.000000	0.000000
112	S3	13	67.811875	67.811875	-21.167525	0.000000	24.465819	-2.256160	0.000000	0.000000	0.000000
113	BEND	13	70.211875	70.211875	-22.883930	0.000000	22.792694	-2.430693	0.000000	0.000000	0.000000
114	S5H	12	70.761875	70.761875	-23.242814	0.000000	22.375917	-2.430693	0.000000	0.000000	0.000000
115	CT	16	70.861875	70.861875	-23.308065	0.000000	22.300140	-2.430693	0.000000	0.000000	0.000000
116	SXF	5	70.961875	70.961875	-23.373317	0.000000	22.224362	-2.430693	0.000000	0.000000	0.000000
117	S2H	9	71.211875	71.211875	-23.536446	0.000000	22.034919	-2.430693	0.000000	0.000000	0.000000
118	QF	17	71.463750	71.463750	-23.700798	0.000000	21.844054	-2.430693	0.000000	0.000000	0.000000
119	QF	18	71.715625	71.715625	-23.865150	0.000000	21.653189	-2.430693	0.000000	0.000000	0.000000
120	S3	14	72.015625	72.015625	-24.060905	0.000000	21.425857	-2.430693	0.000000	0.000000	0.000000
121	BEND	14	74.415625	74.415625	-25.460699	0.000000	19.480100	-2.605226	0.000000	0.000000	0.000000
122	S5H	13	74.965625	74.965625	-25.741758	0.000000	19.007335	-2.605226	0.000000	0.000000	0.000000
123	CT	17	75.065625	75.065625	-25.792859	0.000000	18.921378	-2.605226	0.000000	0.000000	0.000000
124	SXD	5	75.165625	75.165625	-25.843961	0.000000	18.835421	-2.605226	0.000000	0.000000	0.000000
125	S2H	10	75.415625	75.415625	-25.971715	0.000000	18.620529	-2.605226	0.000000	0.000000	0.000000
126	QD	18	75.667500	75.667500	-26.04427	0.000000	18.404024	-2.605226	0.000000	0.000000	0.000000
127	QD	19	75.919375	75.919375	-26.229140	0.000000	18.187520	-2.605226	0.000000	0.000000	0.000000
128	S32H	5	79.169375	79.169375	-27.889943	0.000000	15.393914	-2.605226	0.000000	0.000000	0.000000
129	CT	18	79.269375	79.269375	-27.941044	0.000000	15.307957	-2.605226	0.000000	0.000000	0.000000
130	S3H	8	79.619375	79.619375	-28.119000	0.000000	15.007107	-2.605226	0.000000	0.000000	0.000000
131	QF	19	79.871250	79.871250	-28.248612	0.000000	14.790602	-2.605226	0.000000	0.000000	0.000000
132	QF	20	80.123125	80.123125	-28.373234	0.000000	14.574098	-2.605226	0.000000	0.000000	0.000000
133	S3	15	80.423125	80.423125	-28.530629	0.000000	14.316227	-2.605226	0.000000	0.000000	0.000000
134	BEND	15	82.823125	82.823125	-29.571280	0.000000	12.156958	-2.779759	0.000000	0.000000	0.000000
135	S5H	14	83.373125	83.373125	-29.765974	0.000000	11.642571	-2.779759	0.000000	0.000000	0.000000
136	CT	19	83.473125	83.473125	-29.801373	0.000000	11.549046	-2.779759	0.000000	0.000000	0.000000
137	SXD	6	83.573125	83.573125	-29.836772	0.000000	11.455051	-2.779759	0.000000	0.000000	0.000000
138	S2H	11	83.823125	83.823125	-29.925269	0.000000	11.221709	-2.779759	0.000000	0.000000	0.000000
139	QD	20	84.075000	84.075000	-30.014431	0.000000	10.986143	-2.779759	0.000000	0.000000	0.000000
140	QD	21	84.326875	84.326875	-30.103592	0.000000	10.750577	-2.779759	0.000000	0.000000	0.000000
141	S3	16	84.626875	84.626875	-30.209789	0.000000	10.470002	-2.779759	0.000000	0.000000	0.000000
142	BEND	16	87.026875	87.026875	-30.859676	0.000000	8.162831	-2.954292	0.000000	0.000000	0.000000
143	S10	2	88.026875	88.026875	-31.045884	0.000000	7.180321	-2.954292	0.000000	0.000000	0.000000
144	QF	21	88.278750	88.278750	-31.092785	0.000000	6.932851	-2.954292	0.000000	0.000000	0.000000
145	QF	22	88.530625	88.530625	-31.139686	0.000000	6.685381	-2.954292	0.000000	0.000000	0.000000
146	S32H	6	91.780625	91.780625	-31.744861	0.000000	3.492222	-2.954292	0.000000	0.000000	0.000000
147	CT	20	91.880625	91.880625	-31.763482	0.000000	3.393971	-2.954292	0.000000	0.000000	0.000000

TABLE III (CONTINUES)

AGS BOOSTER LATTICE FOR SURVEY
SURVEY OF BEAM LINE "RING",
ZOHREH PARSA"MAD" VERSION: 6.01/03 RUN: 21-NOV-8 10:18:00
PAGE 5

POS. NO.	ELEMENT NAME NO.	SEQUENCE			POSITIONS			ANGLES		
		SUM(L)	ARC	M	X	Y	Z	THETA RAD	PHI RAD	PSI RAD
148 S3H	9	92.230625	-31.828654	0.000000	3.050093	-2.954292	0.000000	0.000000	0.000000	0.000000
149 QD	22	92.482500	-31.875555	0.000000	2.000000	-2.954292	0.000000	0.000000	0.000000	0.000000
150 QD	23	92.734375	-31.922456	0.000000	2.555153	-2.954292	0.000000	0.000000	0.000000	0.000000
151 S3	17	93.0343375	-31.978319	0.000000	2.260400	-2.954292	0.000000	0.000000	0.000000	0.000000
152 BEND	17	95.434375	-32.217697	0.000000	-0.124572	-3.128825	0.000000	0.000000	0.000000	0.000000
153 S5H	15	95.984375	-32.224719	0.000000	-0.674527	-3.128825	0.000000	0.000000	0.000000	0.000000
154 CT	21	96.084375	-32.225996	0.000000	-0.745119	-3.128825	0.000000	0.000000	0.000000	0.000000
155 SXF	6	96.184375	-32.227273	0.000000	-0.874511	-3.128825	0.000000	0.000000	0.000000	0.000000
156 S2H	12	96.434375	-32.230465	0.000000	-1.124491	-3.128825	0.000000	0.000000	0.000000	0.000000
157 QF	23	96.686250	-32.233680	0.000000	-1.376345	-3.128825	0.000000	0.000000	0.000000	0.000000
158 QF	24	96.938125	-32.236896	0.000000	-1.628200	-3.128825	0.000000	0.000000	0.000000	0.000000
159 S3	18	97.238125	-32.240726	0.000000	-1.928175	-3.128825	0.000000	0.000000	0.000000	0.000000
160 BEND	18	99.638125	-32.062322	0.000000	-4.318482	-3.303358	0.000000	0.000000	0.000000	0.000000
161 S10	3	100.638125	-31.901262	0.000000	-5.305426	-3.303358	0.000000	0.000000	0.000000	0.000000
162 QD	24	100.890000	-31.860694	0.000000	-5.554013	-3.303358	0.000000	0.000000	0.000000	0.000000
163 QD	25	101.141875	-31.820127	0.000000	-5.892600	-3.303358	0.000000	0.000000	0.000000	0.000000
164 S3	19	101.441875	-31.771809	0.000000	-6.0986683	-3.303358	0.000000	0.000000	0.000000	0.000000
165 BEND	19	103.841875	-31.181043	0.000000	-8.421696	-3.477891	0.000000	0.000000	0.000000	0.000000
166 S5H	16	104.391875	-30.99546	0.000000	-8.940886	-3.477891	0.000000	0.000000	0.000000	0.000000
167 CT	22	104.491875	-30.966546	0.000000	-9.035284	-3.477891	0.000000	0.000000	0.000000	0.000000
168 SXF	7	104.591875	-30.933547	0.000000	-9.129683	-3.477891	0.000000	0.000000	0.000000	0.000000
169 S2H	13	104.841875	-30.851048	0.000000	-9.365678	-3.477891	0.000000	0.000000	0.000000	0.000000
170 QF	25	105.093750	-30.767931	0.000000	-9.603444	-3.477891	0.000000	0.000000	0.000000	0.000000
171 QF	26	105.345625	-30.684813	0.000000	-9.841210	-3.477891	0.000000	0.000000	0.000000	0.000000
172 S3	20	105.645625	-30.585815	0.000000	-10.124405	-3.477891	0.000000	0.000000	0.000000	0.000000
173 BEND	20	108.045625	-29.606336	0.000000	-12.309540	-3.652424	0.000000	0.000000	0.000000	0.000000
174 S5H	17	108.595625	-29.331740	0.000000	-12.789326	-3.652424	0.000000	0.000000	0.000000	0.000000
175 CT	23	108.695625	-29.282850	0.000000	-12.876560	-3.652424	0.000000	0.000000	0.000000	0.000000
176 SXD	7	108.795625	-29.233960	0.000000	-12.963794	-3.652424	0.000000	0.000000	0.000000	0.000000
177 S2H	14	109.045625	-29.111734	0.000000	-13.181879	-3.652424	0.000000	0.000000	0.000000	0.000000
178 QD	26	109.297500	-28.98592	0.000000	-13.401599	-3.652424	0.000000	0.000000	0.000000	0.000000
179 QD	27	109.549375	-28.865450	0.000000	-13.621319	-3.652424	0.000000	0.000000	0.000000	0.000000
180 S32H	7	112.799375	-27.276518	0.000000	-16.456420	-3.652424	0.000000	0.000000	0.000000	0.000000
181 CT	24	112.899375	-27.227627	0.000000	-16.543654	-3.652424	0.000000	0.000000	0.000000	0.000000
182 S3H	10	113.249375	-27.056512	0.000000	-16.848972	-3.652424	0.000000	0.000000	0.000000	0.000000
183 QF	27	113.501250	-26.933369	0.000000	-17.068692	-3.652424	0.000000	0.000000	0.000000	0.000000

TABLE III (CONTINUES)

AGS BOOSTER LATTICE FOR SURVEY
SURVEY OF BEAM LINE "RING".

ZOHREH PARSA

"MAD" VERSION: 6.01/03 RUN: 21-NOV-8 10:18:00
PAGE 6

POS. NO.	ELEMENT NAME	SEQUENCE SUM(L)	ARC M	POSITIONS			1 Z M	1 Y M	1 X M	ANGLES		
				1	1	1				1 RAD	1 RAD	1 RAD
184 QF	28	113.753125	113.753125	-26.810227	0.000000	0.000000	-17.288413	-3.652424	0.000000	0.000000	0.000000	0.000000
185 S3	21	114.053125	114.053125	-26.663557	0.000000	0.000000	-17.550114	-3.652424	0.000000	0.000000	0.000000	0.000000
186 BEND		116.453125	116.453125	-25.313900	0.000000	0.000000	-19.530978	-3.826956	0.000000	0.000000	0.000000	0.000000
187 S5H	18	117.003125	117.003125	-24.956775	0.000000	0.000000	-19.956782	-3.826956	0.000000	0.000000	0.000000	0.000000
188 CT	25	117.103125	117.103125	-24.902480	0.000000	0.000000	-20.034201	-3.826956	0.000000	0.000000	0.000000	0.000000
189 SXD	8	117.203125	117.203125	-24.83184	0.000000	0.000000	-20.111620	-3.826956	0.000000	0.000000	0.000000	0.000000
190 S2H	15	117.453125	117.453125	-24.680946	0.000000	0.000000	-20.305167	-3.826956	0.000000	0.000000	0.000000	0.000000
191 QD	28	117.705000	117.705000	-24.521520	0.000000	0.000000	-20.500166	-3.826956	0.000000	0.000000	0.000000	0.000000
192 QD	29	117.956875	117.956875	-24.362095	0.000000	0.000000	-20.695165	-3.826956	0.000000	0.000000	0.000000	0.000000
193 S3	22	118.256875	118.256875	-24.172208	0.000000	0.000000	-20.927421	-3.826956	0.000000	0.000000	0.000000	0.000000
194 BEND	22	120.656875	120.656875	-22.49083	0.000000	0.000000	-22.643826	-4.001489	0.000000	0.000000	0.000000	0.000000
195 S5H	19	121.206875	121.206875	-22.082307	0.000000	0.000000	-23.002710	-4.001489	0.000000	0.000000	0.000000	0.000000
196 CT	19	121.306875	121.306875	-22.006529	0.000000	0.000000	-23.067961	-4.001489	0.000000	0.000000	0.000000	0.000000
197 S3H	11	121.656875	121.656875	-21.741308	0.000000	0.000000	-23.296342	-4.001489	0.000000	0.000000	0.000000	0.000000
198 QF	29	121.908750	121.908750	-21.554444	0.000000	0.000000	-23.460694	-4.001489	0.000000	0.000000	0.000000	0.000000
199 QF	30	122.160625	122.160625	-21.359579	0.000000	0.000000	-23.625047	-4.001489	0.000000	0.000000	0.000000	0.000000
200 S32H	8	125.410625	125.410625	-18.896810	0.000000	0.000000	-25.745723	-4.001489	0.000000	0.000000	0.000000	0.000000
201 CT	27	125.510625	125.510625	-18.821032	0.000000	0.000000	-25.810974	-4.001489	0.000000	0.000000	0.000000	0.000000
202 S3H	12	125.860625	125.860625	-18.555811	0.000000	0.000000	-26.039355	-4.001489	0.000000	0.000000	0.000000	0.000000
203 QD	30	126.112500	126.112500	-18.364946	0.000000	0.000000	-26.203707	-4.001489	0.000000	0.000000	0.000000	0.000000
204 QD	31	126.364375	126.364375	-18.174082	0.000000	0.000000	-26.368600	-4.001489	0.000000	0.000000	0.000000	0.000000
205 S3	23	126.664375	126.664375	-17.946749	0.000000	0.000000	-26.563814	-4.001489	0.000000	0.000000	0.000000	0.000000
206 BEND	23	129.064375	129.064375	-16.000992	0.000000	0.000000	-27.963608	-4.176022	0.000000	0.000000	0.000000	0.000000
207 S5H	20	129.614375	129.614375	-15.528228	0.000000	0.000000	-28.244667	-4.176022	0.000000	0.000000	0.000000	0.000000
208 CT	28	129.714375	129.714375	-15.442271	0.000000	0.000000	-28.295769	-4.176022	0.000000	0.000000	0.000000	0.000000
209 SXF	8	129.814375	129.814375	-15.356314	0.000000	0.000000	-28.346870	-4.176022	0.000000	0.000000	0.000000	0.000000
210 S2H	16	130.064375	130.064375	-15.141421	0.000000	0.000000	-28.474624	-4.176022	0.000000	0.000000	0.000000	0.000000
211 QF	31	130.316250	130.316250	-14.924916	0.000000	0.000000	-28.603336	-4.176022	0.000000	0.000000	0.000000	0.000000
212 QF	32	130.568125	130.568125	-14.708412	0.000000	0.000000	-28.732049	-4.176022	0.000000	0.000000	0.000000	0.000000
213 S3	24	130.868125	130.868125	-14.450541	0.000000	0.000000	-28.885354	-4.176022	0.000000	0.000000	0.000000	0.000000
214 BEND	24	133.268125	133.268125	-12.291272	0.000000	0.000000	-29.926004	-4.350555	0.000000	0.000000	0.000000	0.000000
215 S5H	21	133.818125	133.818125	-11.776885	0.000000	0.000000	-30.120698	-4.350555	0.000000	0.000000	0.000000	0.000000
216 CT	29	133.918125	133.918125	-11.683360	0.000000	0.000000	-30.156097	-4.350555	0.000000	0.000000	0.000000	0.000000
217 S3H	13	134.268125	134.268125	-11.356023	0.000000	0.000000	-30.279994	-4.350555	0.000000	0.000000	0.000000	0.000000
218 QD	32	134.520000	134.520000	-11.120457	0.000000	0.000000	-30.369155	-4.350555	0.000000	0.000000	0.000000	0.000000
219 QD	33	134.771875	134.771875	-10.884891	0.000000	0.000000	-30.458316	-4.350555	0.000000	0.000000	0.000000	0.000000

TABLE III (CONTINUES)

AGS BOOSTER LATTICE FOR SURVEY
SURVEY OF BEAM LINE "RING".

"MAD" VERSION: 6.01/03 RUN: 21-NOV-8 10:18:00 PAGE 7

ELEMENT OCC. POS. NO.	ELEMENT NAME	SEQUENCE SUM(L)	ARC M	POSITIONS			ANGLE RAD	PSI RAD
				X M	Y M	Z M		
220 S3	25	135.071875	135.071875	-10.604316	0.000000	-30.564513	-4.350555	0.000000
221 BEND	25	137.471875	137.471875	-8.297145	0.000000	-31.214401	-4.520888	0.000000
222 S5H	22	138.021875	138.021875	-7.756764	0.000000	-31.316815	-4.520888	0.000000
223 CT	30	138.121875	138.121875	-7.658513	0.000000	-31.335436	-4.520888	0.000000
224 SXF	9	138.221875	138.221875	-7.560262	0.000000	-31.354056	-4.520888	0.000000
225 S2H	17	138.471875	138.471875	-7.314635	0.000000	-31.400608	-4.520888	0.000000
226 QF	33	138.723750	138.723750	-7.067165	0.000000	-31.447099	-4.520888	0.000000
227 QF	34	138.975625	138.975625	-6.816955	0.000000	-31.494410	-4.520888	0.000000
228 S3	26	139.275625	139.275625	-6.524942	0.000000	-31.550273	-4.520888	0.000000
229 BEND	26	141.675625	141.675625	-4.139970	0.000000	-31.789651	-4.699621	0.000000
230 S5H	23	142.225625	142.225625	-3.590015	0.000000	-31.796673	-4.699621	0.000000
231 CT	31	142.325625	142.325625	-3.490023	0.000000	-31.797950	-4.699621	0.000000
232 SXD	9	142.425625	142.425625	-3.390031	0.000000	-31.799227	-4.699621	0.000000
233 S2H	18	142.675625	142.675625	-3.140051	0.000000	-31.802419	-4.699621	0.000000
234 QD	34	142.927500	142.927500	-2.888197	0.000000	-31.805634	-4.699621	0.000000
235 QD	35	143.179375	143.179375	-2.636342	0.000000	-31.808850	-4.699621	0.000000
236 S32H	9	146.429375	146.429375	0.613939	0.000000	-31.850345	-4.699621	0.000000
237 CT	32	146.529375	146.529375	0.713384	0.000000	-31.851622	-4.699621	0.000000
238 S3H	14	146.879375	146.879375	1.063356	0.000000	-31.855690	-4.699621	0.000000
239 QF	35	147.131250	147.131250	1.315210	0.000000	-31.859306	-4.699621	0.000000
240 QF	36	147.383125	147.383125	1.567065	0.000000	-31.862522	-4.699621	0.000000
241 S3	27	147.683125	147.683125	1.867040	0.000000	-31.866352	-4.699621	0.000000
242 BEND	27	150.083125	150.083125	4.257347	0.000000	-31.687948	-4.874154	0.000000
243 S5H	24	150.633125	150.633125	4.890166	0.000000	-31.599364	-4.874154	0.000000
244 CT	33	150.733125	150.733125	4.898861	0.000000	-31.583258	-4.874154	0.000000
245 SXD	10	150.833125	150.833125	4.997555	0.000000	-31.567152	-4.874154	0.000000
246 S2H	19	151.083125	151.083125	5.244291	0.000000	-31.526887	-4.874154	0.000000
247 QD	36	151.335000	151.335000	5.492878	0.000000	-31.486320	-4.874154	0.000000
248 QD	37	151.586875	151.586875	5.741465	0.000000	-31.445753	-4.874154	0.000000
249 S3	28	151.886875	151.886875	6.037548	0.000000	-31.397435	-4.874154	0.000000
250 BEND	28	154.286875	154.286875	8.360561	0.000000	-30.806668	-5.048687	0.000000
251 S5H	25	154.836875	154.836875	8.879751	0.000000	-30.625171	-5.048687	0.000000
252 CT	34	154.936875	154.936875	8.974150	0.000000	-30.592172	-5.048687	0.000000
253 S3H	15	155.286875	155.286875	9.304544	0.000000	-30.47674	-5.048687	0.000000
254 QF	37	155.538750	155.538750	9.542309	0.000000	-30.393556	-5.048687	0.000000
255 QF	38	155.790625	155.790625	9.780075	0.000000	-30.310439	-5.048687	0.000000
256 S32H	10	159.040625	159.040625	12.848019	0.000000	-29.237956	-5.048687	0.000000
257 CT	35	159.140625	159.140625	12.942417	0.000000	-29.204957	-5.048687	0.000000
258 S3H	16	159.490625	159.490625	13.272811	0.000000	-29.089459	-5.048687	0.000000

TABLE III (CONTINUES)

AGS BOOSTER LATTICE FOR SURVEY,
SURVEY OF BEAM LINE "RING",

ZOHREH PARSA

"MAD" VERSION: 6.01/03 RUN: 21-NOV-8 10:18:00
PAGE 8

POS. NO.	ELEMENT NAME	SEQUENCE NO.	ARC M	POSITIONS			ANGLES		
				X M	Y M	Z M	THETA RAD	PHI RAD	PSI RAD
259	QD	38	159.742500	159.949375	13.510577	0.000000	-29.006341	-5.048687	0.000000
260	QD	39	159.994375	159.949375	13.748343	0.000000	-28.923224	-5.048687	0.000000
261	S3	29	160.294375	160.294375	14.031538	0.000000	-28.846687	-5.048687	0.000000
262	BEND	29	162.694375	162.694375	16.216673	0.000000	-27.839047	-5.223220	0.000000
263	S5H	26	163.244375	163.244375	16.696459	0.000000	-27.570151	-5.223220	0.000000
264	CT	36	163.344375	163.344375	16.783693	0.000000	-27.521261	-5.223220	0.000000
265	SXF	10	163.444375	163.444375	16.870927	0.000000	-27.472370	-5.223220	0.000000
266	S2H	26	163.694375	163.694375	17.089012	0.000000	-27.350145	-5.223220	0.000000
267	QF	39	163.946250	163.946250	17.308732	0.000000	-27.227003	-5.223220	0.000000
268	QF	40	164.198125	164.198125	17.528452	0.000000	-27.163860	-5.223220	0.000000
269	S3	30	164.498125	164.498125	17.790154	0.000000	-26.957190	-5.223220	0.000000
270	BEND	30	166.898125	166.898125	19.770118	0.000000	-25.607534	-5.223220	0.000000
271	S5H	27	167.448125	167.448125	20.196821	0.000000	-25.259409	-5.397753	0.000000
272	CT	37	167.548125	167.548125	20.274240	0.000000	-25.196113	-5.397753	0.000000
273	S3H	17	167.898125	167.898125	20.545206	0.000000	-24.974579	-5.397753	0.000000
274	QD	40	168.150000	168.150000	20.740205	0.000000	-24.815154	-5.397753	0.000000
275	QD	41	168.401875	168.401875	20.935204	0.000000	-24.655728	-5.397753	0.000000
276	S3	31	168.701875	168.701875	21.167461	0.000000	-24.465842	-5.397753	0.000000
277	BEND	31	171.101875	171.101875	22.883865	0.000000	-22.792717	-5.572286	0.000000
278	S5H	28	171.651875	171.651875	23.242749	0.000000	-22.375940	-5.572286	0.000000
279	CT	38	171.751875	171.751875	23.308001	0.000000	-22.300163	-5.572286	0.000000
280	SXF	11	171.851875	171.851875	23.373252	0.000000	-22.224385	-5.572286	0.000000
281	S2H	21	172.101875	172.101875	23.536381	0.000000	-22.034941	-5.572286	0.000000
282	QF	41	172.353750	172.353750	23.700734	0.000000	-21.844077	-5.572286	0.000000
283	QF	42	172.605625	172.605625	23.865086	0.000000	-21.653212	-5.572286	0.000000
284	S3	32	172.905625	172.905625	24.060841	0.000000	-21.425880	-5.572286	0.000000
285	BEND	32	175.305625	175.305625	25.460634	0.000000	-19.480122	-5.746819	0.000000
286	S5H	29	175.855625	175.855625	25.741693	0.000000	-19.007358	-5.746819	0.000000
287	CT	39	175.955625	175.955625	25.792795	0.000000	-18.921401	-5.746819	0.000000
288	SXD	11	176.055625	176.055625	25.843897	0.000000	-18.835444	-5.746819	0.000000
289	S2H	22	176.305625	176.305625	25.971651	0.000000	-18.620551	-5.746819	0.000000
290	QD	42	176.557500	176.557500	26.100363	0.000000	-18.404047	-5.746819	0.000000
291	QD	43	176.809375	176.809375	26.229075	0.000000	-18.187542	-5.746819	0.000000
292	S37	1	180.509375	180.509375	28.119835	0.000000	-15.007130	-5.746819	0.000000
293	QF	43	180.761250	180.761250	28.248548	0.000000	-14.790625	-5.746819	0.000000

TABLE III (CONTINUES)

AGS BOOSTER LATTICE FOR SURVEY
SURVEY OF BEAM LINE "RING",

ZOHREH PARSA

"MAD" VERSION: 6.01/03 RUN: 21-NOV-8 10:18:00 PAGE 9

ELEMENT OCC. NAME NO.	POS. NO.	SEQUENCE SUM(L)	POSITIONS			Z M	I RAD	ANGLES		PSI RAD
			X M	Y M	Z M			THETA RAD	PHI RAD	
294 QF	44	181.013125	181.013125	28.377260	0.000000	-14.574121	-5.746819	0.000000	0.000000	0.000000
295 S3	33	181.313125	181.313125	28.530565	0.000000	-14.316249	-5.746819	0.000000	0.000000	0.000000
296 BEND	33	183.713125	183.713125	29.571215	0.000000	-12.156981	-5.921352	0.000000	0.000000	0.000000
297 S5H	30	184.263125	184.263125	29.765910	0.000000	-11.642594	-5.921352	0.000000	0.000000	0.000000
298 CT	40	184.363125	184.363125	29.801309	0.000000	-11.549069	-5.921352	0.000000	0.000000	0.000000
299 SXD	12	184.463125	184.463125	29.836708	0.000000	-1.455544	-5.921352	0.000000	0.000000	0.000000
300 S2H	23	184.713125	184.713125	29.925205	0.000000	-11.221732	-5.921352	0.000000	0.000000	0.000000
301 QD	44	184.965000	184.965000	30.014366	0.000000	-10.986166	-5.921352	0.000000	0.000000	0.000000
302 QD	45	185.216875	185.216875	30.0183527	0.000000	-10.750600	-5.921352	0.000000	0.000000	0.000000
303 S3	34	185.516875	185.516875	30.0209724	0.000000	-10.470025	-5.921352	0.000000	0.000000	0.000000
304 BEND	34	187.916875	187.916875	30.059612	0.000000	-8.162854	-6.095884	0.000000	0.000000	0.000000
305 S5H	31	188.466875	188.466875	30.0962026	0.000000	-7.622473	-6.095884	0.000000	0.000000	0.000000
306 CT	41	188.566875	188.566875	30.098647	0.000000	-7.524222	-6.095884	0.000000	0.000000	0.000000
307 S3H	18	188.916875	188.916875	31.045820	0.000000	-7.180344	-6.095884	0.000000	0.000000	0.000000
308 QF	45	189.168750	189.168750	31.092721	0.000000	-6.932874	-6.095884	0.000000	0.000000	0.000000
309 QF	46	189.420625	189.420625	31.139622	0.000000	-6.685404	-6.095884	0.000000	0.000000	0.000000
310 S37	2	193.120625	193.120625	31.828590	0.000000	-3.050115	-6.095884	0.000000	0.000000	0.000000
311 QD	46	193.372500	193.372500	31.875491	0.000000	-2.802646	-6.095884	0.000000	0.000000	0.000000
312 QD	47	193.624375	193.624375	31.922392	0.000000	-2.555176	-6.095884	0.000000	0.000000	0.000000
313 S3	35	193.924375	193.924375	31.972854	0.000000	-2.260423	-6.095884	0.000000	0.000000	0.000000
314 BEND	35	196.324375	196.324375	32.217632	0.000000	-0.124549	-6.270417	0.000000	0.000000	0.000000
315 S5H	32	196.874375	196.874375	32.224655	0.000000	0.674505	-6.270417	0.000000	0.000000	0.000000
316 CT	42	196.974375	196.974375	32.225931	0.000000	0.774496	-6.270417	0.000000	0.000000	0.000000
317 SXF	12	197.074375	197.074375	32.227208	0.000000	0.874488	-6.270417	0.000000	0.000000	0.000000
318 S2H	24	197.324375	197.324375	32.230400	0.000000	1.124468	-6.270417	0.000000	0.000000	0.000000
319 QF	47	197.576250	197.576250	32.233616	0.000000	1.376322	-6.270417	0.000000	0.000000	0.000000
320 QF	48	197.828125	197.828125	32.236832	0.000000	1.628177	-6.270417	0.000000	0.000000	0.000000
321 S3	36	198.128125	198.128125	32.2406662	0.000000	1.928152	-6.270417	0.000000	0.000000	0.000000
322 BEND	36	200.528125	200.528125	32.062258	0.000000	4.3184950	-6.444950	0.000000	0.000000	0.000000
323 S10	4	201.528125	201.528125	31.901197	0.000000	5.305403	-6.444950	0.000000	0.000000	0.000000
324 QD	48	201.780000	201.780000	31.886630	0.000000	5.553990	-6.444950	0.000000	0.000000	0.000000

TOTAL LENGTH = 201.780000

ARC LENGTH

= 201.780000

ERROR(X) = 0.865636E-10
 ERROR(THETA) = 0.155864E-10
 TOTAL LENGTH = 201.780000
 ARC LENGTH = 201.780000
 ERROR(Z) = -0.496590E-09
 ERROR(PHI) = 0.000000E+00
 ERROR(PSI) = 0.000000E+00

ZOHREH PARSA 21-NOV-8 10:18:34

*USED BNLDAG::DUA&:[PARSA1.MAD.MAD6]MAD6.EX

Page 22

TABLE IV

a - k

LATTICE FUNCTIONS FOR THE AGS - BOOSTER
WITH
 $\Delta(P)/P = -.01 \text{ TO } +.01$ with .002 increments.

TABLE IV a

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18											
PAGE	1										
ELEMENT SEQUENCE	1	HORI ZONTAL	MUX X(CO)	PX(L)	DX	DPX	1	BETAY	ALFAY	MUY Y(CO)	DY DPY
POS. ELEMENT OCC.	DIST [M]	BETAX [L1]	ALFAX [L1]	X(CO) [MMJ]	L.001	[MMJ]	1	Y(CO) [MMJ]	[L1]	L.001	[L1]
NO. NAME NO.											
BEGIN RING	1	0.000	3.721	0.0118	0.000	-4.957	0.096	0.451-0.005	13.368	-0.045	0.000
BEGIN B4S	1	33.630	3.720	0.0118	0.804	-4.957	0.096	0.451-0.005	13.375	-0.045	0.000
BEGIN HCDF	3	33.630	3.720	0.0118	0.804	-4.957	0.096	0.451-0.005	13.375	-0.045	0.000
55 QD	9	33.882	3.867	-0.603	0.815	-5.024	-0.625	0.458 0.061	12.915	1.831	0.000
55 S3	7	34.182	4.265	-0.710	0.827	-5.213	-0.625	0.476 0.061	11.836	1.729	0.000
57 BEND	7	36.582	9.575	-1.466	0.888	-8.755	-0.292	0.831 0.229	5.412	0.922	0.860
58 S5H	6	37.132	11.305	-1.648	0.897	-10.028	-2.292	0.960 0.229	4.494	0.732	0.878
59 CT	8	37.232	11.641	-1.682	0.898	-10.260	-2.292	0.983 0.229	4.350	0.697	0.881
60 SXF	3	37.332	11.986	-1.732	0.899	-10.491	-2.300	1.006 0.230	4.212	0.668	0.885
61 S2H	5	37.582	12.882	-1.816	0.903	-11.072	-2.300	1.005 0.230	3.895	0.652	0.882
62 QF	9	37.834	13.350	-1.882	0.906	-11.456	-0.711	1.065 0.077	3.757	-0.827	0.000
END HCDF	3	37.834	13.350	-0.002	0.906	-11.456	-0.711	1.105 0.077	3.757	-0.827	0.000
BEGIN HCDF	3	38.086	12.884	1.812	0.913	-11.432	0.903	1.104-0.079	3.924	-0.639	0.000
63 QF	18	38.386	11.816	1.711	0.913	-11.158	0.903	1.080-0.079	4.344	-0.748	0.000
64 S3	8	40.786	5.313	0.952	0.962	-0.939	-0.722	1.089-0.086	1.021	-1.598	0.000
65 BEND	8	41.336	4.366	0.753	0.980	-11.340	-0.722	1.137 0.086	11.896	-1.786	0.000
66 S5H	7	41.436	4.217	0.717	0.984	-11.413	-0.722	1.145 0.086	12.260	-1.821	0.000
67 CT	9	41.536	4.072	0.718	0.988	-11.483	-0.722	1.153 0.075	12.463	-1.974	0.000
68 SXD	3	41.786	3.723	0.624	0.998	-11.652	-0.669	1.173 0.075	13.665	-2.072	0.000
69 S2H	6	42.037	3.571	0.620	1.009	-12.038	-2.380	1.214 0.247	14.221	-0.085	1.005
70 QD	10	42.037	3.571	0.620	1.009	-12.038	-2.380	1.214 0.247	14.221	-0.085	1.005
END HCDF	3	42.037	3.571	0.620	1.009	-12.038	-2.380	1.214 0.247	14.221	-0.085	1.005
BEGIN HCDF0	2	42.037	3.571	0.620	1.009	-12.038	-2.380	1.214 0.247	14.221	-0.085	1.005
71 QD	11	42.889	3.713	-0.582	1.021	-2.870	-4.180	1.300 0.429	13.749	1.914	1.007
72 S32H	13	45.539	11.418	-1.765	1.021	-26.590	-4.180	2.722 0.429	14.838	0.800	1.000
73 CT	10	45.639	11.779	-1.802	1.066	-27.012	-4.180	2.766 0.429	4.680	0.766	1.000
74 S3H	4	45.969	13.098	-1.929	1.111	-28.490	-4.180	2.919 0.429	4.180	0.646	1.000
75 QF	11	46.241	13.616	-0.984	1.114	-29.039	-0.123	2.976 0.013	4.017	0.603	1.000
END HCDF0	2	46.241	13.616	-0.984	1.114	-29.039	-0.123	2.976 0.013	4.017	0.603	1.000
BEGIN HCDF	4	46.241	13.181	-0.084	1.114	-29.039	-0.123	2.976 0.013	4.017	0.603	1.000
76 QF	12	46.493	12.477	1.172	1.117	-28.552	3.937	2.926-0.403	4.178	-0.640	1.000
77 S3	9	46.793	12.136	1.677	1.120	-27.359	3.937	2.930-0.403	4.597	-0.743	1.120
78 BEND	9	49.193	5.759	0.951	1.167	-19.665	2.413	2.014-0.243	1.043	-1.502	1.178
79 S5H	8	49.743	4.804	0.768	1.184	-18.325	2.413	1.878-0.243	1.811	-1.682	1.186
80 CT	11	49.843	4.652	0.734	1.187	-18.081	2.413	1.853-0.243	1.2.154	-1.714	1.188
81 SXD	4	49.943	4.501	0.766	1.191	-17.831	2.544	1.827-0.270	1.2.522	-1.929	1.189
82 S2H	7	50.193	4.136	0.677	1.200	-17.189	2.544	1.758-0.270	1.3.521	-2.025	1.192
83 QD	12	50.445	3.960	0.022	1.210	-16.856	0.084	1.721-0.019	1.4.057	-0.059	1.195
END HCDF0	4	50.445	3.960	0.022	1.210	-16.856	0.084	1.721-0.019	1.4.057	-0.059	1.195
BEGIN HCDFL	1	50.445	3.960	0.022	1.210	-16.856	0.084	1.721-0.019	1.4.057	-0.059	1.195
84 QD	13	50.697	4.113	-0.631	1.220	-17.146	-2.372	1.748 0.232	1.3.579	1.915	1.198
85 S3	10	50.997	4.527	-0.733	1.231	-17.865	-2.372	1.819 0.232	1.2.450	1.811	2.002
86 BEND	10	53.397	9.925	-1.490	1.290	-25.476	-3.909	2.580 0.391	1.612	1.248	0.000
87 S5H	9	53.947	11.671	-1.671	1.298	-27.647	-3.909	2.799 0.391	4.602	0.809	0.000
88 CT	12	54.047	12.022	-1.703	1.300	-28.042	-3.909	2.839 0.391	4.443	0.772	1.269
89 S3H	5	54.397	13.267	-1.818	1.304	-29.424	-3.909	2.979 0.391	3.942	0.645	1.283
90 QF	13	54.649	13.722	0.051	1.307	-29.888	0.273	3.025-0.032	3.772	0.631	1.293
END HCDFL	1	54.649	13.722	0.051	1.307	-29.888	0.273	3.025-0.032	3.772	0.631	1.293

TABLE IV A

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
DELTA(P)/P = -0.0100000
SYMM = F

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18
PAGE 2

POS. NO.	ELEMENT OCC. NAME	ELEMENT SEQUENCE	DIST [M]	I BETAX [MJ]	HORIZONTAL [L2P1]	HORIZONTAL [CO] [MM]	DX [EM]	DPX [L.001]	VERTICAL		
									I	BETAY [MJ]	ALFAV [L]
BEGIN	HCFDO	2	54.649	13.722	0.051	1.307-29.888	0.273	3.025-0.032	3.772	0.031	1.293
91	QF	14	54.901	13.216	1.913	1.310-29.286	4.445	2.963-0.454	3.910	-0.579	1.304
92	S32H	4	58.151	4.456	0.756	1.380-14.693	4.445	1.457-0.454	1.399	-1.702	1.386
93	CT	13	58.251	4.307	0.720	1.384-14.245	4.445	1.411-0.454	11.746	-1.737	1.387
94	S3H	6	58.601	3.841	0.596	1.398-12.673	4.445	1.249-0.454	13.017	-1.858	1.392
95	QD	14	58.852	3.697	0.622	1.409-11.770	2.680	1.155-0.280	13.487	0.033	1.395
END	HCFDO	2	58.852	3.697	0.622	1.409-11.770	2.680	1.155-0.280	13.487	0.033	1.395
BEGIN	HCDF	4	58.852	3.697	0.622	1.409-11.770	2.680	1.155-0.280	13.487	0.033	1.395
96	QD	15	59.104	3.864	0.643	1.420-11.301	1.013	1.044-0.117	12.984	1.919	1.398
97	S3	11	59.404	4.288	0.754	1.431-10.994	1.013	1.068-0.117	11.854	1.810	1.402
98	BEND	11	61.804	9.907	-1.547	1.492-10.511	-0.615	0.983-0.047	5.155	0.949	1.452
99	S5H	10	62.354	11.732	-1.738	1.500-10.853	-0.615	1.010-0.047	4.215	0.744	1.471
100	CT	14	62.454	12.087	-1.772	1.501-10.915	-0.615	1.015-0.047	4.668	0.707	1.475
101	SXF	4	62.554	12.450	-1.825	1.503-10.977	-0.623	1.019-0.049	3.928	0.675	1.479
102	S2H	8	62.804	13.394	-1.913	1.506-11.135	-0.623	1.032-0.049	3.611	0.581	1.489
103	QF	15	63.056	13.893	-0.026	1.509-11.094	0.944	1.026-0.096	3.463	0.007	1.501
END	HCDF	4	63.056	13.893	-0.026	1.509-11.094	0.944	1.026-0.096	3.463	0.007	1.501
BEGIN	HCFDL	2	63.056	13.893	-0.026	1.509-11.094	0.944	1.026-0.096	3.463	0.007	1.501
104	QF	16	63.308	13.419	1.865	1.512-10.657	2.478	0.983-0.238	3.604	-0.566	1.512
105	S3	12	63.608	12.320	1.764	1.515-10.906	2.478	0.910-0.238	3.981	-0.567	1.525
106	BEND	12	66.008	5.552	1.009	1.562-5.902	0.821	0.532-0.071	9.378	-1.549	1.590
107	S5H	11	66.558	4.543	0.807	1.580-5.446	0.821	0.493-0.071	11.211	-1.750	1.599
108	CT	15	66.658	4.384	0.770	1.584-5.363	0.821	0.485-0.071	11.568	-1.787	1.600
109	S3H	7	67.008	3.885	0.642	1.597-5.073	0.821	0.460-0.071	12.876	-1.915	1.605
110	QD	16	67.260	3.719	0.618	1.608-4.957	0.821	0.451-0.075	13.381	-0.045	1.608
END	HCFDL	2	67.260	3.719	0.618	1.608-4.957	0.896	0.451-0.075	13.381	-0.045	1.608
END	B4S	1	67.260	3.719	0.618	1.608-4.957	0.896	0.451-0.075	13.381	-0.045	1.608
END	RING	1	201.780	3.713	0.618	4.828-4.957	0.896	0.451-0.075	13.408	-0.045	4.819
TOTAL LENGTH =						QX, QX,			4.827757	QY,	4.818567
ALFA	=					BETAX(MAX)	=	-0.527747	=	0.932452	
GAMMA(TR)	=					DX(MAX)	=	13.898436		14.248702	
						XCO(MAX)	=	3.0025205		0.0000000	
						XCO(R.M.S.)	=	29.887657		0.0000000	
								16.743038		0.0000000	
... SEARCHING FOR CLOSED ORBIT FOR BEAM LINE "RING"						PY		-0.0080000	SYMM = F		
... ITER:	X					BETAY(MAX)	=	0.0000000	ERROR		
... 1						DY(MAX)	=	0.203318E-02			
... 2						VCO(MAX)	=	0.277075E-02			
... 3						VCO(R.M.S.)	=	0.621002E-02			

TABLE IV b

AGS BOOSTER LATTICE FOR SURVEY LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING DELTA(P)/P = -0.0080000 SYMM = F"																
POS.	ELEMENT OCC. NO.	ELEMENT SEQUENCE NAME	DIST [M]	BETAX [1]	ALFAX [M]	HORI [1]	ZONNT [CO]	A L [MM]	PX(CO) [.001]	DX [M]	DPX [1]	VER TIC AL I [M]	MUY [2P1] [MM]	DPY [.0011] [MM]		
		BEGIN RING	1	0.000	3.706	0.016	0.000	-4.037	0.085	0.469-0.007	13.418	-0.035	0.000	0.000		
		BEGIN B4S	33.630	3.706	0.016	0.804	-4.037	0.085	0.469-0.007	13.423	-0.035	0.804	0.000			
		BEGIN HCDF	33.630	3.706	0.016	0.804	-4.037	0.085	0.469-0.007	13.423	-0.035	0.804	0.000			
		QD	33.682	3.853	0.603	0.814	-4.098	0.085	0.503	0.475-0.062	12.957	-1.847	0.000	0.000		
		S3	34.182	4.250	0.710	0.826	-4.242	0.085	0.503	0.475-0.062	11.871	1.744	0.000	0.000		
		BEND	36.582	9.551	-1.465	0.888	-7.074	-1.834	0.849	0.229	5.407	0.928	0.000	0.000		
		S5H	6	37.132	11.277	-1.647	0.897	-8.091	-1.834	0.977	0.229	4.484	0.737	0.000		
		CT	8	37.132	11.612	-1.681	0.898	-8.276	-1.834	1.001	0.229	4.339	0.703	0.000		
		SXF	3	37.332	11.956	-1.727	0.899	-8.424	-1.839	1.024	0.238	4.200	0.673	0.000		
		S2H	5	37.582	12.848	-1.811	0.903	-8.925	-1.839	1.082	0.238	3.883	0.895	0.000		
		QF	9	37.834	13.314	-0.003	0.906	-9.238	-0.559	1.121	0.075	3.742	-0.021	0.000		
		END	3	37.834	13.314	-0.003	0.906	-9.238	-0.559	1.121	0.075	3.742	-0.021	0.000		
		HCDF	3	37.834	13.314	-0.003	0.906	-9.238	-0.559	1.121	0.075	3.742	-0.021	0.000		
		QF	10	38.086	12.850	1.807	0.907	-9.207	0.741	1.095	-0.083	3.905	-0.631	0.000		
		S3	8	38.386	11.788	1.706	0.913	-8.983	0.741	1.095	-0.083	4.320	-0.739	0.000		
		BEND	8	40.786	5.304	0.953	0.962	-8.759	-0.556	1.091	0.080	9.906	0.585	0.000		
		S5H	7	41.336	4.358	0.754	0.980	-9.067	-0.556	1.136	0.080	11.811	-1.583	0.000		
		CT	9	41.336	4.210	0.717	0.984	-9.123	-0.556	1.144	0.080	12.173	-1.779	0.000		
		SXD	3	41.536	4.066	0.711	0.988	-9.178	-0.522	1.152	0.072	12.173	-1.814	0.000		
		S2H	6	41.786	3.731	0.618	0.998	-9.309	-0.522	1.170	0.072	13.555	-1.943	0.000		
		QD	10	42.037	3.572	0.614	1.009	-9.615	-1.889	1.309	0.072	1.002	0.999	0.000		
		END	3	42.037	3.572	0.614	1.009	-9.615	-1.889	1.309	0.072	1.002	0.999	0.000		
		HCDF	2	42.037	3.572	0.614	1.009	-9.615	-1.889	1.309	0.072	1.002	0.999	0.000		
		END	71	QD	11	42.289	3.717	-0.589	1.020	-9.275	-3.026	2.697	0.425	13.623	-1.912	0.000
		S32H	3	45.539	11.461	-1.775	1.042	-21.171	-3.026	2.697	0.425	4.762	0.792	0.000		
		CT	10	45.639	11.822	-1.812	1.065	-21.506	-3.326	2.740	0.425	4.606	0.758	0.000		
		S3H	4	45.989	13.146	-1.939	1.110	-22.688	-3.326	2.898	0.399	4.112	-0.633	0.000		
		QF	11	46.241	13.666	-0.088	1.113	-23.116	-0.097	2.947	0.013	3.954	0.002	0.000		
		END	72	HCDF0	4	46.241	13.666	-0.088	1.113	-23.116	-0.097	2.947	0.013	3.954	0.002	0.000
		HCDF	4	46.241	13.666	-0.088	1.113	-23.116	-0.097	2.947	0.013	3.954	0.002	0.000		
		BEGIN	73	HCDF0	10	45.639	11.822	-1.812	1.116	-22.729	3.135	2.107	0.000	0.000		
		HCDF	10	45.989	13.146	-1.939	1.120	-21.781	3.135	2.776	-0.399	4.526	-0.736	0.000		
		QD	74	46.793	12.187	1.681	1.166	-15.656	1.927	1.995	-0.243	9.971	-1.513	0.000		
		S3H	77	49.193	5.771	0.964	1.183	-14.588	1.927	1.860	-0.243	11.750	-1.696	0.000		
		BEND	78	49.193	5.771	0.964	1.183	-13.454	1.927	1.860	-0.243	12.461	-1.729	0.000		
		S5H	79	49.443	4.805	0.778	1.186	-14.394	1.927	1.869	-0.243	12.461	-1.729	0.000		
		CT	80	49.843	4.651	0.745	1.190	-14.195	2.010	1.809	-0.264	12.461	-1.907	0.000		
		SXD	81	49.943	4.499	0.763	1.195	-14.195	2.010	1.809	-0.264	12.461	-1.92	0.000		
		QD	82	50.193	4.137	0.675	1.199	-13.689	2.010	1.742	-0.264	12.461	-1.92	0.000		
		S2H	83	50.445	3.963	0.619	1.209	-13.428	0.051	1.787	-0.015	1.181	1.181	0.000		
		END	84	50.445	3.963	0.619	1.209	-13.428	0.051	1.787	-0.015	1.189	1.189	0.000		
		HCDFL	1	50.445	3.963	0.619	1.209	-13.428	0.051	1.787	-0.015	1.198	1.198	0.000		
		BEGIN	85	50.697	4.117	-0.634	1.219	-13.663	-1.907	1.735	0.234	13.492	1.915	0.000		
		QD	86	50.997	4.532	-0.737	1.230	-14.239	-1.907	1.806	0.234	12.365	1.811	0.000		
		S3	87	53.397	9.920	-1.483	1.289	-20.329	-3.126	2.567	0.391	1.972	-0.567	0.000		
		S5H	88	53.947	11.664	-1.662	1.297	-22.062	-3.126	2.786	0.391	1.972	-0.571	0.000		
		CT	89	54.397	12.002	-1.695	1.298	-22.377	-3.126	2.825	0.391	1.972	-0.571	0.000		
		S3H	90	54.649	13.238	-1.809	1.303	-23.488	-3.126	2.865	0.391	1.972	-0.574	0.000		
		END	91	54.649	13.688	0.056	1.306	-23.852	0.211	3.011	-0.030	1.286	0.297	0.000		
		HCDFL	92	54.649	13.688	0.056	1.306	-23.852	0.211	3.011	-0.030	1.297	0.297	0.000		

TABLE IV b

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18

ZOHREH PARSA /

LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"

AGS BOOSTER LATTICE FOR SURVEY

DELTA(P)/P = -0.008000

SYMM = F

POS.	ELEMENT SEQUENCE	I	BETAX	ALFAX	HORIZONTAL	MUX	PX(CO)	DX	DPX	I	BETAY	ALFAY	MUY	Y(CO)	DY	DPY
NO.	NAME	[1]	[MJ]	[1]	[L2PI]	[MM]	[.0011]	[M]	[1]	[1]	[MJ]	[L]	[2PI]	[MM]	[.0011]	[M]
BEGIN	HCFDO	2	54.649	13.688	.0.056	1.306-23.852	.0.211	3.011-0.030	3.754	.0.025	1.297	.0.000	0.000	0.000	0.000	0.000
91	QF	14	54.901	13.182	1.913	1.309-23.374	3.541	2.949-0.450	3.894	-.0.583	1.307	.0.000	0.000	0.000	0.000	0.000
92	S32H	4	58.151	4.440	.0.755	1.379-11.774	3.541	1.462-0.450	11.412	-1.712	1.389	.0.000	0.000	0.000	0.000	0.000
93	CT	13	58.251	4.291	.0.720	1.383-11.417	3.541	1.417-0.450	11.761	-1.746	1.390	.0.000	0.000	0.000	0.000	0.000
94	S3H	6	58.601	3.828	.0.595	1.397-10.168	3.541	1.256-0.450	13.036	-1.868	1.395	.0.000	0.000	0.000	0.000	0.000
95	QD	14	58.852	3.684	-.0.021	1.408-9.451	2.124	1.164-0.275	13.510	.0.026	1.398	.0.000	0.000	0.000	0.000	0.000
END	HCFDO	12	58.852	3.684	-.0.021	1.408-9.451	2.124	1.164-0.275	13.510	.0.026	1.398	.0.000	0.000	0.000	0.000	0.000
BEGIN	HCDF	4	58.852	3.684	-.0.021	1.408-9.451	2.124	1.164-0.275	13.510	.0.026	1.398	.0.000	0.000	0.000	0.000	0.000
96	QD	15	59.104	3.850	-.0.640	1.418-9.083	0.785	1.115-0.111	13.010	1.916	1.401	.0.000	0.000	0.000	0.000	0.000
97	S3	11	59.404	4.270	-.0.751	1.430-8.845	0.081	1.081-0.111	11.885	1.405	0.000	0.000	0.000	0.000	0.000	0.000
98	BEND	11	61.804	9.857	-1.540	1.491-8.518	0.514	1.011-0.053	5.205	0.950	1.455	.0.000	0.000	0.000	0.000	0.000
99	S5H	10	62.354	11.669	-1.729	1.499-8.803	0.514	1.040-0.053	4.265	0.747	1.473	.0.000	0.000	0.000	0.000	0.000
100	CT	14	62.454	12.022	-1.764	1.500-8.854	0.514	1.046-0.053	4.118	0.710	1.477	.0.000	0.000	0.000	0.000	0.000
101	SXF	4	62.554	12.382	-1.813	1.502-8.907	0.520	1.051-0.054	3.978	0.678	1.481	.0.000	0.000	0.000	0.000	0.000
102	S2H	8	62.804	13.318	-1.901	1.505-9.037	0.520	1.065-0.054	3.659	0.586	1.492	.0.000	0.000	0.000	0.000	0.000
103	QF	15	63.056	13.813	-.0.024	1.508-9.008	0.753	1.060-0.095	3.511	0.006	1.503	.0.000	0.000	0.000	0.000	0.000
END	HCDF	4	63.056	13.813	-.0.024	1.508-9.008	0.753	1.060-0.095	3.511	0.006	1.503	.0.000	0.000	0.000	0.000	0.000
BEGIN	HCFDL	2	63.056	13.813	-.0.024	1.508-9.008	0.753	1.060-0.095	3.511	0.006	1.503	.0.000	0.000	0.000	0.000	0.000
104	QF	16	63.308	13.342	1.856	1.511-8.657	1.998	0.943-0.242	3.654	0.574	1.514	.0.000	0.000	0.000	0.000	0.000
105	S3	12	63.608	12.250	1.755	1.515-8.053	1.998	0.943-0.242	4.034	0.684	1.527	.0.000	0.000	0.000	0.000	0.000
106	BEND	12	66.078	5.524	1.004	1.562-4.814	0.675	0.556-0.075	9.436	-1.549	1.591	.0.000	0.000	0.000	0.000	0.000
107	S5H	11	66.558	4.522	0.803	1.580-4.440	0.675	0.514-0.075	11.265	-1.749	1.599	.0.000	0.000	0.000	0.000	0.000
108	CT	15	66.658	4.364	0.766	1.583-4.372	0.675	0.506-0.075	11.621	-1.786	1.601	.0.000	0.000	0.000	0.000	0.000
109	S3H	7	67.008	3.869	0.638	1.597-4.133	0.675	0.479-0.075	12.926	-1.913	1.605	.0.000	0.000	0.000	0.000	0.000
110	QD	16	67.260	3.705	0.016	1.608-4.033	0.685	0.469-0.077	13.427	-0.035	1.609	.0.000	0.000	0.000	0.000	0.000
END	HCFDL	2	67.260	3.705	0.016	1.608-4.033	0.685	0.469-0.077	13.427	-0.035	1.609	.0.000	0.000	0.000	0.000	0.000
END	B4S	1	67.260	3.705	0.016	1.608-4.033	0.685	0.469-0.077	13.427	-0.035	1.609	.0.000	0.000	0.000	0.000	0.000
END	RING	1	201.780	3.701	0.016	4.823	0.000	0.000	4.823	0.000	0.000	0.000	0.000	0.000	0.000	0.000
TOTAL LENGTH =			201.780000			QX,	=	4.824956	QY,	=	4.822669					
ALFA	X	=	0.405705E-01	BETAX(MAX)	=	BETAX(MAX)	=	-0.414831	QY.	=	0.746741					
GAMMA(TR)	=	4.964723	DX(MAX)	=	DX(MAX)	=	13.815980	BETAY(MAX)	=	14.114497						
			XCO(MAX)	=	XCO(MAX)	=	3.010862	DY(MAX)	=	0.00000000						
			XCO(R.M.S.)	=	XCO(R.M.S.)	=	23.851559	YCO(MAX)	=	0.154875E-02						
							13.378647	VCO(R.M.S.)	=	0.153442E-04						
... SEARCHING FOR CLOSED ORBIT FOR BEAM LINE "RING"																
... ITER.																
... 1			-0.003087													
... 2			-0.003082													
... 3			-0.003082													

Page 27

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING
DELTA(P)/P = -0.006000 SYMM = F

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18
PAGE 1

TABLE IV C

POS.	ELEMENT OCC. NO.	ELEMENT SEQUENCE	DIST [M]	BETAX [1]	ALFAX [M]	HORI ZON T AL X(CO) [MM]	MUX [2P1]	DX [MM]	DPX [1]	BETAY [M]	ALFAY [1]	VERTIC AL Y(CO) [MM]	DPY [2P1]	DY [MM]
		BEGIN RING	1	0.000	3.691	0.015	0.000	-3.0082	0.487-0.0009	13.471	-0.0226	0.0000	0.0000	0.0000
		BEGIN B4S	1	33.630	3.690	0.015	0.804	-3.0082	0.487-0.0009	13.474	-0.0226	0.0000	0.0000	0.0000
		BEGIN HCDF	3	33.630	3.690	0.015	0.804	-3.0082	0.487-0.0009	13.474	-0.0226	0.0000	0.0000	0.0000
		OD	55	9	33.882	3.838	-0.603	0.814	-3.121	0.379	0.494	0.0062	13.002	1.863
		S3	56	7	34.182	4.234	-0.710	0.826	-3.235	0.379	0.513	0.0062	11.909	1.759
		BEND	57	7	36.582	9.527	-1.464	0.888	-5.358	-1.376	0.867	0.229	5.405	0.935
		S5H	58	6	37.132	11.582	-1.646	0.897	-6.119	-1.376	0.995	0.229	4.476	0.743
		CT	59	8	37.332	11.925	-1.723	0.898	-6.258	-1.376	1.018	0.229	4.330	0.708
		SXF	60	5	37.582	12.812	-1.807	0.903	-6.396	-1.379	1.099	0.230	4.191	0.677
		S2H	61	9	37.834	13.276	-0.003	0.906	-6.538	-1.379	1.099	0.230	3.872	0.589
		QF	62	9	37.834	13.276	-0.003	0.906	-6.971	-0.412	1.138	0.072	3.729	-0.016
		END	63	3	37.834	13.276	-0.003	0.906	-6.971	-0.412	1.138	0.072	3.729	-0.016
		HCDF	64	8	38.086	12.815	-1.801	0.906	-6.951	-0.412	1.138	0.072	3.729	-0.016
		S3	65	8	38.386	11.758	-1.701	0.913	-6.779	-0.570	1.109	-0.088	3.889	0.895
		BEND	66	7	40.786	5.295	0.954	0.962	-6.575	-0.401	1.093	0.075	9.906	0.900
		S5H	67	41	4.336	4.356	0.754	0.980	-6.797	-0.401	1.135	0.075	9.876	-1.577
		CT	68	41	4.336	4.202	0.754	0.984	-6.837	-0.401	1.142	0.075	11.729	-1.772
		SXD	69	3	41.536	4.059	0.764	0.988	-6.877	-0.401	1.150	0.068	12.463	-1.808
		S2H	70	6	41.786	3.728	0.611	0.998	-6.973	-0.382	1.167	0.068	13.449	-2.006
		QD	71	10	42.037	3.573	0.008	1.009	-7.198	-1.406	1.206	0.240	13.977	-0.051
		END	72	3	42.037	3.573	0.008	1.009	-7.198	-1.406	1.206	0.240	13.977	-0.051
		HCFD	73	11	42.037	3.573	0.008	1.009	-7.198	-1.406	1.206	0.240	13.977	-0.051
		HCDFDFO	74	12	42.037	3.573	0.008	1.009	-7.198	-1.406	1.206	0.240	13.977	-0.051
		OD	75	11	42.289	3.721	-0.595	1.020	-7.689	-2.481	1.290	0.420	13.500	1.912
		S32H	76	13	45.539	11.503	-1.785	1.044	-15.802	-2.481	1.672	0.420	4.688	0.784
		CT	77	10	45.639	11.865	-1.822	1.055	-16.052	-2.481	2.714	0.420	4.533	0.750
		S3H	78	4	45.989	13.193	-1.950	1.112	-16.925	-2.481	2.863	0.420	1.006	0.000
		QF	79	11	46.241	13.717	-0.991	1.112	-17.250	-0.072	2.919	0.013	3.890	0.001
		END	80	12	46.241	13.717	-0.991	1.112	-17.250	-0.072	2.919	0.013	3.890	0.001
		HCDFD	81	4	46.241	13.717	-0.991	1.112	-17.250	-0.072	2.919	0.013	3.890	0.001
		BEND	82	12	46.493	13.284	-1.780	1.115	-16.962	2.341	2.870	-0.396	4.047	-0.625
		SXD	83	12	46.493	12.840	-1.780	1.115	-16.962	2.341	2.870	-0.396	4.047	-0.625
		QF	84	7	46.793	1.228	0.685	1.165	-16.555	2.341	2.750	-0.396	4.456	-0.628
		END	85	9	49.193	5.200	0.976	0.996	-6.655	1.442	1.976	-0.242	9.899	-1.524
		S5H	86	8	49.193	4.806	0.789	1.182	-10.887	1.442	1.842	-0.242	11.689	-1.710
		CT	87	11	49.843	4.651	0.755	1.185	-10.742	1.442	1.817	-0.242	12.036	-1.744
		SXD	88	4	49.943	4.498	0.760	1.189	-10.594	1.488	1.792	-0.257	12.401	-1.885
		QF	89	13	50.697	4.121	-0.637	1.218	-10.207	-1.436	1.721	0.236	1.194	-1.915
		S2H	90	10	50.997	4.138	0.672	1.198	-10.220	1.488	1.727	-0.257	13.372	-1.977
		END	91	12	50.445	3.966	0.616	1.208	-10.029	0.026	1.693	-0.010	1.000	0.000
		HCDF	92	4	50.445	3.966	0.616	1.208	-10.029	0.026	1.693	-0.010	1.000	0.000
		BEGIN	93	1	50.445	3.966	0.616	1.208	-10.029	0.026	1.693	-0.010	1.000	0.000
		HCDFL	94	13	54.649	13.654	0.662	1.302	-17.566	-2.344	2.950	0.391	3.900	0.000
		QD	95	13	54.649	13.654	0.662	1.302	-17.566	-2.344	2.950	0.391	2.996	-0.028
		END	96	1	54.649	13.654	0.662	1.302	-17.566	-2.344	2.950	0.391	2.996	-0.028

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
DELTA(P)/P = -0.006000 SYMM = F

TABLE IV C

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18

PAGE 2

H O R I Z O N T A L										V E R T I C A L				
ELEMENT SEQUENCE	POS. NO.	DIST [M]	BETAX [M]	ALFAX [1]	MUX [2P1]	PX(CO) [MM]	DX [M]	DPX [L.001]	BETAY [1]	ALFAY [M]	MUY [2P1]	PY(CO) [MM]	DY [EM]	DPY [1]
BEGIN HCFDO	2	54.649	13.654	0.062	1.305-17.844	0.153	2.996-0.028	3.738	0.019	1.300	0.000	0.000	0.000	0.000
91 QF	14	54.901	13.147	1.914	1.308-17.489	2.644	2.936-0.447	3.880	-0.588	1.310	0.000	0.000	0.000	0.000
92 S32H	4	58.151	4.423	0.754	1.378-8.844	2.644	1.467-0.447	1.430	-1.721	1.392	0.000	0.000	0.000	0.000
93 CT	13	58.251	4.275	0.719	1.382-8.578	2.644	1.422-0.447	1.780	-1.756	1.393	0.000	0.000	0.000	0.000
94 S3H	6	58.601	3.813	0.594	1.396-7.647	2.644	1.264-0.447	1.060	-1.878	1.398	0.000	0.000	0.000	0.000
95 QD	14	58.852	3.670	-0.020	1.407-7.114	1.578	1.173-0.270	13.537	0.019	1.401	0.000	0.000	0.000	0.000
END HCFDO	2	58.852	3.670	-0.020	1.407-7.114	1.578	1.173-0.270	13.537	0.019	1.401	0.000	0.000	0.000	0.000
BEGIN HCDF	4	58.852	3.670	-0.020	1.407-7.114	1.578	1.173-0.270	13.537	0.019	1.401	0.000	0.000	0.000	0.000
96 QD	15	59.104	3.834	-0.638	1.418-6.843	0.569	1.125-0.104	13.041	1.913	1.404	0.000	0.000	0.000	0.000
97 S3	11	59.404	4.252	-0.748	1.429-6.671	0.569	1.093-0.104	11.919	1.806	1.408	0.000	0.000	0.000	0.000
98 BEND	11	61.804	9.805	-1.532	1.490-6.469	-0.402	1.038-0.104	1.457	0.000	0.000	0.000	0.000	0.000	0.000
99 S5H	10	62.354	11.605	-1.721	1.498-6.692	-0.402	1.071-0.059	5.256	0.951	1.457	0.000	0.000	0.000	0.000
100 CT	14	62.454	11.955	-1.756	1.500-6.732	-0.402	1.077-0.059	4.315	0.750	1.476	0.000	0.000	0.000	0.000
101 SXF	4	62.554	12.313	-1.801	1.501-6.773	-0.405	1.083-0.060	4.168	0.714	1.479	0.000	0.000	0.000	0.000
102 S2H	8	62.804	13.241	-1.888	1.504-6.875	-0.405	1.094-0.060	4.027	0.681	1.483	0.000	0.000	0.000	0.000
103 QF	15	63.056	13.731	-0.022	1.507-6.855	0.563	1.093-0.095	3.708	0.590	1.494	0.000	0.000	0.000	0.000
END HCDF	4	63.056	13.731	-0.022	1.507-6.855	0.563	1.093-0.095	3.559	0.590	1.494	0.000	0.000	0.000	0.000
BEGIN HCFDL	2	63.056	13.731	-0.022	1.507-6.855	0.563	1.093-0.095	3.559	0.590	1.494	0.000	0.000	0.000	0.000
104 QF	16	63.308	13.263	1.846	1.510-6.591	1.511	1.050-0.246	3.703	-0.581	1.516	0.000	0.000	0.000	0.000
105 S3	12	63.608	12.179	1.746	1.514-6.135	1.511	0.975-0.246	4.087	-0.690	1.528	0.000	0.000	0.000	0.000
106 BEND	12	66.008	5.496	1.746	1.561-3.679	0.520	0.579-0.080	9.497	-1.551	1.592	0.000	0.000	0.000	0.000
107 S5H	11	66.558	4.501	0.799	1.579-3.391	0.520	0.534-0.080	11.322	-1.749	1.602	0.000	0.000	0.000	0.000
108 CT	15	66.658	4.344	0.762	1.583-3.339	0.520	0.526-0.080	11.678	-1.785	1.602	0.000	0.000	0.000	0.000
109 S3H	7	67.008	3.852	0.634	1.596-3.156	0.520	0.498-0.080	12.979	-1.911	1.606	0.000	0.000	0.000	0.000
110 QD	16	67.260	3.650	0.015	1.607-3.082	0.669	0.487-0.009	13.476	-0.026	1.609	0.000	0.000	0.000	0.000
END HCFL	2	67.260	3.690	0.015	1.607-3.082	0.669	0.487-0.009	13.476	-0.026	1.609	0.000	0.000	0.000	0.000
END B4S	1	67.260	3.690	0.015	1.607-3.082	0.669	0.487-0.009	13.476	-0.026	1.609	0.000	0.000	0.000	0.000
END RING	1	201.780	3.688	0.015	4.823-3.082	0.669	0.487-0.009	13.486	-0.026	4.826	0.000	0.000	0.000	0.000
TOTAL LENGTH =					QX =		QY =							4.825870
ALFA (TR) =					QX =		QY =							0.560531
GAMMA (TR) =					BETAX(MAX) =		BETAY(MAX) =							13.986908
					DX(MAX) =		DY(MAX) =							0.000000
					XCO(MAX) =		YCO(MAX) =							0.000000
					XCO(R.M.S.) =		YCO(R.M.S.) =							0.000000

... SEARCHING FOR CLOSED ORBIT FOR BEAM LINE "RING" , DELTA(P)/P = -0.004000, SYMM = F
 ... ITER. =
 ... 1 -0.002092
 ... 2 -0.002090
 ... 3 -0.002090

AGS BOOSTER LATTICE FOR SURVEY
 LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
 $\Delta t(P)/P = -0.004000$ SYMM = F

TABLE IV d

POS. NO.	ELEMENT OCC. NAME	ELEMENT SEQUENCE	DIST [M]	I BETAX [M]	I ALFAX [M]	H ORI Z [CO] ONT A L	DX [MM]	DPX [MM]	I BETAY [M]	I ALFAY [M]	VER T I C A L	D Y [MM]	DPY [MM]
BEGIN RING	1	0.000		0.000	-2.090	0.050	0.505-0.011	13.527	-0.017	0.000	0.000	0.000	0.000
BEGIN B4S	1	33.630	3.675	0.013	0.803	-2.090	0.050	0.505-0.011	13.528	-0.017	0.000	0.000	0.000
BEGIN HCDF	3	33.630	3.675	0.013	0.803	-2.090	0.050	0.505-0.011	13.528	-0.017	0.000	0.000	0.000
55 QD	9	33.882	3.822	-0.002	0.603	0.814	-2.192	-0.254	0.511	0.063	13.051	1.879	0.000
56 S3	7	34.182	4.218	-0.710	0.826	-2.192	-0.254	0.530	0.063	11.950	1.775	0.864	0.000
57 BEND	7	36.582	9.501	-1.463	0.888	-3.606	-0.918	0.884	0.229	5.405	0.942	0.866	0.000
58 S5H	6	37.132	11.217	-1.645	0.897	-4.113	-0.918	1.012	0.229	4.471	0.749	0.878	0.000
59 CT	8	37.232	11.551	-1.679	0.898	-4.205	-0.918	1.035	0.229	4.324	0.714	0.882	0.000
60 SXF	3	37.332	11.892	-1.719	0.899	-4.297	-0.919	1.058	0.230	4.184	0.681	0.885	0.000
61 S2H	5	37.582	12.776	-1.802	0.903	-4.528	-0.919	1.116	0.230	3.864	0.594	0.895	0.000
62 QF	9	37.834	13.238	-0.004	0.906	-4.679	-0.270	1.154	0.070	3.718	-0.011	0.906	0.000
END HCDF	3	37.834	13.238	-0.004	0.906	-4.679	-0.270	1.154	0.070	3.718	-0.011	0.906	0.000
BEGIN HCFD	3	37.834	13.238	-0.004	0.906	-4.679	-0.270	1.154	0.070	3.718	-0.011	0.906	0.000
63 QF	10	38.386	12.780	-1.795	0.909	-4.664	-0.389	1.123	0.093	3.875	-0.616	0.917	0.000
64 S3	8	38.386	11.728	-1.696	0.913	-4.546	-0.389	1.16	0.230	3.728	-0.594	0.929	0.000
65 BEND	8	40.786	5.286	0.954	0.962	-4.387	-0.257	1.095	0.069	9.809	-1.570	0.989	0.000
66 S5H	7	41.336	4.342	0.754	0.980	-4.529	-0.257	1.134	0.069	11.651	-1.766	0.997	0.000
67 CT	9	41.436	4.195	0.718	0.984	-4.554	-0.257	1.141	0.069	12.009	-1.801	0.999	0.000
68 SXD	3	41.536	4.052	0.697	0.988	-4.580	-0.248	1.147	0.065	12.000	-1.882	1.000	0.000
69 S2H	6	41.786	3.726	0.605	0.998	-4.642	-0.248	1.164	0.065	13.347	-1.974	1.003	0.000
70 QD	10	42.037	3.574	0.601	1.009	-4.790	-0.236	1.202	0.236	13.862	-0.734	1.006	0.000
END HCFD	3	42.037	3.574	0.601	1.009	-4.790	-0.236	1.202	0.236	13.862	-0.734	1.006	0.000
BEGIN HCDF0	2	42.037	3.574	0.601	1.009	-4.790	-0.236	1.202	0.236	13.862	-0.734	1.006	0.000
71 QD	11	42.889	3.724	-0.602	1.020	-5.115	-1.645	1.284	0.416	13.381	1.910	1.009	0.000
72 S32H	3	45.539	11.544	-1.795	1.031	-1.0484	-1.645	2.164	0.416	4.613	0.777	1.003	0.000
73 CT	10	45.639	11.908	-1.795	1.051	-1.049	-1.645	2.688	0.416	4.461	0.742	1.006	0.000
74 S3H	4	45.989	13.241	-1.960	1.091	-1.227	-1.645	2.835	0.416	3.983	0.620	1.094	0.000
75 QF	11	46.241	13.767	-0.095	1.112	-1.442	-0.047	2.890	0.012	3.828	0.001	1.104	0.000
END HCDF0	2	46.241	13.767	-0.095	1.112	-1.442	-0.047	2.890	0.012	3.828	0.001	1.104	0.000
BEGIN HCDF	4	46.241	13.767	-0.095	1.112	-1.442	-0.047	2.890	0.012	3.828	0.001	1.104	0.000
76 QF	12	46.493	13.334	1.784	1.155	-1.251	1.553	2.841	0.392	3.982	-0.618	1.115	0.000
77 S3	9	46.793	12.288	1.689	1.119	-1.0783	1.553	2.723	-0.392	4.386	-0.722	1.126	0.000
78 BEND	9	49.193	5.795	0.988	1.165	-1.751	0.960	1.957	-0.241	9.828	-1.535	1.186	0.000
79 S5H	8	49.443	4.808	0.800	1.181	-2.222	0.960	1.823	-0.241	11.628	-1.724	1.194	0.000
80 CT	11	49.843	4.650	0.765	1.185	-1.125	0.960	1.799	-0.241	11.978	-1.758	1.196	0.000
81 SXD	1	49.943	4.498	0.757	1.188	-1.072	0.980	1.774	-0.251	12.341	-1.864	1.210	0.000
82 S2H	7	50.193	4.140	0.669	1.197	-1.782	0.980	1.711	-0.251	13.299	-1.954	1.210	0.000
83 QD	12	50.445	3.969	0.014	1.207	-6.657	0.009	1.679	-0.006	13.805	-0.022	1.203	0.000
END HCDF0	4	50.445	3.969	0.014	1.207	-6.657	0.009	1.679	-0.006	13.805	-0.022	1.203	0.000
BEGIN HCDF	1	50.445	3.969	0.014	1.207	-6.657	0.009	1.679	-0.006	13.805	-0.022	1.203	0.000
84 QD	13	50.697	4.126	-0.640	1.217	-6.777	-0.962	1.708	0.238	13.321	1.914	2.292	0.000
85 S3	10	50.997	4.542	-0.743	1.229	-7.067	-0.962	1.780	0.238	12.199	1.809	2.303	0.000
86 BEND	10	53.397	9.908	-1.469	1.287	-10.112	-1.562	2.541	0.391	15.485	0.977	2.557	0.000
87 S5H	9	53.947	1.627	-1.645	1.295	-10.975	-1.562	2.758	0.391	4.515	0.780	2.275	0.000
88 CT	12	54.047	11.960	-1.677	1.296	-1.132	-1.562	2.935	0.391	4.361	0.744	2.278	0.000
89 S3H	5	54.397	13.178	-1.789	1.301	-1.681	-1.562	2.935	0.391	3.882	0.619	2.292	0.000
90 QF	13	54.649	13.619	-1.668	1.304	-1.866	-1.562	2.935	0.391	3.724	0.013	3.003	0.000
END HCDFL	1	54.649	13.619	-1.668	1.304	-1.866	-1.562	2.935	0.391	3.724	0.013	3.003	0.000

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
SYMM = F
DELTA(P)/P = -0.004000

TABLE IV d

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18
PAGE 2

POS. ELEMENT OCC. NO.	ELEMENT NAME	SEQUENCE NO.	HORIZONTAL			VERTICAL			DPY [MM]	DPY [MM]
			BETAX [MJ]	ALFAX [MJ]	MUX [E2P1]	PX(CO) [MM]	DY(CO) [MM]	MUY [E2P1]	ALFAY [MJ]	
BEGIN HCFDO		2	54.649	13.619	0.068	1.304-11.866	0.098	2.982-0.026	3.724	0.013
91 QF	14	54.901	13.111	1.914	1.307-11.631	1.755	2.922-0.443	3.869	-0.592	1.313
92 S32H	4	58.151	4.406	0.753	1.377-5.905	1.755	1.472-0.443	11.452	-1.732	1.395
93 CT	13	58.251	4.259	0.718	1.381-5.729	1.755	1.427-0.443	11.808	-1.767	1.396
94 S3H	6	58.601	3.798	0.593	1.395-5.122	1.755	1.271-0.443	13.088	-1.889	1.401
95 QD	14	58.852	3.655	-0.019	1.406-4.760	1.042	1.181-0.265	13.568	0.012	1.404
END HCFDO	2	58.852	3.655	-0.019	1.406-4.760	1.042	1.181-0.265	13.568	0.012	1.404
BEGIN HCDF	4	58.852	3.655	-0.019	1.406-4.760	1.042	1.181-0.265	13.568	0.012	1.404
96 QD	15	59.104	3.814	-0.635	1.417-4.582	0.367	1.135-0.098	13.076	1.407	1.912
97 S3	11	59.404	4.234	-0.745	1.429-4.472	0.367	1.106-0.098	11.956	1.805	1.411
98 BEND	11	61.804	9.753	-1.525	1.489-4.366	0.279	1.065-0.064	5.308	0.952	1.459
99 S5H	10	62.354	11.540	-1.713	1.498-4.520	-0.279	1.101-0.064	4.366	0.754	1.478
100 CT	14	62.454	11.888	-1.747	1.499-4.549	-0.279	1.107-0.064	4.218	0.718	1.481
101 SXF	4	62.554	12.243	-1.789	1.500-4.577	-0.281	1.114-0.065	4.077	0.684	1.485
102 S2H	8	62.804	13.162	-1.875	1.504-4.647	-0.281	1.130-0.065	3.756	0.594	1.496
103 QF	15	63.056	13.647	-0.021	1.507-4.635	0.374	1.126-0.094	3.607	0.003	1.507
END HCDF	4	63.056	13.647	-0.021	1.507-4.635	0.374	1.126-0.094	3.607	0.003	1.507
BEGIN HCFDL	2	63.056	13.647	-0.021	1.507-4.635	0.374	1.126-0.094	3.607	0.003	1.507
104 QF	16	63.308	13.183	1.836	1.510-4.459	1.015	1.082-0.250	3.753	-0.588	1.518
105 S3	12	63.608	12.107	1.736	1.513-4.154	1.015	1.007-0.250	4.140	-0.696	1.530
106 BEND	12	66.008	5.467	0.995	1.561-2.498	0.356	0.602-0.084	9.558	-1.552	1.592
107 S5H	11	66.558	4.478	0.794	1.579-2.302	0.356	0.555-0.084	11.382	-1.749	1.601
108 CT	15	66.658	4.323	0.758	1.582-2.266	0.356	0.547-0.084	11.737	-1.785	1.602
109 S3H	7	67.208	3.835	0.630	1.596-2.141	0.356	0.517-0.084	13.035	-1.911	1.607
110 QD	16	67.260	3.675	0.013	1.607-2.090	0.050	0.505-0.011	13.529	-0.017	1.610
END HCFDL	2	67.260	3.675	0.013	1.607-2.090	0.050	0.505-0.011	13.529	-0.017	1.610
END B4S	1	67.260	3.675	0.013	1.607-2.090	0.050	0.505-0.011	13.529	-0.017	1.610
END RING	1	201.780	3.674	0.013	4.821-2.090	0.050	0.505-0.011	13.533	-0.017	4.828
TOTAL LENGTH =					QX, QX,			4.821234 QY, QY,		4.828163
ALFA	=				BETAX(MAX)	=		-0.199795	=	0.373762
GAMMA(TR)	=				DX(MAX)	=		13.767548	=	13.865950
					XCO(MAX)	=		2.981590	=	0.000000
					XCO(R.M.S.)	=		11.866382	=	0.000000
								6.673468	=	0.000000

... SEARCHING FOR CLOSED ORBIT FOR BEAM LINE "RING", DELTA(P)/P = -0.002000, SYMM = F
... ITER : X = 0.412897E-01
... GAMMA(TR) = 4.921294
... 1 -0.001063
... 2 -0.001063
... 3 -0.001063

Page 3

TABLE IV

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
DELTA(P)/P = -0.002000 SYMM = F

ELEMENT SEQUENCE			HORIZONTAL ALIGNMENT			VERTICAL		
POS.	ELEMENT OCC.	DIST	BETAX	ALFAX	MUX	X(CO)	PX(CO)	MUY
NO.	NAME	[M]	[L]	[L]	[L2P1]	[MM]	[L.001]	[MM]
BEGIN	RING	1	0.000	0.011	0.000	-1.063	0.027	0.000
BEGIN	B4S	3.659	0.011	0.003	-1.063	0.027	0.523-0.013	13.584-0.008
BEGIN	HCDF	3.659	0.011	0.003	-1.063	0.027	0.523-0.013	13.585-0.008
55	QD	3.806	-0.602	0.814	-1.075	-0.127	0.529-0.0063	13.102-1.895
56	S3	3.4182	4.201	0.826	-1.113	-0.127	0.548-0.0063	11.995-1.790
57	BEND	7	36.582	9.474	-1.462	0.888	-1.820	0.229
58	S5H	6	37.132	11.186	-1.644	0.897	-2.073	0.459
59	CT	8	37.232	11.519	-1.678	0.898	-2.119	0.459
60	SXF	3	37.332	11.859	-1.714	0.899	-2.165	0.459
61	S2H	5	37.582	12.739	-1.797	0.903	-2.280	0.459
62	QF	9	37.827	13.199	-1.797	0.906	-2.355	0.459
END	HCDF	3	37.834	13.199	-0.004	0.906	-2.355	0.132
BEGIN	HCFD	3	37.834	13.199	-0.004	0.906	-2.355	0.132
63	QF	10	38.086	12.743	1.790	0.909	-2.346	0.199
64	S3	6	38.386	11.697	1.690	0.913	-2.195	0.199
65	BEND	8	40.786	15.954	0.962	-2.195	0.137-0.097	4.137-0.230
66	S5H	7	41.336	4.334	0.755	0.980	-2.263	0.170-0.229
67	CT	9	41.436	4.187	0.718	0.984	-2.275	0.170-0.230
68	SXD	3	41.536	4.045	0.690	0.988	-2.287	0.174-0.230
69	S2H	6	41.786	3.723	0.758	0.998	-2.318	0.174-0.230
70	QD	10	42.037	3.575	-0.005	1.009	-2.391	0.461-0.664
END	HCFD	3	42.037	3.575	-0.005	1.009	-2.391	0.132-0.664
BEGIN	HCDFO	2	42.037	3.575	-0.005	1.009	-2.391	0.132-0.664
71	QD	11	42.289	3.728	-0.608	1.020	-2.552	0.121-0.662
72	S32H	3	45.539	11.586	-1.805	1.033	-5.216	0.121-0.662
73	CT	10	45.639	11.951	-1.842	1.044	-5.298	0.121-0.662
74	S3H	4	45.98	13.288	-1.971	1.109	-5.818	0.411-0.662
75	QF	11	46.241	13.816	-0.099	1.112	-5.692	0.023-0.662
END	HCDFO	12	46.241	13.816	-0.099	1.112	-5.692	0.012-0.662
BEGIN	HCFD	4	46.241	13.385	-1.978	1.115	-5.597	0.773-0.388
76	QF	12	46.493	12.339	1.693	1.118	-5.364	0.773-0.388
77	S3H	9	46.793	5.807	1.000	1.164	-3.857	0.479-0.240
78	BEND	9	49.193	4.810	0.810	1.181	-3.593	0.479-0.240
79	S5H	8	49.743	4.810	0.651	1.184	-3.454	0.479-0.240
80	CT	11	49.843	4.943	0.754	1.187	-3.497	0.484-0.240
81	SXD	4	50.69	4.130	0.643	1.217	-3.375	0.483-0.240
82	S2H	7	50.193	4.141	0.667	1.197	-3.375	0.483-0.240
83	QD	12	50.445	3.972	0.611	1.207	-3.314	0.600-0.002
END	HCFD	4	50.445	3.972	0.611	1.207	-3.314	0.600-0.002
BEGIN	HCDFL	1	50.445	3.972	0.611	1.207	-3.314	0.600-0.002
84	QD	13	50.695	4.130	-0.643	1.217	-3.375	0.483-0.240
85	S3	10	50.997	4.548	-0.746	1.228	-3.520	0.483-0.240
86	BEND	10	53.397	9.901	-1.461	1.286	-5.043	0.781-0.391
87	S5H	9	53.947	11.608	-1.636	1.294	-5.473	0.781-0.391
88	CT	12	54.047	11.939	-1.667	1.295	-5.551	0.781-0.391
89	S3H	15	54.397	13.147	-1.778	1.300	-5.825	0.781-0.391
90	QF	13	54.649	13.583	-0.918	1.303	-5.918	0.781-0.391
END	HCDFL	1	54.649	13.583	-0.973	1.303	-5.918	0.781-0.391

"MAD" VERSION: 6.01/03

RUN: 19-NOV-8 08:07:18

PAGE 1

TABLE IV e

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8
 LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
 PAGE 2
 $\Delta(p)/p = -0.02000$
 $\text{SYMM} = \text{F}$

POS. NO.	ELEMENT NAME NO.	SEQUENCE	DIST [M]	H O R I Z O N T A L				V E R T I C A L							
				BETAX [1]	ALFAX [1]	MUX [CO] [L2P11] [MM]	PX(CO) [L.0011]	DX [M]	DPX [11]	I [M]	BETAY [1]	ALFAY [1]	MUY [CO] [C2P11] [MM]	DY [L.0011]	DPY [11]
BEGIN	HCFDO	2	54.649	13.583	0.073	1.303	-5.918	0.047	2.967-0.025	3.713	0.006	0.000	0.000	0.000	0.000
91	QF	14	54.901	13.075	1.915	1.306	-5.802	0.874	2.908-0.439	3.860	-0.597	1.316	0.000	0.000	0.000
92	S32H	4	58.151	4.389	0.753	1.376	-2.957	0.874	1.476-0.439	11.478	-1.742	1.398	0.000	0.000	0.000
93	CT	13	58.251	4.242	0.717	1.380	-2.869	0.874	1.432-0.439	11.830	-1.777	1.399	0.000	0.000	0.000
94	S3H	6	58.601	3.783	0.592	1.394	-2.563	0.874	1.278-0.439	13.120	-1.900	1.403	0.000	0.000	0.000
95	QD	14	58.852	3.640	-0.019	1.405	-2.388	0.516	1.190-0.260	13.604	0.006	1.406	0.000	0.000	0.000
END	HCFDO	2	58.852	3.640	-0.019	1.405	-2.388	0.516	1.190-0.260	13.604	0.006	1.406	0.000	0.000	0.000
BEGIN	HCDF	4	58.852	3.640	-0.019	1.405	-2.388	0.516	1.190-0.260	13.604	0.006	1.406	0.000	0.000	0.000
96	QD	15	59.104	3.802	-0.631	1.416	-2.301	0.177	1.146-0.092	13.114	1.911	1.409	0.000	0.000	0.000
97	S3	11	59.404	4.215	-0.742	1.428	-0.177	0.177	1.18-0.092	11.997	1.805	1.413	0.000	0.000	0.000
98	BEND	11	61.804	9.695	-1.517	1.489	-2.210	-0.145	1.092-0.070	5.360	0.954	1.452	0.000	0.000	0.000
99	SSB	10	62.354	11.474	-1.704	1.497	-2.290	-0.145	1.130-0.070	4.446	0.758	1.480	0.000	0.000	0.000
100	CT	14	62.454	11.819	-1.738	1.499	-2.304	-0.145	1.137-0.070	4.268	0.722	1.483	0.000	0.000	0.000
101	SXF	4	62.554	12.171	-1.776	1.500	-2.319	-0.146	1.144-0.070	4.127	0.688	1.487	0.000	0.000	0.000
102	S2H	8	62.804	13.082	-1.862	1.503	-2.315	-0.146	1.162-0.070	3.805	0.598	1.497	0.000	0.000	0.000
103	QF	15	63.056	13.563	-0.019	1.506	-2.350	-0.146	1.162-0.070	3.655	0.595	1.508	0.000	0.000	0.000
END	HCDF	4	63.056	13.563	-0.019	1.506	-2.350	-0.146	1.159-0.093	3.655	0.595	1.508	0.000	0.000	0.000
BEGIN	HCFDL	2	63.056	13.563	-0.019	1.506	-2.350	-0.146	1.159-0.093	3.655	0.595	1.508	0.000	0.000	0.000
104	QF	16	63.308	13.101	1.826	1.509	-2.262	0.511	1.115-0.254	3.803	-0.595	1.519	0.000	0.000	0.000
105	S3	12	63.608	12.033	1.727	1.513	-2.108	0.511	1.038-0.254	4.194	-0.702	1.531	0.000	0.000	0.000
106	BEND	12	66.008	5.436	0.991	1.561	-1.272	0.183	0.625-0.089	9.622	-1.555	1.593	0.000	0.000	0.000
107	SSB	11	66.558	4.455	0.790	1.578	-1.171	0.183	0.576-0.089	11.444	-1.751	1.601	0.000	0.000	0.000
108	CT	15	66.658	4.301	0.753	1.582	-1.153	0.183	0.567-0.089	11.798	-1.786	1.602	0.000	0.000	0.000
109	S3H	7	67.008	3.817	0.625	1.596	-1.089	0.183	0.535-0.089	13.094	-1.911	1.607	0.000	0.000	0.000
110	QD	16	67.260	3.658	0.011	1.607	-1.063	0.027	0.523-0.013	13.585	-0.008	1.610	0.000	0.000	0.000
END	HCFDL	2	67.260	3.658	0.011	1.607	-1.063	0.027	0.523-0.013	13.585	-0.008	1.610	0.000	0.000	0.000
END	B4S	1	67.260	3.658	0.011	1.607	-1.063	0.027	0.523-0.013	13.585	-0.008	1.610	0.000	0.000	0.000
END	RING	1	201.780	3.658	0.011	4.820	-1.063	0.027	0.523-0.013	13.586	-0.008	4.830	0.000	0.000	0.000
TOTAL LENGTH =			201.7800000			QX	=	QX	=	4.829541					
ALFA	=		0.416347E-01			BETAX(MAX)	=	QY,	=	0.186378					
GAMMA(TR)	=		4.9008558			DX(MAX)	=	QY,	=	13.751647					
ITER	i		0.0000000			XCO(MAX)	=	QY,	=	0.00000000					
						XCO(R.M.S.)	=	QY,	=	0.00000000					
... SEARCHING FOR CLOSED ORBIT FOR BEAM LINE "RING"						Y		Y		Y					
... ITER	i														
... ...															

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
SYMM = F
DELTA(P)/P = 0.000000

TABLE IV 4

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18 PAGE 1									
ZOHREH PARSA /									
HORIZONTAL LATTICE									
ELEMENT SEQUENCE	DIST	BETAX	ALFAX	HORIZONTAL MUX	X(CO)	PX(CO)	DX	DPX	I
POS. ELEMENT NO.	[M]	[M]	[L]	[L]	[MM]	[MM]	[M]	[M]	[I]
BEGIN RING	1	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
BEGIN B4S	1	33.630	0.009	0.803	0.000	0.000	0.540-0.015	13.644	0.000
BEGIN HCDF	3	33.630	0.009	0.803	0.000	0.000	0.540-0.015	13.644	0.000
55 QD	9	33.882	3.789	-0.602	0.814	0.000	0.546-0.064	13.157	1.912
56 S3	7	34.182	4.183	-0.710	0.826	0.000	0.565-0.064	12.041	1.806
57 BEND	7	36.582	9.447	-1.461	0.888	0.000	0.918-0.229	15.413	0.000
58 S5H	6	37.132	11.154	-1.643	0.897	0.000	1.045-0.229	4.467	0.762
59 CT	8	37.232	11.486	-1.676	0.898	0.000	1.068-0.229	4.319	0.727
60 SXF	3	37.332	11.825	-1.710	0.900	0.000	1.090-0.229	4.177	0.691
61 S2H	5	37.582	12.700	-1.793	0.903	0.000	1.148-0.229	3.853	0.812
62 QF	9	37.834	13.158	-0.005	0.906	0.000	1.185-0.065	3.703	0.895
END HCDF	3	37.834	13.158	-0.005	0.906	0.000	1.185-0.065	3.703	0.878
BEGIN HCDF	3	38.086	12.705	1.783	0.909	0.000	1.180-0.102	3.853	0.881
63 QF	10	38.386	11.665	1.685	0.913	0.000	1.180-0.102	3.853	0.885
64 S3	8	40.786	15.266	0.954	0.962	0.000	1.098-0.059	9.687	0.996
65 BEND	8	41.336	4.326	0.755	0.981	0.000	1.131-0.059	11.508	0.996
66 S5H	7	41.436	4.178	0.719	0.984	0.000	1.136-0.059	11.862	0.996
67 CT	9	41.536	4.038	0.682	0.988	0.000	1.142-0.059	12.223	0.916
68 SXD	3	41.786	3.720	0.592	0.998	0.000	1.157-0.102	0.799	0.928
69 S2H	6	42.037	3.575	-0.011	1.009	0.000	1.098-0.059	9.687	0.989
70 QD	10	42.037	3.575	-0.011	1.009	0.000	1.131-0.059	11.508	0.996
END HCDF	3	42.037	3.575	-0.011	1.009	0.000	1.131-0.059	11.752	0.997
BEGIN HCDO	2	42.289	3.731	-0.615	1.021	0.000	1.136-0.059	11.788	0.999
71 QD	11	42.289	3.731	-0.615	1.021	0.000	1.142-0.059	1.823	0.999
72 S32H	3	45.539	11.993	-1.852	1.03	0.000	1.059-0.059	13.157	1.912
73 CT	18	45.639	11.993	-1.852	1.03	0.000	1.193-0.229	13.644	0.000
74 S3H	4	45.989	13.335	-1.981	1.108	0.000	1.193-0.229	11.862	0.000
75 QF	11	46.241	13.866	-0.102	1.111	0.000	1.193-0.229	13.644	0.000
END HCDO	2	46.241	13.866	-0.102	1.111	0.000	1.193-0.407	13.157	1.912
BEGIN HCDF	4	46.241	13.866	-0.102	1.111	0.000	1.273-0.407	0.799	0.000
76 QF	12	46.493	13.435	1.102	1.103	0.000	2.635-0.407	4.467	0.762
77 S3	9	46.793	12.389	1.697	1.114	0.000	2.635-0.407	4.319	0.727
78 BEND	9	49.193	15.820	1.012	1.163	0.000	2.778-0.407	3.853	0.603
79 S5H	8	49.743	4.812	0.821	1.180	0.000	2.831-0.011	3.703	0.000
80 CT	11	49.843	4.651	0.786	1.183	0.000	2.831-0.011	1.009	0.000
81 SXD	4	49.943	4.498	0.751	1.187	0.000	2.784-0.385	3.853	0.000
82 S2H	7	50.193	4.144	0.664	1.196	0.000	2.669-0.385	4.247	0.709
83 QD	12	50.445	3.976	0.008	1.206	0.000	1.919-0.239	9.687	1.558
END HCDF	4	50.445	3.976	0.008	1.206	0.000	1.787-0.239	11.508	1.752
BEGIN HCDFL	1	50.445	3.976	0.008	1.206	0.000	1.763-0.239	11.862	1.207
84 QD	13	50.697	4.135	-0.646	1.216	0.000	1.740-0.239	12.223	1.821
85 S3	10	50.997	4.553	-0.749	1.227	0.000	1.680-0.239	13.157	1.912
86 BEND	10	53.397	9.894	-1.453	1.285	0.000	1.650-0.002	1.207	0.000
87 S5H	9	53.947	11.588	-1.627	1.293	0.000	1.650-0.002	1.207	0.000
88 CT	12	54.047	11.916	-1.658	1.294	0.000	1.650-0.002	1.207	0.000
89 S3H	5	54.397	13.115	-1.768	1.299	0.000	1.681-0.242	13.157	1.912
90 QF	13	54.649	13.546	0.079	1.302	0.000	1.721-0.242	1.214	0.000
END HCDFL	1	54.649	13.546	0.079	1.302	0.000	1.721-0.242	1.214	0.000

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
DELTA(P)/P = $\theta .0000000$
SYMM = F

TABLE IV f

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18

PAGE 2

POS. NO.	ELEMENT OCC. NAME NO.	ELEMENT SEQUENCE	DIST [M]	BETAX [1]	ALFAX [1]	HORIZONTAL [2PI]	MUX [1]	PX(CO) [MM]	DX [M]	DPX [1]	1 BETAY [1]	ALFY [M]	1 MUY [2PI]	VERITICAL [MM]	PY(CO) [MM]	DY [M]	DPY [1]
BEGIN HCFDO	2	54.649	13.546	.0.079	1.302	.0.000	.0.000	2.951-0.0223	3.703	.0.000	1.308	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
91 QF	14	54.901	13.038	1.915	1.305	.0.000	.0.000	2.894-0.435	3.853	-0.603	1.319	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
92 S32H	4	58.151	4.371	0.752	1.376	.0.000	.0.000	1.481-0.435	11.508	-1.752	1.400	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
93 CT	13	58.251	4.224	0.716	1.379	.0.000	.0.000	1.437-0.435	11.862	-1.788	1.401	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
94 S3H	6	58.601	3.767	0.590	1.393	.0.000	.0.000	1.285-0.435	13.157	-1.912	1.406	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
95 QD	14	58.852	3.624	-0.018	1.404	.0.000	.0.000	1.198-0.255	13.644	.0.000	1.409	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
END HCFDO	2	58.852	3.624	-0.018	1.404	.0.000	.0.000	1.198-0.255	13.644	.0.000	1.409	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
BEGIN HCDF	4	58.852	3.624	-0.018	1.404	.0.000	.0.000	1.198-0.255	13.644	.0.000	1.409	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
96 QD	15	59.104	3.785	-0.628	1.415	.0.000	.0.000	1.156-0.085	13.157	.0.000	1.412	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
97 S3	11	59.404	4.195	-0.739	1.427	.0.000	.0.000	1.130-0.085	12.041	1.806	1.416	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
98 BEND	11	61.804	9.644	-1.509	1.488	.0.000	.0.000	1.130-0.085	5.413	0.956	1.464	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
99 S5H	10	62.354	11.407	-1.695	1.497	.0.000	.0.000	1.118-0.075	5.413	0.956	1.481	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
100 CT	14	62.454	11.749	-1.729	1.498	.0.000	.0.000	1.167-0.075	4.319	0.727	1.485	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
101 SXF	4	62.554	12.098	-1.763	1.439	.0.000	.0.000	1.175-0.075	4.177	0.691	1.489	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
102 S2H	8	62.804	13.001	-1.848	1.503	.0.000	.0.000	1.193-0.075	3.853	0.603	1.499	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
103 QE	15	63.056	13.477	-0.017	1.506	.0.000	.0.000	1.191-0.093	3.703	0.603	1.509	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
END HCDF	4	63.056	13.477	-0.017	1.506	.0.000	.0.000	1.191-0.093	3.703	0.603	1.509	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
BEGIN HCFDL	2	63.056	13.477	-0.017	1.506	.0.000	.0.000	1.191-0.093	3.703	0.603	1.509	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
104 QE	16	63.308	13.018	1.816	1.509	.0.000	.0.000	1.147-0.258	3.853	-0.603	1.520	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
105 S3	12	63.608	11.959	1.717	1.512	.0.000	.0.000	1.076-0.258	4.247	-0.709	1.532	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
106 BEND	12	66.008	5.405	0.986	1.560	.0.000	.0.000	0.647-0.094	9.687	-1.558	1.593	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
107 S5H	11	66.558	4.431	0.785	1.578	.0.000	.0.000	0.596-0.094	11.508	-1.752	1.601	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
108 CT	15	66.658	4.278	0.749	1.582	.0.000	.0.000	0.586-0.094	11.862	-1.788	1.603	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
109 S3H	7	67.008	3.798	0.621	1.595	.0.000	.0.000	0.544-0.094	13.157	-1.912	1.607	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
110 QD	16	67.260	3.642	0.009	1.607	.0.000	.0.000	0.540-0.015	13.644	.0.000	1.610	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
END HCFDL	2	67.260	3.642	0.009	1.607	.0.000	.0.000	0.540-0.015	13.644	.0.000	1.610	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
END B4S	1	67.260	3.642	0.009	1.607	.0.000	.0.000	0.540-0.015	13.644	.0.000	1.610	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
END RING	1	201.780	3.642	0.009	4.820	.0.000	.0.000	0.540-0.015	13.644	.0.000	4.830	.0.000	.0.000	.0.000	.0.000	.0.000	.0.000
TOTAL LENGTH =					QX,*	=		4.8200000	QY,*	=					4.829999		
ALFA	=				BETAX(MAX)	=		0.001048	BETAY(MAX)	=					-0.001678		
GAMMA(TR)	=				DX(MAX)	=		13.865707	DY(MAX)	=					13.644032		
					XCO(MAX)	=		2.951449	YCO(MAX)	=					0.0000000		
					XCO(R.M.S.)	=		0.0000000	YCO(R.M.S.)	=					0.0000000		

... SEARCHING FOR CLOSED ORBIT FOR BEAM LINE "RING"																		
... ITER:	X	0.001097	PX	0.0000032	V	0.0000000		0.0000000	PY	0.0000000								
... 1		0.001097	-0.881238	-0.0000031		0.0000000		0.0000000	2.951449							0.0000000		
... 2		0.001097	-0.0000031	-0.0000031		0.0000000		0.0000000	0.0000000							0.155487E-05		
... 3		0.001097	-0.0000031	-0.0000031		0.0000000		0.0000000	0.0000000							0.347445E-11		

Page 35

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
DELTA(P)/P = 0.002000 SYMM = F

TABLE IV 3

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18 PAGE 1

POS. ELEMENT OCC. NO.	ELEMENT NAME	DIST [M]	I	HORIZONTAL			VERTICAL			I BETAY [M]	I ALFAY [M]	I DPY [M]
				BETAX [1]	ALFAX [1]	MUX [2P1]	PX(CO) [MM]	DX [M]	PY(CO) [MM]			
BEGIN RING	1	0.000	3.624	0.0007	0.000	1.097	-0.031	0.557-0.017	13.706	0.0008	0.000	0.000
BEGIN B4S	1	33.630	3.624	0.0007	0.803	1.097	-0.031	0.557-0.017	13.706	0.0008	0.000	0.000
BEGIN HCDF	3	33.630	3.624	0.0007	0.803	1.097	-0.031	0.557-0.017	13.706	0.0008	0.000	0.000
55 QD	9	33.882	3.772	-0.602	0.814	1.110	0.128	0.563-0.064	13.213	1.928	0.000	0.000
56 S3	7	34.182	4.165	-0.710	0.826	1.148	0.128	0.583-0.064	12.091	1.821	0.000	0.000
57 BEND	7	36.582	9.419	-1.460	0.888	1.853	0.459	0.935-0.229	5.420	0.964	0.860	0.000
58 S5H	6	37.132	11.121	-1.642	0.897	2.105	0.459	1.060-0.229	4.469	0.769	0.877	0.000
59 CT	8	37.232	11.452	-1.675	0.898	2.151	0.459	1.083-0.229	4.319	0.733	0.881	0.000
60 SXF	3	37.332	11.790	-1.705	0.900	2.197	0.459	1.106-0.229	4.177	0.696	0.885	0.000
61 S2H	5	37.582	12.661	-1.788	0.903	2.311	0.459	1.163-0.229	3.851	0.608	0.895	0.000
62 QF	9	37.834	13.117	-0.906	0.906	2.385	0.127	1.200-0.062	3.699	0.005	0.000	0.000
END HCDF	3	37.834	13.117	-0.906	0.906	2.385	0.127	1.200-0.062	3.699	0.005	0.000	0.000
BEGIN HCDF	3	38.086	12.667	-1.777	0.909	2.375	-0.208	1.194-0.106	3.62	0.005	0.000	0.000
63 QF	10	38.086	12.667	-1.777	0.909	2.375	-0.208	1.194-0.106	3.62	0.005	0.000	0.000
64 S3	8	38.386	11.632	1.679	0.913	2.313	-0.208	1.163-0.106	4.235	-0.702	0.928	0.000
65 BEND	8	40.786	15.255	0.954	0.962	1.993	0.127	1.200-0.062	3.632	-1.552	0.989	0.000
66 S5H	7	41.336	4.317	0.755	0.981	2.259	0.127	1.129-0.054	11.442	-1.746	0.995	0.000
67 CT	9	41.436	4.170	0.719	0.984	2.271	0.112	1.134-0.054	11.794	-1.781	0.995	0.000
68 SXD	3	41.536	4.031	0.675	0.988	2.282	0.115	1.140-0.056	12.151	-1.794	1.000	0.000
69 S2H	6	41.786	3.717	0.585	0.999	2.310	0.115	1.153-0.056	13.055	0.668	-1.881	0.000
70 QD	10	42.037	3.576	-0.017	0.910	2.382	0.454	1.188-0.225	13.542	0.017	1.006	0.000
END HCDF	3	42.037	3.576	-0.017	0.910	2.382	0.454	1.188-0.225	13.542	0.017	1.006	0.000
BEGIN HCDF0	2	42.037	3.576	-0.017	0.910	2.382	0.454	1.188-0.225	13.542	0.017	1.006	0.000
71 QD	11	42.289	3.734	-0.621	1.021	2.540	0.809	1.267-0.402	13.051	1.913	1.009	0.000
72 S32H	3	45.639	11.667	-1.825	1.102	2.540	0.809	1.267-0.402	13.051	1.913	1.009	0.000
73 CT	10	45.639	12.035	-1.862	1.010	2.545	0.809	1.267-0.402	13.051	1.913	1.009	0.000
74 S3H	14	45.989	13.381	-1.991	1.108	5.528	0.809	2.609-0.492	4.248	0.719	1.083	0.000
75 QF	11	46.241	13.915	-0.106	1.111	5.633	0.822	2.749-0.492	3.789	0.595	1.097	0.000
END HCDF0	2	46.241	13.915	-0.106	1.111	5.633	0.822	2.801-0.011	3.642	0.000	0.000	0.000
76 QD	4	46.241	13.915	-0.106	1.111	5.633	0.822	2.801-0.011	3.642	0.000	0.000	0.000
BEGIN HCDF	4	46.493	13.945	-0.606	1.114	5.633	0.822	2.801-0.011	3.642	0.000	0.000	0.000
77 QF	12	46.493	13.945	-0.606	1.114	5.633	0.822	2.801-0.011	3.642	0.000	0.000	0.000
78 BEND	9	46.793	12.439	1.700	1.118	5.310	-0.765	2.755-0.381	3.790	-0.595	1.119	0.000
79 S5H	8	49.193	5.833	1.024	1.163	3.818	-0.476	1.899-0.238	9.667	-1.569	1.192	0.000
80 CT	11	49.743	4.815	0.831	1.179	3.557	-0.476	1.769-0.238	11.448	-1.767	1.201	0.000
81 SXD	7	49.943	4.652	0.796	1.183	3.557	-0.476	1.746-0.238	11.805	-1.803	1.202	0.000
82 S2H	7	50.193	4.485	1.794	1.186	3.462	-0.471	1.722-0.233	11.216	-1.804	1.203	0.000
83 QD	12	50.445	3.980	0.006	1.205	3.286	0.008	1.636-0.006	13.077	1.910	1.213	0.000
END HCDF	4	50.445	3.980	0.006	1.205	3.286	0.008	1.636-0.006	13.077	1.910	1.213	0.000
BEGIN HCDFL	1	50.445	3.980	0.006	1.205	3.286	0.008	1.636-0.006	13.077	1.910	1.213	0.000
84 QD	13	50.697	4.146	-0.649	1.215	3.348	0.487	1.667-0.244	1.207	-1.892	1.216	0.000
85 S3	18	50.997	4.559	-0.752	1.226	3.494	0.487	1.740-0.244	11.965	1.803	1.226	0.000
86 BEND	10	53.397	9.887	-1.446	1.284	5.016	0.780	2.501-0.390	5.380	0.946	1.265	0.000
87 S5H	9	53.947	11.568	-1.617	1.292	5.444	0.780	2.715-0.390	4.447	0.753	1.283	0.000
88 CT	12	54.047	11.894	-1.648	1.293	5.522	0.780	2.754-0.390	4.301	0.718	1.286	0.000
89 S3H	13	54.397	13.083	-1.757	1.298	5.795	0.780	2.890-0.390	3.842	0.595	1.300	0.000
90 QF	13	54.649	13.509	-0.043	1.301	5.888	-0.043	2.936-0.021	3.696	-0.006	1.311	0.000
END HCDFL	1	54.649	13.509	-0.043	1.301	5.888	-0.043	2.936-0.021	3.696	-0.006	1.311	0.000

TABLE IV]

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
DELTA(P)/P = 0.002000 SYMM = F

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18
PAGE 2

ELEMENT SEQUENCE	POS. ELEMENT OCC.	DIST [M]	BETAX [M]	ALFAX [1]	HORIZ ON T A L MUX X(CO) [MM]	PX(CO) [MM]	DX [M]	OPX [1]	I BETAY [M]	ALFAY [1]	MUY [L] [ZPI]	PY(CO) [MM]	DY [L] [MM]	DPY [1]
BEGIN HCFDO	2	54.649	13.509	0.0885	1.301	5.888	-0.043	2.936-0.021	3.696	-0.006	1.311	0.000	0.000	0.000
91 QF	14	54.901	13.000	1.916	1.304	5.773	-0.866	2.879-0.431	3.849	-0.609	1.321	0.000	0.000	0.000
92 S32H	4	58.151	4.352	0.751	1.375	2.965	-0.866	1.485-0.431	1.542	-1.763	1.402	0.000	0.000	0.000
93 CT	13	58.251	4.206	0.715	1.379	2.879	-0.866	1.442-0.431	1.897	-1.799	1.404	0.000	0.000	0.000
94 S3H	6	58.601	3.750	0.589	1.393	2.577	-0.866	1.292-0.431	1.197	-1.923	1.408	0.000	0.000	0.000
95 QD	14	58.852	3.608	-0.017	1.404	2.404	-0.506	1.207-0.250	13.688	-0.006	1.411	0.000	0.000	0.000
END HCFDO	12	58.852	3.608	-0.017	1.404	2.405	-0.506	1.207-0.250	13.688	-0.006	1.411	0.000	0.000	0.000
BEGIN HCDF	4	58.852	3.608	-0.017	1.404	2.405	-0.506	1.207-0.250	13.688	-0.006	1.411	0.000	0.000	0.000
96 QD	15	59.104	3.767	-0.625	1.414	2.321	-0.164	1.165-0.079	13.203	1.913	1.414	0.000	0.000	0.000
97 S3	11	59.404	4.175	-0.736	1.426	2.272	-0.164	1.142-0.079	12.089	1.807	1.418	0.000	0.000	0.000
98 BEND	11	61.804	9.589	-1.588	1.498	2.262	-0.156	1.144-0.081	15.465	0.959	1.465	0.000	0.000	0.000
99 S5H	10	62.354	11.338	-1.687	1.496	2.348	-0.156	1.189-0.081	4.519	0.766	1.483	0.000	0.000	0.000
100 CT	14	62.454	11.678	-1.720	1.498	2.364	-0.156	1.197-0.081	4.369	0.731	1.486	0.000	0.000	0.000
101 SXF	4	62.554	12.025	-1.750	1.499	2.379	-0.156	1.205-0.080	4.227	0.695	1.490	0.000	0.000	0.000
102 S2H	8	62.804	12.919	-1.835	1.502	4.418	-0.156	1.225-0.080	3.902	0.607	1.500	0.000	0.000	0.000
103 QF	15	63.056	13.390	-0.016	1.505	2.414	-0.185	1.223-0.092	3.752	-0.001	1.510	0.000	0.000	0.000
END HCDF	4	63.056	13.390	-0.016	1.505	2.414	-0.185	1.223-0.092	3.752	-0.001	1.510	0.000	0.000	0.000
BEGIN HCFDL	2	63.056	13.390	-0.016	1.505	2.414	-0.185	1.223-0.092	3.752	-0.001	1.510	0.000	0.000	0.000
104 QF	16	63.308	12.934	1.806	1.508	2.326	-0.519	1.179-0.261	3.903	-0.610	1.521	0.000	0.000	0.000
105 S3	12	63.608	11.883	1.707	1.512	2.170	-0.519	1.101-0.261	4.307	-0.607	1.533	0.000	0.000	0.000
106 BEND	12	66.008	5.373	0.981	1.560	1.317	-0.192	0.669-0.098	9.754	-1.562	1.593	0.000	0.000	0.000
107 S5H	11	66.558	4.406	0.780	1.578	1.211	-0.192	0.616-0.098	11.574	-1.755	1.601	0.000	0.000	0.000
108 CT	15	66.558	4.254	0.744	1.582	1.192	-0.192	0.606-0.098	11.928	-1.790	1.603	0.000	0.000	0.000
109 S3H	7	67.008	3.779	0.616	1.596	1.125	-0.192	0.572-0.098	13.221	-1.913	1.607	0.000	0.000	0.000
110 QD	16	67.260	3.624	0.007	1.607	1.097	0.097	0.557-0.017	13.706	0.008	1.610	0.000	0.000	0.000
END HCFDL	2	67.260	3.624	0.007	1.607	1.097	0.097	0.557-0.017	13.706	0.008	1.610	0.000	0.000	0.000
END B4S	1	67.260	3.624	0.007	1.607	1.097	0.097	0.557-0.017	13.706	0.008	1.610	0.000	0.000	0.000
END RING	1	201.780	3.624	0.007	4.820	1.097	0.097	0.557-0.017	13.707	0.008	4.830	0.000	0.000	0.000
TOTAL LENGTH =		201.7800000			QX,	=	=	4.820310	QY,	=	=	4.829533		
ALFA =		0.422958E-01			BETAX(MAX)	=	=	0.096209	BETAY(MAX)	=	=	-0.190458		
GAMMA(TR) =		4.862407			DX(MAX)	=	=	13.914840	DY(MAX)	=	=	13.707415		
					XCO(MAX)	=	=	2.936023	VCO(MAX)	=	=	0.000000		
					XCO(R.M.S.)	=	=	5.887512	VCO(R.M.S.)	=	=	0.000000		
								3.324695				0.000000		
... SEARCHING FOR CLOSED ORBIT FOR BEAM LINE "RING"					Y									
... ITER:	X	0.002228	-0.000068											
... 1		0.002229	-0.000066											
... 2		0.002229	-0.000066											
... 3		0.002229	-0.000066											

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18

TABLE IV 6

AGS BOOSTER LATTICE FOR SURVEY
 LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
 $\Delta(P)/P = \frac{0.004}{0.004}$
 $\text{SYMM} = F$

POS. ELEMENT OCC. NO.	ELEMENT SEQUENCE NAME	DIST [M]	I BETAX [M]	I ALFAX [1]	H OR I Z ON T A L X(CO) [2P11]	MUX [NMM] [MM]	DPX [M]	I DX [1]	I DPY [M]	VER T I C A L	
										PY(CO) [MM]	DY [M]
BEGIN RING	1	0.000	3.607	0.005	0.000	2.229	-0.066	0.575-0.019	13.769	0.016	0.000
BEGIN B4S	1	33.630	3.606	0.005	0.803	2.229	-0.066	0.575-0.019	13.770	0.016	0.000
BEGIN HCDF	3	33.630	3.606	0.005	0.803	2.229	-0.066	0.575-0.019	13.770	0.016	0.000
55 QD	9	33.882	3.754	-0.602	0.814	2.253	0.580	0.065	13.273	1.944	0.000
56 S3	7	34.182	4.146	-0.710	0.826	2.330	0.580	0.065	12.143	1.837	0.000
57 BEND	7	34.582	9.389	-1.459	0.889	3.739	0.918	0.951	0.229	5.436	0.859
58 S5H	6	37.132	11.087	-1.641	0.897	4.242	0.918	0.951	0.229	4.473	0.875
59 CT	8	37.232	11.418	-1.674	0.899	4.333	0.918	0.999	0.229	4.322	0.740
60 SXF	3	37.332	11.754	-1.700	0.900	4.424	0.916	1.122	0.229	4.179	0.702
61 S2H	5	37.886	12.621	-1.783	0.903	4.653	0.916	1.178	0.229	3.851	0.894
62 QF	9	37.834	13.075	-0.006	0.906	0.250	1.214	0.660	3.697	0.613	0.000
END HCDF	3	37.834	13.075	-0.006	0.906	0.250	1.214	0.660	3.697	0.610	0.000
BEGIN HCFD	3	38.086	12.627	1.771	0.909	4.777	-0.425	1.208-0.111	3.697	0.916	0.000
63 QF	16	38.386	11.598	1.673	0.913	0.650	1.175-0.111	4.225	0.915	0.841	0.000
64 S3	8	40.786	15.475	0.955	0.963	4.397	-0.425	1.175-0.111	4.225	0.927	0.915
65 BEND	8	41.336	4.308	0.755	0.981	4.515	0.214	1.170-0.111	4.695	0.927	0.915
66 S5H	7	41.436	4.162	0.719	0.985	4.536	0.214	1.170-0.111	4.586	0.905	0.905
67 CT	9	41.536	4.024	0.668	0.989	4.558	0.223	1.137	0.053	1.000	0.000
68 SXD	3	41.786	3.713	0.578	0.999	4.613	0.223	1.150	0.053	1.000	0.000
69 S2H	6	42.037	3.576	0.523	0.991	4.754	0.900	1.184	0.221	1.003	0.000
70 QD	16	42.037	3.576	0.023	1.010	4.754	0.900	1.184	0.221	1.003	0.000
END HCFD	3	42.037	3.576	0.023	1.010	4.754	0.900	1.184	0.221	1.003	0.000
BEGIN HCDF0	2	42.037	3.576	0.023	1.010	4.754	0.900	1.184	0.221	1.003	0.000
71 QD	11	42.289	3.737	-0.628	1.021	5.068	1.609	1.261	0.398	1.000	0.000
72 S32H	13	45.339	11.707	-1.835	1.021	5.276	1.609	2.543	0.398	1.000	0.000
73 CT	18	45.639	12.877	-1.872	1.021	5.437	1.609	2.582	0.398	1.000	0.000
74 S3H	4	45.989	13.427	-2.002	1.028	5.998	1.609	2.720	0.398	1.000	0.000
75 QF	11	46.241	13.963	-0.110	1.111	2.006	0.044	2.772	0.110	3.581	0.000
END HCDF0	2	46.241	13.963	-0.110	1.111	2.006	0.044	2.772	0.110	3.581	0.000
BEGIN HCDF	4	46.241	13.963	-0.110	1.111	2.006	0.044	2.772	0.110	3.581	0.000
76 QF	12	46.493	13.535	1.797	1.141	0.019	-1.523	2.726-0.377	3.727	0.588	1.120
77 S3H	9	46.793	12.489	1.704	1.117	0.564	-1.523	2.613-0.377	4.110	0.587	1.320
78 BEND	9	49.193	5.847	1.036	1.162	7.597	-0.950	1.880-0.236	3.726	0.581	1.194
79 S5H	8	49.743	4.818	0.842	1.179	7.982	-0.950	1.751-0.236	1.130	1.000	1.203
80 CT	11	49.843	4.654	0.807	1.182	6.982	-0.950	1.728-0.236	1.130	1.000	1.109
81 QD	4	49.943	4.145	0.652	1.215	6.888	-0.931	1.705-0.227	1.107	1.000	1.204
END HCDFL	1	50.445	3.984	0.004	1.205	6.543	0.023	1.621	0.010	1.019	0.000
BEGIN HCDFL	1	50.445	3.984	0.004	1.205	6.543	0.023	1.621	0.010	1.019	0.000
82 S2H	7	50.943	4.145	-0.652	1.215	6.668	0.978	1.653	0.246	1.000	0.000
83 QD	12	50.445	3.984	0.004	1.205	6.543	0.023	1.621	0.010	1.019	0.000
END HCDFL	4	50.445	3.984	0.004	1.205	6.543	0.023	1.621	0.010	1.019	0.000
BEGIN HCDFL	1	50.445	3.984	0.004	1.205	6.543	0.023	1.621	0.010	1.019	0.000
84 QD	13	50.697	4.145	-0.652	1.215	6.668	0.978	1.653	0.246	1.000	0.000
85 S3	10	50.997	4.566	-0.755	1.225	6.961	0.978	1.648-0.227	1.018	-1.872	1.218
86 BEND	10	53.397	9.879	-1.438	1.283	10.004	1.560	2.487	0.390	1.430	1.267
87 S5H	9	53.947	11.547	-1.608	1.291	10.859	1.560	3.489	0.019	1.212	1.285
88 CT	12	54.047	11.870	-1.639	1.293	1.014	1.560	2.739	0.390	1.212	1.289
89 S3H	13	54.397	13.051	-1.747	1.293	1.155	1.560	2.874	0.390	1.300	1.302
90 QF	13	54.649	13.471	0.091	1.300	1.174	1.560	2.920-0.019	1.313	0.691	1.313
END HCDFL	1	54.649	13.471	0.091	1.300	1.174	1.560	2.920-0.019	1.313	0.691	1.313

TABLE IV A

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18
 LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
 ZOHREH PARSA /

POS.	ELEMENT OCC.	ELEMENT NAME	SEQUENCE NO.	DIST [M]	BETAX [1]	ALFAX [EM]	H ORIZON T AL MUX X(CO) PX(CO) DX [MM]	DPX [1] I	BETAY [1]	ALFAY [EM]	MUY [2PI] Y(CO) PY(CO) DY [MM]	DPY [1]		
BEGIN	HCFDO		2	54.649	13.471	0.091	1.300 11.744 -0.083	2.920-0.019	3.691 -0.013	1.313	0.000	0.000	0.000	
91	QF		14	54.901	12.961	1.916	1.303 11.517 -1.723	2.865-0.427	3.846 -0.615	1.324	0.000	0.000	0.000	
92	S32H		4	58.151	4.333	0.749	1.374 5.939 -1.723	1.489-0.427	11.580	-1.774	1.404	0.000	0.000	0.000
93	CT		13	58.251	4.187	0.714	1.378 5.768 -1.723	1.447-0.427	11.937	-1.810	1.406	0.000	0.000	0.000
94	S3H		6	58.601	3.733	0.588	1.392 5.167 -1.723	1.298-0.427	13.243	-1.935	1.410	0.000	0.000	0.000
95	QD		14	58.852	3.591	-0.016	1.403 4.826 -1.001	1.215-0.245	13.737	-0.011	1.413	0.000	0.000	0.000
END	HCFDO		2	58.852	3.591	-0.016	1.403 4.826 -1.001	1.215-0.245	13.737	-0.011	1.413	0.000	0.000	0.000
	HCDF		4	58.852	3.591	-0.016	1.403 4.826 -1.001	1.215-0.245	13.737	-0.011	1.413	0.000	0.000	0.000
BEGIN	QD		15	59.104	3.749	-0.622	1.414 4.662 -0.316	1.175-0.072	13.253	1.915	1.416	0.000	0.000	0.000
96	QD		11	59.404	4.154	-0.732	1.426 4.567 -0.316	1.154-0.072	12.140	1.816	1.420	0.000	0.000	0.000
97	S3		11	61.804	9.532	-1.492	1.488 4.577 0.323	1.170 0.086	5.519	0.962	1.467	0.000	0.000	0.000
98	BEND		10	62.354	11.269	-1.678	1.496 4.754 0.323	1.217 0.086	4.570	0.771	1.484	0.000	0.000	0.000
99	S5H		14	62.454	11.606	-1.711	1.497 4.786 0.323	1.226 0.086	4.420	0.736	1.488	0.000	0.000	0.000
100	CT		4	62.554	11.950	-1.737	1.499 4.818 0.322	1.234 0.086	4.277	0.698	1.491	0.000	0.000	0.000
101	SXF		4	62.804	12.836	-1.821	1.502 4.898 0.322	1.256 0.086	3.951	0.612	1.501	0.000	0.000	0.000
102	S2H		8	63.056	13.302	-0.014	1.505 4.893 0.368	1.255-0.091	3.800	-0.003	1.511	0.000	0.000	0.000
103	QF		15	63.056	13.302	-0.014	1.505 4.893 0.368	1.255-0.091	3.800	-0.003	1.511	0.000	0.000	0.000
END	HCDF		4	63.056	13.302	-0.014	1.505 4.893 0.368	1.255-0.091	3.800	-0.003	1.511	0.000	0.000	0.000
	BEGIN	HCFDL	2	63.056	13.302	-0.014	1.505 4.893 0.368	1.255-0.091	3.800	-0.003	1.511	0.000	0.000	0.000
104	QF		16	63.308	12.849	1.795	1.508 4.715 -1.046	1.218-0.265	3.953	-0.617	1.522	0.000	0.000	0.000
105	S3		12	63.608	11.806	1.697	1.512 4.402 -1.046	1.131-0.265	4.354	-0.722	1.533	0.000	0.000	0.000
106	BEND		12	66.008	5.340	0.976	1.560 2.678 -0.393	1.255-0.091	9.821	-1.556	0.000	0.000	0.000	0.000
107	S5H		11	66.558	4.381	0.776	1.578 2.463 -0.393	0.636-0.103	11.642	-1.758	0.000	0.000	0.000	0.000
108	CT		15	66.658	4.230	0.739	1.582 2.424 -0.393	0.625-0.103	11.996	-1.793	1.602	0.000	0.000	0.000
109	S3H		7	67.009	3.759	0.612	1.596 2.287 -0.393	0.590-0.103	13.289	-1.916	1.607	0.000	0.000	0.000
110	QD		16	67.260	3.606	0.005	1.606 2.229 -0.066	0.575-0.019	13.772	0.016	1.610	0.000	0.000	0.000
END	HCFDL		2	67.260	3.606	0.005	1.607 2.229 -0.066	0.575-0.019	13.772	0.016	1.610	0.000	0.000	0.000
END	BAS		1	67.260	3.606	0.005	1.607 2.229 -0.066	0.575-0.019	13.772	0.016	1.610	0.000	0.000	0.000
END	RING		1	201.780	3.605	0.005	4.821 2.229 -0.066	0.575-0.019	13.776	0.016	4.828	0.000	0.000	0.000
TOTAL LENGTH =				201.78000			QX, QY,	=	4.821236	QV,	=	4.828138		
ALFA	X			0.426119E-01	BETAX(MAX)	=	PY	=	0.187891	QV.	=	-0.380013		
GAMMA(TR)	=			4.844341	DX(MAX)	=		=	13.963957	BETAY(MAX)	=	13.775956		
					XCO(MAX)	=		=	2.920346	DX(MAX)	=	0.000000		
					XCO(R.M.S.)	=		=	11.743923	YCO(MAX)	=	0.000000		
									6.641259	YCO(R.M.S.)	=	0.000000		

... SEARCHING FOR CLOSED ORBIT FOR BEAM LINE "RING"	, DELTA(P)/P =	0.000000	SYMM = F
... ITER.	X	0.000000	ERROR =
... 1	0.003394	0.000000	0.161451E-02
... 2	0.003396	0.000000	0.131262E-04
... 3	0.003396	0.000000	0.317276E-09

TABLE IV

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
SYMM = F
DELTAP/P = 0.0060000

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 PAGE 1

POS. ELEMENT NO.	ELEMENT SEQUENCE	HORIZONTAL			VERTICAL		
		DIST [M]	BETAX [LM]	ALFAX [LM]	PX(CO) [MM]	DX [MM]	DY [MM]
BEGIN RING	1	0.000	3.588	0.003	0.000	3.396	-0.106
BEGIN B4S	1	33.630	3.588	0.003	0.864	3.396	-0.106
BEGIN HCDF	3	33.630	3.588	0.003	0.884	3.396	-0.106
55 QD	9	33.882	3.736	-0.601	0.814	4.431	0.065
56 S2	7	34.182	4.127	-0.710	0.827	3.546	0.388
57 BEND	7	36.582	9.360	-1.457	0.889	5.657	1.376
58 S5H	6	37.132	11.053	-1.640	0.898	6.409	1.376
59 CT	8	37.232	11.382	-1.673	0.899	6.546	1.376
60 SXF	3	37.352	11.717	-1.696	0.900	6.683	1.373
61 S2H	5	37.582	12.580	-1.778	0.904	7.024	1.373
62 QF	9	37.834	13.032	-0.007	0.907	7.242	0.367
END HCDF	3	37.834	13.032	-0.007	0.907	7.242	0.367
BEGIN HCFD	3	37.834	13.032	-0.007	0.907	7.242	0.367
63 QF	10	38.086	12.587	-1.764	0.910	7.207	-0.057
64 S3	8	38.386	11.564	-1.667	0.914	7.012	-0.115
65 BEND	8	40.786	5.234	0.954	0.963	6.599	0.001
66 S5H	7	41.336	4.299	0.755	0.981	6.766	0.043
67 CT	9	41.436	4.153	0.719	0.985	6.797	0.043
68 SXD	3	41.535	4.016	0.660	0.989	6.828	0.325
69 S2H	6	41.786	3.710	0.571	0.999	6.933	0.049
70 QD	10	42.037	3.576	-0.029	1.010	7.116	1.338
END HCFD	3	42.037	3.576	-0.029	1.010	7.116	1.338
BEGIN HCDF0	2	42.037	3.576	-0.029	1.010	7.116	1.338
71 QD	11	42.289	3.740	-0.634	1.021	7.583	2.400
72 S32H	3	45.530	11.747	-1.845	1.022	15.583	2.516
73 CT	10	45.639	12.118	-1.882	1.104	15.574	2.400
74 S3H	4	45.989	13.472	-2.012	1.08	16.409	2.400
75 QF	11	46.241	14.011	-0.114	1.111	16.719	0.064
END HCDF0	2	46.241	14.011	-0.114	1.111	16.719	0.064
BEGIN HCDFD	4	46.241	14.011	-0.114	1.111	16.719	0.064
76 QF	12	46.493	13.584	1.800	1.114	16.441	0.064
77 S3	9	46.793	12.538	1.707	1.117	15.763	-2.274
78 BEND	9	49.193	5.860	1.048	1.162	11.337	-1.421
79 S5H	8	49.743	4.821	0.852	1.178	10.560	-1.421
80 CT	11	49.843	4.655	0.817	1.182	10.419	-1.421
81 SXD	4	49.943	4.500	0.744	1.185	10.400	-1.377
82 S2H	7	50.193	4.152	0.658	1.194	9.938	-1.377
83 QD	12	50.445	3.989	0.001	1.204	9.772	0.046
END HCDFD	4	50.445	3.989	0.001	1.204	9.772	0.046
BEGIN HCDFL	13	50.445	3.989	0.001	1.204	9.772	0.046
84 QD	13	50.697	4.151	-0.655	1.214	9.961	1.472
85 S3	10	50.997	4.572	-0.758	1.225	10.400	1.472
86 BEND	10	53.397	9.871	-1.429	1.282	14.965	2.339
87 S5H	9	53.947	11.526	-1.598	1.291	16.244	2.339
88 CT	12	54.047	11.847	-1.629	1.292	16.476	2.339
89 S3H	5	54.397	13.017	-1.736	1.296	17.290	2.339
90 QF	13	54.649	13.432	0.097	1.299	17.569	-0.119
END HCDFL	1	54.649	13.432	0.097	1.299	17.569	-0.119

TABLE IV {

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
DELTA(P)/P = 0.006000 SYMM = F

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18
PAGE 2

ELEMENT SEQUENCE	POS. ELEMENT OCC. NO.	DIST [M]	BETAX [EM]	ALFAX [E1]	HORI Z COUNT AL MUX [L2PI]	PX(CO) [MM]	DX [EM]	DPX [EM]	I BETAY [EM]	ALFAY [E1]	VERTICAL MUY [2PI]	PY(CO) [MM]	DY [EM]	DY [EM]	
BEGIN HCFDO	2	54.649	13.432	0.097	1.299	17.569	-0.119	2.904-0.017	3.688	-0.020	1.315	0.000	0.000	0.000	
91 QF	14	54.901	12.922	1.917	1.302	17.231	-2.572	2.850-0.423	3.846	-0.621	1.326	0.000	0.000	0.000	
92 S32H	4	58.151	4.313	0.748	1.374	8.921	-2.572	1.493-0.423	11.622	-1.786	1.406	0.000	0.000	0.000	
93 CT	13	58.251	4.168	0.712	1.377	8.665	-2.572	1.451-0.423	11.981	-1.822	1.407	0.000	0.000	0.000	
94 S3H	6	58.601	3.716	0.587	1.391	7.770	-2.572	1.305-0.423	13.292	-1.947	1.412	0.000	0.000	0.000	
95 QD	14	58.852	3.574	-0.015	1.402	7.264	-1.486	1.223-0.240	13.789	-0.015	1.415	0.000	0.000	0.000	
END HCFDO	2	58.852	3.574	-0.015	1.402	7.264	-1.486	1.223-0.240	13.789	-0.015	1.415	0.000	0.000	0.000	
BEGIN HCDF	4	58.852	3.574	-0.015	1.402	7.264	-1.486	1.223-0.240	13.789	-0.015	1.415	0.000	0.000	0.000	
96 QD	15	59.104	3.731	-0.618	1.413	7.021	-0.454	1.185-0.066	13.307	1.918	1.418	0.000	0.000	0.000	
97 S3	11	59.404	4.133	-0.729	1.425	6.886	-0.454	1.165-0.066	12.194	1.814	1.421	0.000	0.000	0.000	
98 BEND	11	61.804	9.475	-1.484	1.487	6.943	0.502	1.196-0.092	15.573	0.965	1.468	0.000	0.000	0.000	
99 S5H	10	62.354	11.198	-1.669	1.496	7.217	0.502	1.246-0.092	14.621	0.775	1.485	0.000	0.000	0.000	
100 CT	14	62.454	11.533	-1.782	1.497	7.267	0.502	1.255-0.092	14.471	0.741	1.489	0.000	0.000	0.000	
101 SXF	4	62.554	11.874	-1.724	1.499	7.317	0.498	1.264-0.091	14.327	0.702	1.492	0.000	0.000	0.000	
102 S2H	8	62.804	12.751	-1.807	1.502	7.402	0.498	1.286-0.091	14.000	0.690	1.502	0.000	0.000	0.000	
103 QF	15	63.056	13.212	-0.012	1.505	7.434	-0.551	1.286-0.091	13.848	-0.004	1.512	0.000	0.000	0.000	
END HCDF	4	63.056	13.212	-0.012	1.505	7.434	-0.551	1.286-0.091	13.848	-0.004	1.512	0.000	0.000	0.000	
BEGIN HCFDL	2	63.056	13.212	-0.012	1.505	7.434	-0.551	1.286-0.091	13.848	-0.004	1.512	0.000	0.000	0.000	
104 QF	16	63.308	12.763	1.785	1.508	7.166	-1.580	1.241-0.269	4.0003	-0.625	1.522	0.000	0.000	0.000	
105 S3	12	63.608	11.728	1.687	1.512	6.695	-1.580	1.162-0.269	6.616	1.534	0.000	0.000	0.000	0.000	
106 BEND	12	66.008	5.307	0.567	1.560	4.000	-0.603	0.714-0.107	9.891	-1.570	1.592	0.000	0.000	0.000	
107 S5H	11	66.558	4.355	0.771	1.579	3.754	-0.603	0.655-0.107	11.713	-1.762	1.601	0.000	0.000	0.000	
108 CT	15	66.658	4.205	0.734	1.582	3.694	-0.603	0.645-0.107	12.066	-1.797	1.602	0.000	0.000	0.000	
109 S3H	7	67.008	3.738	0.607	1.596	3.484	-0.603	0.607-0.107	13.359	-1.919	1.606	0.000	0.000	0.000	
110 QD	16	67.260	3.587	0.003	1.607	3.396	-0.106	0.592-0.021	13.840	0.023	1.609	0.000	0.000	0.000	
END HCFDL	2	67.260	3.587	0.003	1.607	3.396	-0.106	0.592-0.021	13.840	0.023	1.609	0.000	0.000	0.000	
END B4S	1	67.260	3.587	0.003	1.607	3.396	-0.106	0.592-0.021	13.840	0.023	1.609	0.000	0.000	0.000	
END RING	1	201.780	3.585	0.003	4.823	3.396	-0.106	0.592-0.021	13.850	0.023	4.826	0.000	0.000	0.000	
TOTAL LENGTH =		201.780000			QX, QY,	=		4.822774	QY,	=	4.825811				
ALFA	=	0.429182E-01			BETAX(MAX)	=		0.276111		=	-0.570392				
GAMMA(TR)	=	4.827019			DX(MAX)	=		14.013023	BETAY(MAX)	=	13.849585				
					XCO(MAX)	=		2.904409	DY(MAX)	=	0.000000				
					XCO(R.M.S.)	=		17.568722	YC0(MAX)	=	0.000000				
								9.949599	VCO(R.M.S.)	=	0.000000				

... SEARCHING FOR CLOSED ORBIT FOR BEAM LINE "RING"	"	DELTA(P)/P = 0.008000, SYMM = F
... ITER:	X	ERROR
... 1	0.004595	0.000000
... 2	0.004596	0.000000
... 3	0.004596	0.000000

Page 4

TABLE IV

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING
DELTA(P)/P = 0.008000 SYMM = F

POS. ELEMENT NO.	ELEMENT OCC. NAME NO.	ELEMENT SEQUENCE			HORIZONTAL			VERTICAL			ALPHA		
		DIST [M]	BETAX [LM]	ALFAX [LM]	MUX [L2P1]	PX(CO) [MM]	DX [M]	DY [MM]	MUY [L2P1]	PY(CO) [MM]	DPY [M1]	DPY [M1]	
BEGIN RING		0.0000	3.570	0.0001	0.0000	4.596	-0.149	0.608-0.023	13.901	0.030	0.000	0.000	
BEGIN BAS	1	33.630	3.569	0.0001	0.804	4.596	-0.149	0.608-0.023	13.906	0.030	0.000	0.000	
BEGIN HCDF	3	33.630	3.569	0.0001	0.804	4.596	-0.149	0.608-0.023	13.906	0.030	0.000	0.000	
55 QD	9	33.882	3.717	-0.601	0.815	4.642	0.666	0.614	0.066	1.398	1.977	0.000	
56 S3	7	34.107	-0.709	0.827	4.796	0.518	0.633	0.666	1.254	1.868	0.811	0.000	
57 BEND	7	36.582	9.329	-1.456	0.889	7.606	1.834	0.982	0.229	5.457	0.457	0.000	
58 S5H	6	37.132	11.017	-1.638	0.898	8.607	1.834	1.106	0.229	4.488	0.876	0.000	
59 CT	8	37.232	11.346	-1.672	0.899	8.789	1.834	1.129	0.229	4.335	0.754	0.000	
60 SXF	3	37.332	11.679	-1.691	0.901	8.901	1.829	1.151	0.228	4.189	0.713	0.000	
61 S2H	5	37.582	12.538	-1.773	0.904	9.424	1.829	1.207	0.228	3.858	0.883	0.000	
62 QF	9	37.834	12.988	-0.008	0.907	9.713	0.480	1.242	0.055	3.699	0.623	0.000	
END HCDF	3	37.834	12.988	-0.008	0.907	9.713	0.480	1.242	0.055	3.699	0.622	0.000	
BEGIN HCFD	3	38.086	12.988	-0.008	0.907	9.713	0.480	1.242	0.055	3.699	0.620	0.000	
63 QF	18	38.386	11.529	1.660	0.914	9.398	-0.886	1.199	0.120	3.837	-0.580	0.000	
64 S3	6	40.786	5.223	0.954	0.963	8.892	0.388	1.192	0.038	4.213	-0.683	0.000	
65 BEND	8	41.336	4.290	0.755	0.982	9.013	0.387	1.122	0.038	9.489	-1.535	0.000	
66 S5H	7	41.336	4.144	0.718	0.986	9.051	0.387	1.126	0.038	11.269	-1.728	0.000	
67 CT	9	41.536	4.000	0.653	0.989	9.091	0.420	1.130	0.046	11.616	-1.763	0.000	
68 SXD	3	41.786	3.706	0.565	1.000	0.420	1.141	0.046	1.146	0.926	0.914	0.000	
69 S2H	6	41.786	3.743	0.640	1.022	0.885	3.181	1.248	0.388	12.829	-1.792	0.000	
70 QD	18	42.037	3.576	-0.035	1.011	9.468	1.769	1.173	0.213	13.264	0.797	0.000	
END HCFD	3	42.037	3.576	-0.035	1.011	9.468	1.769	1.173	0.213	13.264	0.797	0.000	
BEGIN HCDF0	2	42.037	3.576	-0.035	1.011	9.468	1.769	1.173	0.213	13.264	0.797	0.000	
71 QD	11	42.289	4.539	1.886	1.022	0.885	3.181	1.248	0.388	12.759	1.924	1.000	
72 S32H	3	45.539	11.786	-1.855	1.022	0.885	3.181	1.249	0.388	14.185	0.736	1.000	
73 CT	18	45.639	12.158	-1.892	1.104	0.657	3.181	2.490	0.388	4.185	0.771	1.000	
74 S3H	4	45.989	13.517	-2.023	1.108	2.657	3.181	2.628	0.388	4.042	0.699	0.000	
75 QF	11	46.241	14.058	-0.118	1.111	2.171	0.084	2.711	0.010	3.460	-0.001	1.110	
END HCDF0	2	46.241	14.058	-0.118	1.111	2.171	0.084	2.711	0.010	3.460	-0.001	1.110	
BEGIN HCFD	4	46.241	14.058	-0.118	1.111	2.171	0.084	2.711	0.010	3.460	-0.001	1.110	
76 QF	12	46.493	13.632	1.803	1.114	2.180	-3.017	2.666	-0.370	3.602	-0.573	1.121	
77 S3H	9	46.793	12.587	1.711	1.117	2.0	9.006	-3.017	2.557	3.975	-0.682	1.099	
78 BEND	8	49.193	5.874	1.060	1.162	1.538	-1.889	1.841	-0.233	9.413	-1.603	1.198	
79 S5H	8	49.743	4.825	0.863	1.178	1.008	-1.889	1.714	-0.233	11.276	-1.810	1.206	
80 CT	11	49.843	4.657	0.827	1.181	1.820	-1.889	1.691	-0.233	11.639	-1.848	1.000	
81 SXD	14	49.943	4.502	0.741	1.185	1.637	-1.889	1.669	-0.214	11.996	-1.752	1.208	
82 S2H	7	50.193	4.155	0.656	1.194	1.187	-1.812	1.617	-0.214	12.885	-1.836	1.212	
83 QD	12	50.445	3.994	-0.001	1.204	1.971	0.078	1.592	0.017	13.341	0.835	1.215	
END HCDF0	4	50.445	3.994	-0.001	1.204	1.971	0.078	1.592	0.017	13.341	0.835	1.215	
BEGIN HCDFL	1	50.445	3.994	-0.001	1.204	1.971	0.078	1.592	0.017	13.341	0.835	1.215	
84 QD	13	50.697	4.156	-0.658	1.214	1.226	1.970	1.626	0.250	12.851	1.902	1.218	
85 S3	10	50.997	4.578	-0.761	1.224	1.813	1.970	1.699	0.250	11.751	1.795	1.222	
86 BEND	10	53.397	9.863	-1.421	1.282	1.897	3.117	2.459	0.389	5.298	0.917	1.271	
87 S5H	9	53.947	11.505	-1.588	1.290	2.159	3.117	2.669	0.389	4.401	0.727	1.289	
88 CT	12	54.047	11.823	-1.619	1.291	2.190	3.117	2.708	0.389	4.261	0.693	1.293	
89 S3H	15	54.397	12.984	-1.725	1.296	2.290	3.117	2.842	0.389	3.821	0.572	1.317	
90 QF	13	54.649	13.394	0.103	1.299	2.290	3.117	2.888	0.015	3.687	-0.026	1.317	
END HCDFL	1	54.649	13.394	0.103	1.299	2.290	3.117	2.888	0.015	3.687	-0.026	1.317	

TABLE IV

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
DELTA(P)/P = 0.008000
SYMM = F

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18

PAGE 2

		V E R T I C A L										
POS.	ELEMENT OCC. NAME NO.	DIST [M]	BETAX [1]	ALFAX [1]	MUX [2P11]	X(CO) [MM1]	PX(CO) [MM1]	DX [M]	DPX [1]	BETAV [1]	ALFA Y [1]	
BEGIN	HCFDO	2	54.649	13.394	0.103	1.299	23.361	-0.151	2.888-0.015	3.687	-0.826	1.317
91	QF	14	54.901	12.883	1.917	1.302	22.915	-3.413	2.834-0.418	3.848	-0.628	1.328
92	S22H	4	58.151	4.293	0.747	1.373	11.910	-3.413	1.496-0.418	11.668	-1.797	1.408
93	CT	13	58.251	4.148	0.711	1.377	11.571	-3.413	1.455-0.418	12.028	-1.833	1.409
94	S3H	6	58.601	3.698	0.585	1.391	10.386	-3.413	1.311-0.418	13.345	-1.959	1.413
95	QD	14	58.852	3.557	-0.014	1.402	9.717	-1.961	1.230-0.235	13.845	-0.820	1.416
END	HCFDO	2	58.852	3.557	-0.014	1.402	9.717	-1.961	1.230-0.235	13.845	-0.820	1.416
BEGIN	HCDF	4	58.852	3.557	-0.014	1.402	9.717	-1.961	1.230-0.235	13.845	-0.820	1.416
96	QD	15	59.104	3.712	-0.615	1.413	9.400	-0.580	1.194-0.060	13.364	1.419	0.000
97	S3	11	59.404	4.111	-0.725	1.425	9.228	-0.580	1.177-0.060	12.251	1.818	1.423
98	BEND	11	61.804	9.417	-1.475	1.487	9.360	0.691	1.221-0.097	5.627	0.968	1.469
99	S5H	10	62.354	11.127	-1.659	1.496	9.737	0.691	1.274-0.097	4.673	0.780	1.486
100	CT	14	62.454	11.460	-1.693	1.497	9.805	0.691	1.284-0.097	4.521	0.746	1.489
101	SXF	4	62.554	11.797	-1.710	1.498	9.873	0.684	1.293-0.096	4.377	0.706	1.493
102	S2H	8	62.804	12.666	-1.793	1.502	10.043	0.684	1.317-0.096	4.052	0.652	1.502
103	QF	15	63.056	13.122	-0.010	1.505	10.037	0.732	1.317-0.096	3.896	-0.621	1.512
END	HCDF	4	63.056	13.122	-0.010	1.505	10.037	0.732	1.317-0.096	3.896	-0.621	1.512
BEGIN	HCFDL	2	63.056	13.122	-0.010	1.505	10.037	0.732	1.317-0.096	3.896	-0.621	1.512
104	QF	16	63.308	12.676	1.774	1.508	9.680	-2.122	1.192-0.273	4.054	-0.632	1.523
105	S3	12	63.608	11.649	1.677	1.512	9.048	-2.122	1.192-0.273	4.460	-0.735	1.534
106	BEND	12	66.008	5.273	0.966	1.561	5.532	-0.822	0.735-0.112	9.961	-1.575	1.592
107	S5H	11	66.558	4.328	0.766	1.579	5.083	-0.822	0.675-0.112	11.785	-1.766	1.600
108	CT	15	66.658	4.179	0.730	1.583	5.002	-0.822	0.664-0.112	12.139	-1.801	1.601
109	S3H	7	67.008	3.717	0.602	1.597	4.717	-0.822	0.625-0.112	13.431	-1.923	1.606
110	QD	16	67.260	3.568	0.001	1.608	4.596	-0.149	0.608-0.023	13.910	0.030	1.608
END	HCFDL	2	67.260	3.568	0.001	1.608	4.596	-0.149	0.608-0.023	13.910	0.030	1.608
END	B4S	1	67.260	3.568	0.001	1.608	4.596	-0.149	0.608-0.023	13.910	0.030	1.608
END	RING	1	201.780	3.565	0.001	4.825	4.596	-0.149	0.608-0.023	13.928	0.030	4.823
TOTAL LENGTH =			201.780000			QX			4.824923	QY		4.822551
ALFA	=		0.432149E-01		BETAX(MAX)	=			0.360883	QY,		-0.761640
GAMMA(TR)	=		4.810421	PX	DX(MAX)	=			14.062001	BETAY(MAX)	=	13.92848
					XCO(MAX)	=			2.888203	DY(MAX)	=	0.000000
					XCO(R.M.S.)	=			23.361379	YCO(MAX)	=	0.000000
									13.249608	YCO(R.M.S.)	=	0.000000

Page 43

TABLE IV

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18

ZOHREH PARSA /

PAGE 1

AGS BOOSTER LATTICE FOR SURVEY
 LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
 $\Delta(P)/P = 0.010000$ SYMM = F

POS.- ELEMENT OCC. NO.	ELEMENT NAME	ELEMENT SEQUENCE			HORIZONTAL			VERTICAL		
		DIST [M]	BETAX [M]	ALFAX [L]	MUX [CO]	PX(CO) [MM]	DX [M]	DY [MM]	BETAY [L]	ALFAY [M]
BEGIN RING	1	0.000	0.000	5.551	-0.001	5.829	-0.197	0.625-0.025	13.969	0.036
BEGIN B4S	1	33.630	0.001	3.550	-0.001	5.829	-0.197	0.625-0.025	13.976	0.036
BEGIN HCDF	3	33.630	0.001	3.550	-0.001	5.829	-0.197	0.625-0.025	13.976	0.036
55 QD	9	33.882	0.000	3.698	-0.000	5.815	-0.000	0.630-0.066	13.464	1.993
56 S3	7	34.182	0.007	4.087	-0.709	0.827	0.000	0.650	12.313	1.884
57 BEND	7	35.582	0.000	9.298	-1.767	0.890	0.586	0.650	0.000	0.000
58 S5H	6	37.132	10.981	-1.637	0.898	10.834	2.292	1.121-0.229	4.498	0.875
59 CT	8	37.232	11.309	-1.670	0.900	11.060	2.292	1.143-0.229	4.344	0.761
60 SXF	3	37.332	11.641	-1.686	0.901	11.287	2.283	1.165-0.227	4.198	0.882
61 S2H	5	37.582	12.496	-1.767	0.904	11.852	2.283	1.221-0.227	3.864	0.629
62 QE	9	37.834	12.944	-0.009	0.907	12.211	0.587	1.256-0.052	0.857	0.000
END HCDF	3	37.834	12.944	-0.009	0.907	12.211	0.587	1.256-0.052	0.825	0.000
BEGIN HCFD	3	38.086	12.505	1.750	0.911	12.143	-1.130	1.247-0.124	3.703	0.025
63 QF	10	38.386	11.494	1.654	0.914	11.807	-1.130	1.210-0.124	4.198	0.902
64 S3	8	40.786	5.212	0.954	0.964	11.805	0.458	1.102-0.124	4.211	0.000
65 BEND	8	41.336	4.281	0.755	0.982	11.254	0.458	1.119-0.033	9.458	0.982
66 S5H	7	41.436	4.136	0.718	0.986	11.300	0.458	1.123-0.033	11.220	0.000
67 CT	9	41.536	4.001	0.645	0.990	11.348	0.510	1.126-0.043	11.565	0.000
68 SXD	3	41.786	3.703	0.558	1.000	1.147	0.510	1.137-0.043	11.906	0.000
69 S2H	6	42.037	3.576	-0.041	1.011	1.809	2.192	1.168-0.210	1.759	0.925
70 QE	10	42.037	3.576	-0.041	1.011	1.809	2.192	1.168-0.210	0.986	0.000
END HCFD	3	42.037	3.576	-0.041	1.011	1.809	2.192	1.168-0.210	0.986	0.000
BEGIN HCDF0	2	42.037	3.576	-0.041	1.011	1.809	2.192	1.168-0.210	0.996	0.000
71 QD	11	42.289	3.745	-0.647	1.022	1.573	3.954	1.241-0.384	12.671	0.998
72 S32H	13	45.539	1.825	-1.864	1.102	2.594	3.954	2.463-0.384	1.759	0.000
73 CT	10	45.639	12.198	-1.902	1.104	2.685	3.954	2.500-0.384	1.763	0.000
74 S3H	4	45.989	13.562	-2.033	1.108	2.055	3.954	2.632-0.384	1.884	0.000
75 QF	11	46.241	14.105	-0.122	1.111	2.562	0.103	2.680-0.009	3.401	-0.001
END HCDF0	2	46.241	14.105	-0.122	1.111	2.562	0.103	2.680-0.009	3.401	-0.001
BEGIN HCDF	4	46.241	14.105	-0.122	1.111	2.562	0.103	2.680-0.009	3.401	-0.001
76 QE	12	46.493	13.680	1.806	1.739	1.062	2.106	-3.636-0.366	0.565	1.110
77 S3	19	46.793	12.635	1.714	1.117	2.592	-3.752	2.529-0.366	3.949	-0.676
78 BEND	9	49.193	5.888	1.072	1.161	18.699	-2.353	1.821-0.231	9.347	-1.615
79 S5H	8	49.443	4.829	0.873	1.178	17.418	-2.353	1.696-0.231	11.220	-1.825
80 CT	11	49.843	4.659	0.837	1.181	17.418	-2.353	1.673-0.231	11.585	-1.863
81 SXD	4	49.943	4.503	0.739	1.184	16.958	-2.353	1.652-0.208	1.941	-1.212
82 S2H	7	50.193	4.159	0.654	1.194	16.405	-2.235	1.601-0.208	1.821	-1.315
83 QD	12	50.445	3.998	-0.003	1.203	1.612	1.578	0.021	1.270	0.943
END HCDF0	4	50.445	3.998	-0.003	1.203	1.612	1.578	0.021	1.270	0.943
BEGIN HCDFL	1	50.445	3.998	-0.003	1.203	1.612	1.578	0.021	1.270	0.943
84 QD	13	50.697	4.162	-0.661	1.213	1.643	2.472	1.611-0.252	1.780	0.000
85 S3	10	50.997	4.585	-0.763	1.224	17.197	2.472	1.685-0.252	11.684	1.224
86 BEND	10	53.397	9.854	-1.413	1.281	24.801	3.895	2.444-0.389	5.276	0.907
87 S5H	9	53.947	11.483	-1.578	1.289	26.921	3.895	2.654-0.389	0.719	1.217
88 CT	12	54.047	11.798	-1.608	1.291	27.307	3.895	2.692-0.389	4.252	0.294
89 S3H	5	54.397	12.950	-1.714	1.295	28.657	3.895	2.825-0.389	3.819	0.308
90 QF	13	54.649	13.354	0.109	1.298	29.121	-0.179	2.872-0.013	3.688	-0.033
END HCDFL	1	54.649	13.354	0.109	1.298	29.121	-0.179	2.872-0.013	1.319	0.000

AGS BOOSTER LATTICE FOR SURVEY
LINEAR LATTICE PARAMETERS FOR BEAM LINE: "RING"
DELTA(P)/P = $\frac{0.010000}{F}$

TABLE IV A

"MAD" VERSION: 6.01/03 RUN: 19-NOV-8 08:07:18

PAGE 2

POS. ELEMENT OCC. NO.	ELEMENT SEQUENCE NAME	H O R I Z O N T A L			V E R T I C A L		
		DIST [M]	BETAX [L]	ALFAX [L]	PX(CO) [MM]	DX [M]	DY [MM]
BEGIN HCFDO	2	54.649	13.354	0.109	1.298	29.121	-0.179
91 QF	14	54.901	12.843	1.917	1.301	28.568	-4.246
92 S32H	4	58.151	4.273	0.746	1.373	14.906	-4.246
93 CT	13	58.251	4.129	0.710	1.376	14.486	-4.246
94 S3H	6	58.601	3.680	0.584	1.390	13.015	-4.246
95 QD	14	58.852	3.539	-0.013	1.402	12.185	-2.425
END HCFDO	2	58.852	3.539	-0.013	1.402	12.185	-2.425
BEGIN HCDF	4	58.852	3.539	-0.013	1.402	12.185	-2.425
96 QD	15	59.104	3.693	-0.611	1.413	11.798	-0.693
97 S3	11	59.404	4.069	-0.721	1.425	11.592	-0.693
98 BEND	11	61.804	9.358	-1.467	1.487	11.828	0.893
99 S5H	10	62.354	11.055	-1.650	1.496	12.313	0.891
100 CT	14	62.454	11.385	-1.683	1.497	12.401	0.891
101 SXF	4	62.554	11.719	-1.697	1.498	12.489	0.880
102 S2H	8	62.804	12.580	-1.779	1.502	12.706	0.880
103 QF	15	63.056	13.030	-0.008	1.505	12.702	-0.911
END HCDF	4	63.056	13.030	-0.008	1.505	12.702	-0.911
BEGIN HCFDL	2	63.056	13.030	-0.008	1.505	12.702	-0.911
104 QF	16	63.308	12.588	1.763	1.508	12.254	-2.671
105 S3	12	63.608	11.569	1.666	1.512	1.461	-2.671
106 BEND	12	66.008	5.237	0.961	1.561	7.024	-1.050
107 S5H	11	66.558	4.300	0.761	1.579	6.452	-1.050
108 CT	15	66.658	4.153	0.724	1.583	6.348	-1.050
109 S3H	7	67.008	3.695	0.597	1.597	5.984	-1.050
110 QD	16	67.260	3.548	-0.001	1.608	5.829	-0.197
END HCFDL	2	67.260	3.548	-0.001	1.608	5.829	-0.197
END B4S	1	67.260	3.548	-0.001	1.608	5.829	-0.197
END RING	1	201.780	3.543	-0.001	4.828	5.829	-0.197
TOTAL LENGTH =		201.780000	QX =	4.827681	QY =	=	4.818355
ALFA (TR) =		0.435019E-01	BETAX(MAX) =	0.442220	BETAY(MAX) =	=	-0.953803
GAMMA(TR) =		4.794526	DX(MAX) =	14.110854	DY(MAX) =	=	14.011904
XCO(MAX) =			XCO(R.M.S.) =	2.871719	YCO(MAX) =	=	0.000000
XCO(R.M.S.) =			XCO(R.M.S.) =	29.121348	YCO(R.M.S.) =	=	0.000000
				16.541174			

ZOHREH PARSA / 19-NOV-8 08:07:13

page 45