# The QTUNE Program--The AGS Extracted Beam Transport Program 

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# The "QTUNE" Program--The AGS Extracted Beam Transport Program 

J.F. Ryan

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## Introduction

The purpose of this Technical Note is to document the extracted beam transport program called "QTUNE". This program can be used to calculate beam sizes in the four SEB lines and the FEB line from the ring to the primary targets using the known power supply and magnet characteristics. Typical TTY and Versatec outputs for the "U" line and "C" line are shown in Figures 1 and 2. The program is run with the R-R QTUNE command when in the operations area.

## Discussion

The primary purpose of this program is to calculate the horizontal and vertical beam sizes in the various beam lines using the present settings of the power supplies and the best known values of beam emittance. Beam splitting is not considered. All beam is assumed going down each line when calculating beam sizes. The magnetic data is calculated from the calculated magnet current using a 4th order power series. Power supply and magnet current limitations for the beam lines are included. Various groups of quadrupoles in the beam lines can be tuned to vary waist locations and sizes.

This program uses 5 by 5 matrices to include momentum dispersion effects. Because this program is similar to a first order "TRANSPORT" run, one output option will write on the "MATRIC-DAT" data file matrices and beam sizes in a similar format to "TRANSPORT". All other output data is written on the "QTUNEDAT" data file which should be printed after exiting from the program.

## Program Options

The various program options are shown on the HELP file in Figure 3.
The "A" command will print on the "MATRIC-DAT" file the transport matrices and emittances using the beam line chosen with the constant BFILE and the power supply data chosen with constraints IAGSFG and IENUT. Figures $4 \mathrm{~A}-\mathrm{B}$ show a part of this file.

The "B command prints the calculated currents and fields in the magnets. The power supply values are chosen with the constants BFILE, IAGSFG and IENUT. Figures $5 A-B$ show this file for the " $C$ " line.

The "H", "D", "E", "K" and "L" command descriptions are shown on Figure 3.
The "C" command is used to change one or more constants shown in Figure 6 using the NAMELIST feature. These constants only have numerical values. Those that effect the graphics output are XYRANG, ZRANGE, LFRAME, AND TEKVER. The input beam at H13 (FEB) or F13 (SEB) is described with PBEAM, ABEF13, ABEH13, DPP and H13MOM (FEB only). The beam line is chosen with BFILE, and IAGSFG selects if the power supply command or readback is used to calculate the magnet current. An off-line program, "ENUTQ", can be chosen to supply the power supply values and is selected using constant IENUT. This program, similar to "AGAST", rather than the TTY option, should be used for off-line communication since these values can be easily transferred to and from the on-line program "AGAST". The constant TEGFG is used to change to a different "ENUTQ" file.

The "G" command is used to plot beam sizes as on Figures 1, 2 or 7. An "E" will exit from this option. During FEB or SEB operation the constants are initialized so that a "G" command will plot the "U" line or "C" line beam sizes. The values of certain parameters are printed on the graph, "QTUNE-DAT", and sent to "AGAST" or "ENUTQ". These are shown in Figure 8 and defined in Figure 9.

The " $P$ " and " $M$ " commands will print on "QTUNE-DAT" the constants of the beam line and magnets as shown in Figures 10 and 11.

The "T" command, shown in Figure 12, is used to tune various groups of quads to meet desired values of waist parameters described in Figure 9. The beam sizes at the targets cannot be used to tune the quads before the targets, but can be varied by changing the waist locations and sizes. If tuning is mathematically successful and the program is on-line, the quad power supplies will be changed.

The "W" command calculates the values of the FEB or SEB parameters without plotting the graph.

## Theory and Units

The beam is considered a collection of particles traveling down a beam line with the magnetic elements described with a matrix $R_{i}$.


Or
$\rightarrow$ BEAM DIRECTION $\rightarrow$


The characteristics of the beam particles at the output can be determined from the following matrix equation:

$$
\begin{equation*}
\left[\mathrm{x}_{1}\right]=[\mathrm{R}] \times\left[\mathrm{X}_{\mathrm{o}}\right] \tag{2}
\end{equation*}
$$

"QTUNE" uses a $5 \times 5$ order matrix for the magnetic elements, [R]. Equation 2 can be expanded to:

$$
\left[\begin{array}{l}
\mathrm{x}_{1}  \tag{3}\\
\theta_{1} \\
\mathrm{Y}_{1} \\
\phi_{1} \\
\delta_{1}
\end{array}\right]=\left[\begin{array}{lllll}
\mathrm{R}_{11} & \mathrm{R}_{12} & \mathrm{R}_{13} & \mathrm{R}_{14} & \mathrm{R}_{15} \\
\mathrm{R}_{21} & \mathrm{R}_{22} & \mathrm{R}_{23} & \mathrm{R}_{24} & \mathrm{R}_{25} \\
\mathrm{R}_{31} & \mathrm{R}_{32} & \mathrm{R}_{33} & \mathrm{R}_{34} & \mathrm{R}_{35} \\
\mathrm{R}_{41} & \mathrm{R}_{42} & \mathrm{R}_{43} & \mathrm{R}_{44} & \mathrm{R}_{45} \\
\mathrm{R}_{51} & \mathrm{R}_{52} & \mathrm{R}_{53} & \mathrm{R}_{54} & \mathrm{R}_{55}
\end{array}\right] \times\left[\begin{array}{l}
\mathrm{x}_{0} \\
\theta_{0} \\
\mathrm{x}_{0} \\
\phi_{0} \\
\delta_{0}
\end{array}\right]
$$

where standard TRANSPORT definitions apply to the particle characteristics:
$X_{o}--$ horizontal displacement of input ray, in inches, with respect to assumed central trajectory.
$\theta_{0}-\infty$ the angle (mr) that this input ray makes in horizontal plane with respect to central trajectory.
$Y_{0}--$ vertical displacement of input ray (inches) with respect to central trajectory.
$\phi_{0}--$ the angle (mr) that this input ray makes in vertical plane with respect to central trajectory.
$\delta_{0}--\Delta \mathrm{P} / \mathrm{P}=$ fractional momentum deviation (\%) of this input ray and the assumed central trajectory.

The units for the $[R]$ matrix are:

$$
\begin{aligned}
& R_{11}\left(\frac{\operatorname{In} X}{\operatorname{In} X}\right) \quad R_{12}\left(\frac{\operatorname{In} X}{\operatorname{mr} X}\right) \quad R_{13}\left(\frac{\operatorname{In} X}{\operatorname{In} Y}\right) \quad R_{14}\left(\frac{\operatorname{In} X}{\operatorname{mr} Y}\right) \quad R_{15}\left(\frac{\operatorname{In} X}{\%}\right) \\
& R_{21}\left(\frac{m r X}{\operatorname{In} X}\right) \quad R_{22}\left(\frac{m r X}{\operatorname{mr~X}}\right) \quad R_{23}\left(\frac{m r X}{\operatorname{In} Y}\right) \quad R_{24}\left(\frac{m r X}{m r X}\right) \quad R_{25}\left(\frac{m r X}{\%}\right) \\
& R_{31}\left(\frac{\operatorname{In} \mathrm{Y}}{\operatorname{In} \mathrm{X}}\right) \quad \mathrm{R}_{32}\left(\frac{\operatorname{In} \mathrm{Y}}{\operatorname{mr} \mathrm{X}}\right) \quad \mathrm{R}_{33}\left(\frac{\operatorname{In} \mathrm{Y}}{\operatorname{In} \mathrm{Y}}\right) \quad \mathrm{R}_{34}\left(\frac{\operatorname{In} \mathrm{Y}}{\operatorname{mr} \mathrm{Y}}\right) \quad \mathrm{R}_{35}\left(\frac{\operatorname{In} \mathrm{Y}}{\%}\right) \\
& R_{41}\left(\frac{\operatorname{mr} Y}{\operatorname{In} X}\right) \quad R_{42}\left(\frac{\operatorname{mr} Y}{m r X}\right) \quad R_{43}\left(\frac{m r Y}{\operatorname{In} Y}\right) \quad R_{44}\left(\frac{m r Y}{m r Y}\right) \quad R_{45}\left(\frac{\mathrm{mr} Y}{\%}\right) \\
& \mathrm{R}_{51}\left(\frac{\%}{\operatorname{In} \mathrm{X}}\right) \quad \mathrm{R}_{52}\left(\frac{\%}{\operatorname{mr} X}\right) \quad \mathrm{R}_{53}\left(\frac{\%}{\operatorname{In} \mathrm{Y}}\right) \quad \mathrm{R}_{54}\left(\frac{\%}{\operatorname{mr} Y}\right) \quad \mathrm{R}_{55}\left(\frac{\%}{\%}\right)
\end{aligned}
$$

Figures 4A-B show the individual element matrix and total [R] matrix at different points in the "C" line. "QTUNE" calculates matrices for drift spaces, horizontal and vertical focussing quadrupoles, wedge dipole and pitching magnets without edge focusing, and rectangular dipole and pitching magnets with edge focussing.

The beam is considered an array of particles that is described with a fth order symmetrical sigma ellipsoid. For historical reasons the program uses a rms beam and then converts this to a $99 \%$ beam. The symmetric SIGMA matrix at at the beam line input is:
$\left[\begin{array}{lllll}\left.\sigma_{0}\right] \\ \sigma_{11} & \sigma_{21} & \sigma_{31} & \sigma_{41} & \sigma_{51} \\ \sigma_{21} & \sigma_{22} & \sigma_{32} & \sigma_{42} & \sigma_{52} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} & \sigma_{43} & \sigma_{53} \\ \sigma_{41} & \sigma_{42} & \sigma_{43} & \sigma_{44} & \sigma_{54} \\ \sigma_{51} & \sigma_{52} & \sigma_{53} & \sigma_{54} & \sigma_{55}\end{array}\right]$

$$
\begin{aligned}
& \sqrt{\sigma_{11}}=X_{\max }=\text { maximum (half) width of the beam envelop in the } X \\
& \text { (bend) plane at the given point (inches). } \\
& \sqrt{\sigma_{22}}=\theta_{\max }=\text { maximum (half) angular divergence of the beam } \\
& \text { envelope in the } \mathrm{X} \text {-bend plane. } \\
& \sqrt{\sigma_{33}}=Y_{\text {max }}=\operatorname{maximum} \text { (half) height of the beam envelope. } \\
& \sqrt{\sigma_{44}}=\phi_{\max }=\text { maximum (half) angular divergence of the beam } \\
& \text { envelope in the } Y \text { (non-bend) plane. } \\
& \sqrt{\sigma_{55}}=\delta_{\text {max }}=\text { half-width }(1 / 2 \Delta \mathrm{P} / \mathrm{P}) \text { of the momentum interval } \\
& \text { being transmitted by the system. }
\end{aligned}
$$

The coupling elements are the $\sigma_{i j}$ elements for $i$ not equal to $j$. "QTUNE" assumes that the input beam for the SEB or FEB lines have no input $X-Y$ coupling or:
\(\left[\begin{array}{lllll}\sigma_{0} <br>

0\end{array}\right]\)| $\sigma_{11}$ | $\sigma_{21}$ | 0 | 0 | 0 |
| :--- | :--- | :--- | :--- | :--- |
| $\sigma_{21}$ | $\sigma_{22}$ | 0 | 0 | 0 |
| 0 | 0 | $\sigma_{33}$ | $\sigma_{43}$ | 0 |
| 0 | 0 | $\sigma_{43}$ | $\sigma_{44}$ | 0 |
| 0 | 0 | 0 | 0 | $\sigma_{55}$ |

The input FEB beam is also assumed to have input momentum dispersion or the $R_{15}$ and $R_{25}$ elements are non-zero at H13.

At any point in the beam line, the SIGMA matrix $\left[\sigma_{1}\right]$ can be found from the input matrix $\left[\sigma_{0}\right]$ and the total $[R]$ matrix to this point:

$$
\begin{equation*}
\left[\sigma_{1}\right]=[R] \times\left[\sigma_{0}\right] \times\left[R^{\mathrm{T}}\right] \tag{6}
\end{equation*}
$$

where $\left[R^{T}\right]$ is the transpose of $[R]$.
The graphs of Figures 1 and 2 are obtained by plotting $\sqrt{\sigma_{11}}$ and $\sqrt{\sigma_{33}}$ along the beam line for a $99 \%$ beam. The program also plots the horizontal momentum dispersion parameters, $R_{15}$ and $R_{25}$, along the beam line.

The input SIGMA matrix, $\left[\sigma_{0}\right]$ is obtained from the constants ABEF13 or ABEHI3 and DPP. For no $X-Y$ coupling, the horizontal part of $\left[\sigma_{0}\right]$ is:

$$
\begin{array}{ll}
{\left[\begin{array}{ll}
\sigma_{11} & \sigma_{21} \\
\sigma_{21} & \sigma_{22}
\end{array}\right]=\varepsilon_{H}\left[\begin{array}{cc}
\beta_{H} & -\alpha_{H} \\
-\alpha_{H} & \partial_{H}
\end{array}\right]} \\
\sigma_{11} & =\varepsilon_{H} \beta_{H} \\
\sigma_{21} & =-\varepsilon_{H} \alpha_{H} \\
\sigma_{22} & =\varepsilon_{H} \gamma_{H}=\varepsilon_{H}\left(\frac{1+\alpha_{H}^{2}}{\beta_{H}}\right)
\end{array}
$$

where $\alpha, \beta$, and $\varepsilon$ are the rms beam Twiss parameters as specified in ABEF13 or ABEH13. These are initialized to the best know values of the emittance at F13 (from H. Weisberg) or H13 (W. Weng).
$\alpha$ - dimensionless
B - kiloinch
$\varepsilon-$ epislon $=$ rms emittance (inch-mrad)
The $99 \%$ beam emittance $=9.2103 \varepsilon_{\text {rms }}$
The $99 \%$ beam width plotted $=3.0348$ (beam width for rms beam)
The vertical $\left[\sigma_{0}\right]$ elements, $\sigma_{33}, \sigma_{43}$, and $\sigma_{44}$ are obtained in a similar way.

If $X-Y$ coupling occurs downstream, the beam ellipsoid is assumed to have the same 5th order volume or no losses are assumed. THe horizontal and vertical emittances may change. To determine the location of a waist, the emittance in that plane is needed at the entrance to the drift space. The emittance is the projection of the ellipsoid on that plane or

$$
\varepsilon_{H}=\operatorname{DET}\left(\begin{array}{ll}
\sigma_{11} & \sigma_{21}  \tag{8}\\
\sigma_{21} & \sigma_{22}
\end{array}\right) \text { or } \varepsilon_{V}=\operatorname{DET}\left(\begin{array}{ll}
\sigma_{33} & \sigma_{43} \\
\sigma_{43} & \sigma_{44}
\end{array}\right)
$$

where DET is the determinant.

Equation (6) can be expanded and simplified for an input beam with no $X-Y$ coupling (Equation (5)).

$$
\begin{equation*}
[\sigma]_{1}=[\mathrm{R}] \times[\sigma]_{0} \times\left[R^{T}\right] \tag{6}
\end{equation*}
$$

At Point 1

$$
\begin{align*}
\left(\sigma_{11}\right)_{1}=\left(X_{\text {max }}\right)^{2} & =\left(\sigma_{11}\right)_{\circ} R_{11}^{2}+2\left(\sigma_{21}\right) R_{11} R_{12}+\left(\sigma_{22}\right)_{\circ} R_{12}^{2}  \tag{7}\\
& +\left(\sigma_{33}\right)_{\circ} R_{13}^{2}+2\left(\sigma_{43}\right)_{\circ} R_{13} R_{14}+\left(\sigma_{44}\right)_{\circ} R_{14}^{2} \\
& +\left(\sigma_{66}\right)_{\circ} R_{16}^{2} \\
\left(\sigma_{33}\right)_{1}=\left(Y_{\text {max }}\right)^{2} & =\left(\sigma_{11}\right)_{\circ} R_{31}^{2}+2\left(\sigma_{21}\right)_{\circ} R_{32} R_{31}+\left(\sigma_{22}\right)_{\circ} R_{32}^{2}  \tag{8}\\
& +\left(\sigma_{33}\right)_{\circ} R_{33}^{2}+2\left(\sigma_{43}\right)_{\circ} R_{34} R_{33}+\left(\sigma_{44}\right)_{\circ} R_{34}^{2} \\
& +\left(\sigma_{66}\right)_{\circ} R_{36}^{2}
\end{align*}
$$

$$
+\left(\sigma_{22}\right)_{o} R_{12} R_{32}+\left(\sigma_{33}\right)_{o} R_{13} R_{33}+\left(\sigma_{43}\right)_{o} \cdot x
$$

$$
\left(\mathrm{R}_{14} \mathrm{R}_{33}+\mathrm{R}_{13} \mathrm{R}_{34}\right)
$$

$$
+\left(\sigma_{44}\right)_{\circ} R_{14} R_{34}+\left(\sigma_{66}\right)_{o} R_{16} R_{36}
$$

Where the $\left(\sigma_{i j}\right)_{o}$ are the input beam components and the $R_{i j}$ are the total matrix elements from the input to the Point 1 in the beam line. The input beam Twiss parameters ( $\alpha, \beta, \varepsilon$ ) can be found experimentally by fitting several beam width measurements to Equation (6) or (7) knowing the elements of the [R] matrix at the measurement point.
mn.
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A.D. Physicists

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Figure 1





```
& <CR - - PRIMT ON "DTUNE.DAT" BEAN LINE DATA UTHH FIELOS & CURRENTSIN
    MATFETS
& <BN- - HADNE THE OONGTANTS
O<R - DELETE STHRT DUER\ ON THE "QTUNE.DAT" FLLE.
E<CR> - EXIT
G <RE - FLOT GEQ PROFILES & GET WALST PARAMETERS FROM PRESENT
MAGNET SETTIMGS
K GCQ>-- TYPE DUT COHSIATS AND THEIF DEFINLTIOHS
L<C* -- LIST &PRIHT) DN "GTMNE DAT" COHQTANTG & DEFINITIONG
M<CR` - PRIHT OH "QTUME DRT MGGNET LENGTHG & FIELO US CURRENT POLER
    SERIES COEFF. FON BEAT LIHE NHGHETS
P<CRY - PRIHT ON "QTHUE DAT" PONER SUPPLY P&RGMETERS FOR BEGMLLINE
    HmGNETS
T<CR> - TUNE THE DUADS SY UMRYMG THE DUADS OR WALST PARADETERS ON
AGAST AHO PLOT SEAM PROTILES.
N SCP - - CALCULATES HATST PHRMDETERG FROM AGAST COMNANDS % SEND WAIST
IHFORMATION'TO AGHST FOR MORHING REPORT; HO PLOTS MADE.
```



## GRHS PARTUETERS:

ALPHA, BETA, EPSTLNT (H,V) AT F13: -6.33881 .9952 .01014040 .8708 .90 .127990 .60150



ELEMEMT

## Z (ITCHES)

| START $===$ | 1.00000 |
| :---: | :---: |
|  | 0.00000 |
|  | 0.00000:1 |
|  | 0.00000 .1 |
|  | 0.00000 |
|  | O. 0001 CNCHES |

TOTAL MATRIK'ニ==
0. 0800 INCMES
1.00000
0.00000
0.03000
0.00000
0.00000
1.43 .025 IMCHPS

TOTAL. MATRIX $===$


TOTAL MATRTK $===$
188.1\%5. IMCHES

| $=$ = | 1.00000 |
| :---: | :---: |
|  | 0.00009 |
|  | 0.00008 |
|  | 0.00000 |
|  | 0.00000 |
|  | 186.250 IMCMES |

TOTAL MATRIX $===$

ELEMENT OR TOTAL MATRTX TROM: START
0.00003
1.00009
.00300
0.00303
0.00000
0.00000
0.00030
1.03000
0.03030
0.00003

| 0.00000 | 0.00000 |
| :--- | :--- |
| 0.00090 | 0.00000 |
| 0.00000 | 0.00000 |
| 1.00000 | 0.00000 |


| 1.00030.i |  | 0:00003 | 0.00000 |
| :---: | :---: | :---: | :---: |


| 6. $00300{ }^{1}$ | 1.00000 | 0 - 00000 |  |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| 9.00000m | 0.00030 | : 1.0000 | 0.00000 |
| 0.00000. | 0.00000 | 10.00000 | 1.00000 |
| 0.00000 | 0.00003 | 0.00000 | 0.00000 |


| 0.00090 | 0.00000 |
| :--- | :--- |
| 0.00000 | 0.00000 |
| 0.12393 | 0.00000 |
| 1.00000 | 0.00000 |
| 0.00003 | $: 1.00000$ |

0.00000
0.00000
0.00000
$1: 000000$


TRANSPORT BLEAM MATRIX


| $1.00000: 1$ | 0.14383 | - 10.100000 | 0.00000 |
| :---: | :---: | :---: | :---: |
| 0.000004 | 1.00000 | 0: 01300 | 0.03030 |
| - 00000 | 0.00000 | 1.00009 | 0.14883 |
| 0.0000 | 0.00000 | 19:00030 | 1:00000 |
| 0.00030 | 0.00000 | 2:00000 | 0.00000 |


$-0.02801:$
-7.11699
$0.00090:$
0.02000
1.02030



185.8 EO . I ROHES

"C" LINE HAGNETS FROM F13 TO C CTARGET

| --mLIEHENT--MAGNET |  |  |  | --POWER SUPPLY DATA--- |  |  | - MAGNET DATA FOR 296000 GEVZC-- |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | Varie. | LABEL: | EITD | DDF 1 | CHD/RDBE: DDF2E | CED/RDEK |  |  |  |
| 1 |  |  | DRITT |  |  |  |  |  | 0.0 |
| 2 | CDI | CD1 | RDPOL | CD1 | -2243 | 0 | 1.40188.5: | -445: 524. | -0.67027 |
| 3 |  |  | DRIPT |  |  |  |  | -6.5502 | $-6.55019$ |
| 4 | Col | CQ1 | QUAIP | CQ1 | -1898 | \% | 1.42650. | -6.5502 | -0.0. |
| 5 | C02 | C02 | DRIET | C02 | 1073 | 0 | 1.07800m: | 4.9843 | 4.98428 |
| 7 |  |  | DRITT |  |  |  |  |  | -1.39052 |
| 8 | cos | C03 | gUad | Ca3 ${ }^{\text {c }}$ | -303 | 0 | $0.30300 \%$ | -1.3905 | -1.39052 |
| 9 |  |  | DRIPT | CQ4 | $68 \%$ | 0 | $0.51525]$ | 12.3747 | 2.37467 |
| 11 | C84 | Cat | DRIFT | Ged |  |  |  |  | 0.0 |
| 12 |  | AB1 | DRIFT |  |  |  | . |  | 0.0 |
| 13 |  |  | DRIFT |  |  |  | : |  | 0.0 |
| 14 |  | BT3 | DRIMT |  |  |  |  |  | - |
| 15 |  |  | DRITT |  |  |  |  |  | 0.0 |
| 16 |  | AP1 | DRIFT |  |  |  |  |  | 0.0 |
| 17 |  |  | DRITT |  |  |  |  |  | 9.0 |
| 18 |  | CP1 | DRIFT |  |  |  |  |  | 0.0 |
| 19 |  |  | PRIFT |  |  |  | : |  | 0.0 |
| 20 |  | AD2 | DRIFT |  |  |  |  |  | 0.0 |
| 21 |  |  | DRIFT |  |  |  |  |  | 0.0 |
| 22 |  | AD3 | DRIFT |  |  |  | : |  | 0.0 |
| 23 | CD2 ${ }^{\prime}$ | CD2 | RDPOL | CD283 | 3269 : | 0 | 1.225883. | 510.4198 | 10.76775 |
| 25 |  |  | DRIET |  |  |  |  | 510.3109 | - 0.0675 |
| 26 | CD3 | CD3 | RDPOL | CD288 | 3269 " ${ }^{\text {CDST }}$ | 0 | 1.22588: |  | (3.) |
| 27 | C05 | C35 : | DRIFT | C0588 | -1105 .. | 0 | 0.27625 | -4.0898: | -4.038979 |
| 29 |  |  | DRIFT |  |  |  |  |  | 9.0.77303 |
| 30 | cos | cab | CUAD | C@687 | 10000 | 0 | 0.25000 a | 3.7638 | 3.77383 |
| 31 |  |  | DRIET |  | $1000:$ | 0 | $0.250001:$ | 3.7733: | 3.77383 |
| 32 33 | $\mathrm{CO} /$ | CQ\% | RUAD | as6eri | 1000: |  |  |  | 0.0 |
| 33 | C03 | Ces | drilit | C@588 | -1105 | (1) | 0.27625:. | . -4.0893 | -4.08979 |
| 35 |  |  | DRIFT |  |  |  |  |  | 0.0 : |
| 36 |  | CP2 | DRITT |  |  |  |  |  | 0.0) |
| $3 \%$ |  |  | DRIFT |  |  |  |  |  | 0.0 |
| 38 |  | B04 | DRIFT |  |  |  |  |  | 0.0 |
| 39 |  |  | DRIFT | CDA | -2681 | 0 | 1:00537. | -514.3680 | -6.76386 |
| 41 |  |  | DRIFT |  |  |  |  |  | 0.010 |
| 42 | ce9 | Ca9: | $\cdots \mathrm{OLAD}$ | ce9 | 1 | 0 | $0.00006{ }^{\circ}$ | . $\quad 0.0126:$ | 0.01256 |
| 43 |  |  | DRITT |  |  | 0 | 0.09675\% | 1.2642\% | 1.26418 |
| 44 4 | ce10. | C010 | gUAD | Co10 | 2658 : |  | 0.9967 .n |  | $0.0$ |
| 45 | Co11: | Coll 1 : | DRIIFT | C011: | -3502 | 0 | 1.31325. | $-6.0712 \%$ | -6.07116 |
| 46 |  |  | DRIFT |  |  |  |  |  | 0.00308 |
| 48 | co12 | C012 | OUAD | CQ12.. | 2390 | 0 | 1.69250 m | 8.0039 | 0.0 |
| 49 |  |  | PRIPT |  |  |  |  |  | 0.0 |
| W0 |  | CTGT | DRITT |  |  |  |  |  |  |


B) DDF2 (GECONDARY P:S. READBACES) ARW GAS RDBES WITH THE POMADITY OF MORHALL READBACK.



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## 15-Ju1-82: 13:59

```
ALPHA, BETA, ERSILON (H,V) AT F13: -6.3308 1.9952:0.01404 0..8703 0.12799 0.0150
```




| Cn\%\% | CH\%\% | $\mathrm{CH} \% \mathrm{~V}$ Z | CNTVVK | CA\%HI | CA\%IHO | CA\%VI | CA\%VO | CT\%HZ | CT\%HX | CT\%VZ | CT\%VX |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $-199.76$ | 403.93 | 1296.98 | 277.03. | $-1355.70$ | 29\%7.50 | $-1533.36$ | $-162.67$ | -33.40 | 62.45 | $-56.59$ | 95435 |
| BT\%HE | BT\%HX | BT\%VZ | BT\%VY | AT\% ${ }^{\text {diz }}$ | AT\%HE | AT\%VZ | AT\%VX | Bindiv | TG\%GH | TG\%GV |  |
| -1.00 | 62:00 | 3.08 | 32.00 | 854.00 | 224.00 | -1592.00 | 127.00 | 86.52 | 93.04 | 125.76 |  |

## 15-5u1-82 14:03)

## ORTS PARAMETERS:

ALPHA, BETA, EPSILOT (H,V) AT F13: - 0.3388 1.9952 0.019040.8708:0.127930.01.50


 -199 an 103.09
-199.76 403.98 1296.99

2"자.03-1858.79: $2977.59-1533.36 \cdot-162.67$
2.6.03-180®.69: $2967.50-1533.36 \cdot-162.67$-33.40. 62.45

AT\%HZ AT\%HK AT\%VZ AT\%VK: BHDIV: TG\%GE: TG\%GV
CT\%VZ . CT\%VX
$-20.59 \% \quad 95.35$


DEFINITMON
HHLL WIDTH MLLS): OF HORLZ. BEAM AT NAIST NEAR'A TGTA (QTUNEPGM.)
 (HALF WIDTH (MILS) OF" VERT, BEAM AT WAIST NEAR'A: TGT. W(QTUNE: PGM:):
 (HALF WIDTH (HILS) GF: HORIZ. BEAM AT WAIST NPAR 'B' TGT, (OTUNE PGM.) (Z POS. OF; 'B' TGT HORZ:WAIST,INCH'; $0=$ 'B' TGT; $-50=50$ IN. UPSTM 'B') (HALF WIDTH(MILS) OF VERT. BRAM AT WAIST NEAR 'B'ITGT: (QTUNE PGM.) (Z POS. OF.'B' TGT VERT. WAIST, INCH; O= 'B' TGT; $-50=50 ;$ IN. UPSTRM 'B'T) (1000 TIMES BEAM HORIZ. EMITTANCE: ALPHATAT CQ5 DPSTREAM (Q TUNE USES)! ( 1000 TIMES BEAM HORIZ. EMITTANCE IALPHA AT CQ8 DONNSTREAM (Q TUNE USE) (1000 TIMES BEAM VERTICAL EMITTANCE ALPHA AT CQS UPSTREAM (Q TUNE USE) (1000 TIMES BEAM VERTICAL EMITTANCE ALPHA AT CQS UPSTREAM (Q TUNE USE
(1000 TTMES BEAM VERTICAL EMITTANCE ALPHA AT CQ8 DNSTREAM (Q TUNE USE)
 (Z POS. MIDDLE C LINE (IMCH FROM F13)OF FORZ. WAIGT (Q TUNE PGM USES) (HALM-FDTH (MILS) OF VERT. BEAM AT WAIST MID C LINE (O TUNEIPGML)

(HALF WIDTH(MILS) OF HOPIZ. BEAT 'AT WAIGT NEAR , C' TGT. (OTUNE PGM USES)
 (HALF WIDTH (IMLS) OF VERT. BEAM AT: WAIST NEAR 'G; TGT: (QTUNE PGF USES)
 (CALCULATED HORIZONTAL HALF WIDTH BEAM SIZE IN MILS AT "A" TARGET)
CALCULATED VERTICAL HALF WIDTH BEAM SIZE IN MILS*AT "A" TARGET) (CALCULATED HORIZONTAL HALF WIDTH BEAM SIZE IN MILS AT "B" TARGET)
(CALCULATED VERTICAE HALF WIDTH BEAM SIZE IH MILS AT "B" TARGET):
(CALCULATED HORIEONTAL HALF WIDTH BEAM SIZE IN MILG AT "G" TARGDT) (CALCULATED VERTICAL HALW WIDTH BEAM SIZE IN NTLS;AT "G" TARGET) (CALCULATED. HORZ, HALF. WIDTH BEAM SIZE IM MILS AT: T TGT. - QTUTM PGM) (CALCULATRD. VERT. HALF WIDTH BEAKISILE IN ILILS AT TU TGT. - CTUNE PGM): (1000 K GALQ. MOMENTUM DLSPRRSION(INGH/RATIO) AT EMD DF 8 DEG. MAGNET) (1000 X GALC. MOMENTUM DISPERSION•PRIME(MR/RATIO) AT END OF B DRG. MA) (HALT WIDTH(MILS) OF HORZ. BEAM AT WAIGT NEAR TGT: - GTUNE PGM. USES) ( $Z$ POS. QR: U TGT. HORZ. WAIST, INCH; $0=0$ TGT, ; $-50=50 \because I N$ UPSTRM U TG) (HALP WIDTR (MILS) OH VERT. BEAM AT. WAIST NEAR TGT! - QTUNE PGM, USES) ( $2 \mathrm{POS} . \mathrm{ON} \mathrm{U}$ TGT. VERT. WAIST, INCH; $0=0$ TGT.; $-50=50: I N$. UPSTRM U TG)
" Q " LINE MAGNETS FROM F13 TO CITARGET

"C" LINE MAGNETS FROM T13 TO G TARGET

| -- EIEMENT-- |  |  | MIAGNET- |  |  | EFT.LEN |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | TAmE | LABELE | KIND | croder | * | INGES |
| 1 |  |  | $\operatorname{TRIPT}$ |  | 20 | 143.825 |
| 2 | GD1 | CDI | RDPOL | 15 CO 0 | -7 | 34.350 |
| 3 |  |  | DRIET |  | 0 | 8.085 |
| 4 | CO1 | CQ1 | mual | N3@36 | 1 | 37.509 |
| 5 |  |  | TRTMT |  | 6) | 46.500 |
| 6 | C02 | C02 | guad | N3@48 | 2 | 49.50 |
| 7 |  |  | DRIFT |  | 0 | 20.500 |
| 8 | C03 | C03 | MUAD | N3043 | 2 | 49.600 |
| 9 |  |  | DRIFT |  | 0 | 26.500 |
| 10 | CQ 4 | cos | @UAD | 173036 | 1 |  |
| 11 |  |  | DRITT |  | 0 | 33.125 |
| 12 |  | AB1 | DRIFT |  | 0 | 106.250 |
| 13 |  |  | DRIFT |  | 0 | 163.750 |
| 14 |  | BE3 | DRIMT |  | 0 | 106.250 |
| 15 |  |  | DRIFT |  | 0 | 68.750 |
| 16 |  | AP1 | DRITI |  | 0 | 122. ${ }^{\text {en }}$ |
| 17 |  |  | WRITT |  | 0 | 15.500 |
| 18 |  | CP1 | $\mathbb{D R I F T}$ |  | 0 | 122.500 |
| 19 |  |  | PRTMT |  | 0 | 70.024 |
| 20 |  | AD2 | DRIFT |  | 0 | 96.000 |
| 21 |  |  | DRIET |  | 9 | 22.191 |
| 22 |  | A1D3 | DRIET |  | 0 | 96.000 |
| 23 |  |  | DRIFT |  | (1) | 434.033 |
| 24 | CD2 | CDs | RIPPOL | 5C90T | 8 | 91.500 |
| 25 |  |  | DRIFT |  | 0 | 84.501 |
| 26 | CD3 | CD3 | RDPPOL | 5C90T | 8 | 91.500 |
| 29 |  |  | DRETPT |  | ${ }^{6}$ | 24.650 |
| 28 | CQ5 | C05 | QUAD | - 4016 | 3 | 17.200 |
| 29 |  |  | DREIT |  | (9) | 184.800 |
| 50 | C06 | G96 ${ }^{\text {a }}$ | mud | 4016 | 2 | 1 C .200 |
| 31 |  |  | $\mathbb{T R I P T}$ |  | (3) | 6.800 |
| 32 | cas | Cor. ${ }^{\text {c }}$ | $\because$ QUAD | 4016 | 3 | 18.200 |
| 33 |  |  | DRIPT |  | 0 | 124.809 |
| 34 | Ces | C08.: | ; OUAD | 4016 | 3 | 17.200 |
| 35 |  |  | MRIPT |  | 0 | 229.150 |
| 36 |  | CP2 | DRIPT |  | 0 | 122.503 |
| 37 |  |  | DRIPT |  | 0 | 248.897 |
| 38 |  | RDA | DRIPT |  | 0 | 92.509 |
| 39 |  |  | DRIPT |  | 0 | 256.120 |
| 40 | CD4 | CDIA | RDPPOL | D121 | 9 | 123.500 |
| 41 |  |  | DRIFT |  | 0 | 461.013 |
| 42 | CQ9 | CQ9 | QUAD | 4916 | 3 | 17.200 |
| 43 |  |  | DREFT |  | 0 | 601,900 |
| dis | C010 | 10 | Quab |  | 4 | 36.0070 |
| 45 |  |  | Mrint |  | (3) | 813.570 |
| 46 | cel 1 | CQ1 1 | $\therefore$ QUAD | N3036 | 1 | 37.590 |
| 47 |  |  | DRIFT |  | 0 | 84.542 |
| 48 | CQ12 | CO12 | QUAD | N3Q36 | 1 | 37.500 |
| 49 |  |  | DRIFT |  | 0 | 240.155 |
| 50 |  | CTGT | DRIFT |  | 0 | 0.000 |




```
WHEN REOUSTED GTUE G. }2,3.45,6, INE ;PLOT HADE IF TUNTMG OKYALL
    DEUICES AQSUNEO COHBIAHT EVEPT THE NUADS
```



```
    GFTER REDOING MLL DEULCES.
E--.-TPE E TO LEME THNLUQ RODE
```




```
3-FGN REHDS HLL BCTY%' ADO TUNES CRO-12.
4 - PGM READS ALL "BT&%" MHL TUNES g09-13.
5 --FGM READS "ATYR" ANO TUNES ARTXS AND AQS.
6 --PGM READS "UTR??" GND TUNES UQ1 I-4.4.
*wNOTE: IF TBALMG OK BUT POU. SUPPLY GATURATED, PLOT MADE BUTUALUES THED \& NOT SENT TO AGAET: \(12551=\) SATUR. TO TUNE MAKE SMAL CHANGES CLES THAN 269.
TYPE ERR TO CONTINUE
```


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