

BNL-104604-2014-TECH

AGS/AD/Tech Note No. 176;BNL-104604-2014-IR

The U Line--1981

J. Ryan

November 1981

Collider Accelerator Department Brookhaven National Laboratory

# **U.S. Department of Energy**

USDOE Office of Science (SC)

Notice: This technical note has been authored by employees of Brookhaven Science Associates, LLC under Contract No.DE-AC02-76CH00016 with the U.S. Department of Energy. The publisher by accepting the technical note for publication acknowledges that the United States Government retains a non-exclusive, paid-up, irrevocable, world-wide license to publish or reproduce the published form of this technical note, or allow others to do so, for United States Government purposes.

# DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or any third party's use or the results of such use of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof or its contractors or subcontractors. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

Accelerator Department BROOKHAVEN NATIONAL LABORATORY Associated Universities, Inc. Upton, New York 11973

AGS Division Technical Note No. 176

The "U" Line--1981

J. Ryan

November 5, 1981

#### Introduction

This technical note is an attempt to redocument the FEB transport line as beam sizes observed on "U" line flags do not compare well with the calculated beam sizes. Magnet locations were checked and compared with the locations in the FEB manual. Flags were removed and measured. In most cases new flags were reinstalled. Power supply and magnet information was obtained from the EAG magnetics section and compared with observed magnetic information. The beam pipe size was measured along the U line. The effects of the correction sextupole being at the wrong polarity and UQ8A being run at a very high current were studied.

#### Magnet and Power Supply Data

Figure la - le shows a printed output from the program QTUNE which lists the characteristics of the U line. A drawing of the beam line is shown in Figure 8. The magnet steel lengths were all measured. The effective lengths were obtained from the magnetics group or estimated. The magnet spacings were measured when possible and compared with the FEB manual. The trim magnets and new magnets were located. No major discrepancies were found between the FEB manual and the "U" line. Figure la-b shows the magnet effective lengths, locations, types and apertures. The flag locations are given. The power supply information is shown with the maximum power supply current. Figure lc repeats some information in la - lb and also gives the magnetic field data. This data is expressed as a power series and is valid for all currents from zero to the maximum magnet current listed. The quadrupole gradient data was obtained from excitation curves and the effective length. The dipole KG-IN information was obtained in a similar manner. For example, a quad gradient is:

$$G = A_{\emptyset} + A_{1}I + A_{2}I^{2} + A_{3}I^{3} + A_{4}I^{4} kG/in$$

with the current in kiloamps. The power series represents the data supplied within  $\pm$  0.4% in most cases and  $\pm$  2% in the worst case.

Figure 1d - 1e shows calculated information assuming the power supplies are at a given AGAST setting. The settings listed are also used for the groups of Figures 3 and 6. A negative command or readback corresponds to an AGAST "A" reading--213A is -213. The current and field information is calculated from the constants of Figure 1a - 1c. As the note in Figure 1e explains, the gain of the elements (GEL) is the bend angle of the dipoles or the gradient of the quads with the proper sign for a horizontal or vertical focusing quad. On Figure 1e, certain useful variables available on AGAST and calculated by the QTUNE program are defined. All AGAST names having a "%" character are parameters calculated by the program. Further information can be found on a paper on the "QTUNE" program.

Figure 1f shows the location and power supply information for the "U" line trim magnets. The trim magnet information is not used to calculate beam sizes. All dipole or pitching trim magnets in the "U" line are 6.75D25 magnets. The constants for this magnet are:

 $A_{\not 0} = 0.09519696 \quad \text{Eff. length} = 30.75 \text{ inch}$   $A_{1} = 103.4235 \quad \text{Max. magnet current} = 0.60 \text{ kA}$   $A_{2} = -22.57931$   $A_{3} = 172.3323$   $A_{4} = -220.1772$   $\text{KG-In} = A_{\not 0} + A_{1}I + A_{2}I^{2} + A_{3}I^{3} \text{ for I in kiloamps.}$ 

The power supplies were calibrated in June 1981 by Joe LeLaidier, an EAG technician. The magnetic fields were measured in most magnets later in June, but at a different AGAST setting from Figure 1 with the Bell Gaussmeter. The probe was held next to the pole tips by Ken Reece. Using the AGAST CMD or RDBK that gave the most accurate power supply calibration, the magnetic fields were calculated in the "U" line magnets. The results are shown in Figure 2 using measured pole tip radii. For the sextupole US1A, the gradient dimensions are KG/in<sup>2</sup>. The pole tip fields for UQ12, 13 and 14 were not measured because magnet covers or tight spaces prevented putting the probe in the magnet gap. Figure 2 shows large errors for UQ7, UQ8A and the correction sextupoles US1A and US1B.

- 2 -

Beam sizes in the FEB line can now be measured only from flag measurements. The flags are radelin that are mounted at a 45 degree angle so that a TV monitor may observe the beam striking the flag. Except for U799F all flags are tilted in the vertical plane. Flag U799F is tilted in the horizontal plane. To compensate for the tilt, the graticule spacing in the tilt plan is 1.41 times the effective spacing as observed on the TV monitor. All "U" line flags have been measured and most have been replaced with new flags. One flag was found to be mounted incorrectly in July 1981, so that the long dimension was not in the tilt plane. In most cases, the graticules appear about one inch apart on the TV so that a beam just touching all four marks would be a one inch by one inch beam. Some flags have holes and one flag has a hole and no marks. The following table shows the flags now (October 1981) and as they were in May-June 1981 and perhaps for several years before 1981. The flag 273F is located at 273 feet but is labelled on the flag as 303. It was necessary to use the shorter 303 instrument box in the 273 location when the replacement sextupoles were used near the 8 degree magnets.

- 3 -

#### U15F, U380F

• ; ;



# U618F, U667F, U772F, U799F





Ð



		OLD DIM	ENSIONS	CURRENT DIMENSIONS					
	Actu	<u>1a1</u>	<u> 0n</u>	TV	Actu	1al	<u>On TV</u>		
	a(AH)	<u>b(BH)</u>	a(AH)	<u>b(BH)</u>	a(AH)	<u>b(вн)</u>	a(AH)	<u>b(BH)</u>	
U15F	2.0	1.25	2.0	0.88	2.0	1.25	2.0	0.88	
Hole U15F	1.31	0.63	1.31	0.44	1.31	0.63	1.31	0.44	
U380F	1.0	1.42	1.0	1.0	1.02	1.41	1.02	1.0	
Hole U380F	1.38	0.4	1.38	0.28	1.31	0.37	1.38	0.26	
U165F		NO GRA	TICULES			NO GRAT	TICULES		
Hole U165F	0.75	1.0	0.75	0.70	0.75	1.0	0.75	0.70	
U273(303)	0.78	1.51	0.78	1.07	0.7	1.5	0.7	1.06	
Hole U273(303)	1.69	0.47	1.20	0.44 1.62		0.44	1.15		
		1	_ •		\				

(All Dimensions in Inches)

		OLD DIM	ENSIONS		<u>_</u>	<u>IONS (10</u>	/81)		
	Actu	lal	<u> 0n </u>	<u>rv</u>		Act	ual	On TV	
	<u>a</u>	b	a	b		a	<u>b</u>	a	b
U618F	1.4	1.0	1.4	0.7	1	.0	1.38	1.0	0.98
U667F	1.02	1.35	1.02	0.96	1	0	1.25	1.0	0.88
U772F	1.0	1.38	1.0	0.98	1	0	1.38	1.0	0.98
U799F	1.37	1.0	0.97	1.0	1	.38	1.0	0.98	1.0
U815F	NO GI	RATICULES	5 - 0.6	25 DIA.		NO GR	ATICULES	- 0.625	DIA.

"U" Line Flag Dimensions

The best known input beam is used to calculate the beam widths in the U line. Weng's<sup>1</sup> input emittance for the new H5 extraction system is used with input momentum dispersion and input momentum spread in the horizontal plane. The emittances listed in the FEB manual, used by Weng, and used in the QTUNE program are listed on the next page.

- 4 -

, ţ

### H13 Input FEB Emittance

- 5 -

ţ

		FEB Manual	Weng		QTUNE
α <sub>x</sub>	=	-5.67	-5.67		-5.67
β x	=	5.746 cm/mrad	= 57.46 m/rad	=	2.62 in/mrad
ε x	=	0.12 cm-mrad(0.0472 in	-mrad)		
ε x	==	1.5 x 10	<sup>-6</sup> m-rad(0.5906 in-mrad)	= 0.0064	412 in-mrad rms
∆ P/P	=		± 0.12%	=	± 0.12%
х Р	=		-2.96 m/ratio (-2.96 c	m/%) =	-1.165 in/%
$x_{n}^{1}$	=		-295 mrad/ratio (-2.95	mrad/%)	= -2.95  mrad/%
α	=	0.987	0.987		0.987
β	=	3.7 m/rad =	0.370 cm/mrad	=	0.1457 in/mrad
ε	=	0.186 cm-mrad(0.073	2 in-mrad)		
ε γ	=	1.5 x 10 <sup>-</sup>	<sup>6</sup> m-rad(0.0590 in-mrad)	= 0.0064	412 in-mrad rms

Weng used a slightly different horizontal emittance from the FEB manual since he also included momentum spread and dispersion. Some beam sizes were first calculated using TRANSPORT to check the QTUNE program. The results compare very accurately. The QTUNE program was used to plot graphs since this program takes the information directly from an AGAST display. For historical reasons QTUNE uses the inch system and the rms emittance and plots beam sizes and make calculations for a 99% beam. The program also plots the momentum dispersion parameters along the beam line.

 $\epsilon$  (99% beam) = -2 ln (0.01)  $\epsilon$  = 9.2103  $\epsilon$  rms

beam width (99% beam) = 3.0348 (beam width for rms beam).

AGS Div. Tech. Note No. 176

#### Beam Size Results

The following discussion uses beam half sizes. Using the best known flag sizes, as measured by J.W. Glenn, the observed beam sizes were:

- 6 -

Flag	<u>Horizontal (inch)</u>	<u>Vertical (inch)</u>
U15	0.67	0.28
U165	?	0.70
U273	0.35	0.60
U380	1.0	0.60
U618	0.35	1.37
U667	0.28	1.15
U772	0.87	0.28
U <b>799</b>	0.25	0.60
U815	0.030	0.020

Figure 3a - 3c show the calculated beam sizes in the "U" line using the AGAST settings and field expansions of Figure 1. Printed below the curve on Figure 3a are the AGAST settings and the calculated parameters that are defined on Figure 1e. The observed beam sizes are marked as crosses. Figure 3a also shows the calculated value of the momentum dispersion parameters X and X' p along the beam line. For clarity, these were left off Figures 3b and 3c. All curves are with the same AGAST settings of Figure 1. After the 8 degree magnet, the momentum dispersion parameters are:

 $X_p = 0.339 \text{ in}/\%$   $X'_p = -2.04 \text{ mr}/\%$ 

These parameters are U8%MD and U8%MP. For a dispersionless line after these magnets, these values should both be zero. Weng<sup>1</sup> shows that it is necessary to change the beam line upstream of the 8 degree magnets to achieve this since the "U" line has initial momentum dispersion.

Figure 3 shows a large error between the calculated vertical half size and observed size in most of the beam line. The parameters TG%UH and TG%UV show that the calculated beam half sizes at the target are 0.256 and 0.076 inches which does not agree with the flag sizes. The cause for these errors is not known, but some possible causes were investigated.

Figure 4 and the following table show that small changes in UQ11-UQ14 will make the calculated beam small of the target. The small calculated beam of 52 by 25 mils is greater than the observed 30 by 20 mil beam.

- 7 -

Name	AGAST Start	AGAST Small Beam	Percent Change
UQ11	435B	514B	18.0
UQ12	2916A	2689A	- 7.8
UQ13	2746A	2511A	- 8.6
UQ 14	1894B	1963B	3.6
Horiz. Half Size	0.257 inch	0.053 inch	
Vert. Half Size	0.076	0.025	

#### Sextupole Results

<u>،</u> ۱۰

The effect of the correction sextupoles in the FEB line were investigated to try to explain the flag discrepancies. Second order TRANSPORT was used to determine sextupole effects. A simplification was made, as shown below, to separate the 8 degree dipole into a short dipole followed or preceeded by a short sextupole. Both short magnets had double the actual magnetic field.



Dipole = 68.82688 KG Sextupole = 3.4622 KG Dipole = 68.8268 KG Sextupole = 3.4622 KG

System Used for Transport

The sextupole field in the 8 degree magnet is not well known. The following table gives the fields in that magnet and the external shimmed sextupole US1A.

8 -

8 Degree Correction Coil	External Shimmed Sextupole
$A_{0} = 0.00194$	0.13574
$A_1 = 2.317825$	1.3395
$A_2 = -0.040949$	0.66138
$A_3 = -0.35138$	- 0.89414
$A_4 = \emptyset$	- 0.243625
Effective Length = 75 inch	26.06 inch
Pole Tip Radius = 2.0 inch	2.063 inch
Sextupole Gradient	Sx Table

The gradient can be found from:

 $S_x = A_0 + A_1I + A_2I^2 + A_3I^3 + A_4I^4 KG/in^2$  for I in kiloamps.

The 8 degree dipoles produce a sextupole error field that adds to the dipole field on the horizontal midplane. Since the dipoles have a field that is up to bend protons to the east, the equivalent sextupole is as shown



TRANSPORT considers this sextupole a negative sextupole. The external and internal correction sextupoles must have the opposite polarity.

- 9 -

Figures 5a - 5b give the TRANSPORT data file for the external sextupoles at the correct polarity to cancel the dipole error field. The results of several computer runs are shown in Figure 6 for the beam line starting at the first correction sextupole upstream of the 8 degree magnets. The power supplies are set at the same value as in Figure 2. Curve 1 is a first order calculation or a second order calculation, with no sextupoles which also is the same as Figures 3a - c. Curve 2 shows the effect of shorter dipoles at twice the field and no sextupoles. Curve 3 assumes that the correction sextupoles are off but the dipole error sextupoles are on. Curves 4 and 5 show the correction sextupoles on at the correct and wrong polarities. It should be noted that curves 3-5 are valid for either polarity of the dipole error field. Curve 4 shows that the correction sextupoles do cancel the effect of the error field. The only difference occurs down near Ql1 in the horizontal plan and this difference is less than 0.030 inches. These correction sextupoles are also at a field 12 percent too strong to cancel the dipole error as shown below:

 $S_x \propto \frac{\text{field}}{(\text{radius})^2} \times \text{length}$   $S_x = 32.46 \text{ KG/in for 8° error}$  $S_x = 36.34 \text{ KG/in for US1A}$ 

The crosses show the measured beam sizes. It can be seen that if the correction sextupoles were at the wrong polarity, some vertical errors could be explained. However, the curves show that the horizontal beam would also blow up and this was not observed. One can conclude that the sextupoles were operating at the correct polarity.

#### Varying UQ8A

The quadrupole UQ8A is a vertical focusing quad that had a large error between calculated and measured gradients as shown in Figure 2. Figure 7 shows the effect of increasing the current in that magnet. For a current of 0.70 KA, the vertical beam fits inside the beam pipe and approaches the observed beam at 618F and 667F. This current, however, is 46 times the assumed current and - 10 - AGS Div. Tech. Note No. 176

larger than the maximum current from AGAST for 4000 counts (0.25 KA). This current is, however, less an the magnet rating of 1.2 kA. This effect is not understood, but another possible cause could be the excitation of spare magnets existing in the U line. For example, UQ8B is 28.8 feet downstream of UQ8A and cables are connected to the coils of this magnet.

# Conclusions

The errors or discrepancies of Figure 3 have not been satisfactorily explained. Magnetic field measurements should be repeated. The unused magnets should be checked to confirm that they are not energized. If the beam line information can be verified, a new H13 emittance may be needed to produce a calculated beam similar to the observed beam.

#### References

- W.T. Weng, Momentum Dispersion of AGS Fast Extracted Beam, BNL 24658, April 1978.
- 2. W.T. Weng, The New AGS Fast Extraction System, BNL 51310, September 1980.

mn

# 21-0CT-81 16:36

BFILE	(BEAM FILE NUMBER: 1=A,2=B,3=C,4=D,5=U)	44. 44. 44.
r demn Abef13	(ALPHA, BETA (KILOINCH), EPSILON (INCH-MRAD, RMS) AT F1	29.40 R
	HORIZONTAL: -6.6358 2.2660 VERTICAL: 0.8708 0.1279	Ö.0078 Ö.0075
ABEH13	(ALPHA, BETA (KILOINCH), EPSILON (INCH-MRAD, RMS) AT H1 HORIZONTAL: -5.6700 2.2620	3.0044
DPP	(DELTA P/P) OR MONEN, FRACT, IN Z FOR 992(11 LN) REAM)	0.1200
Highom	(INPUT HORZ, MOMEN, DISPERSION AT HIS; INCH/Z, MR/Z)	~ ~
TERVER	(=1 FOR TEKTRÖNİX PLOTS,=2(MODEL 1200) OR -2(MODEL 1100) VERSATEK'& NO TÜNING)	<b>4</b>
LFRAME	(=0 OR NEG. TO SUPPRESS FRAMES & LABELS ON GRAPHS; -1.0 OR 1 FOR ALL CRAPHS; -2 OF 2 FOR NO SOMEN.	*5
	DISPERSION PLOTE)	2
IAGSFG	(AGS_FLAG;=1 FOR_MAGNET_VALUES_FROM_TTY;=2 FOR	
DOTTNO	AGASI KUBK5,=3 FUN AGASI CUMMAND5) /Doudd cuddiy dran fime in me affed fan	44.44
7RANCE	(PLOTTING RANCE IN REAR IINE FET (NIMAYN N	1100
	0,000 (STARTING POINT OR 0 FEET FROM F13)	
	10000.000 (END POINT OR END OF BEAM LINE)	
LENUT (	O="AGAST" OR TTY <sub>3</sub> -1 = OFFLINE "ENUTO") A-UST CHEORDER (STUDIE)	- 1
Latrix (	V-UGE CURRENT EMUTE RIUWASTEG" FILES-1 TU CHANCE FILE NAMEY	ň
XYRANG	(MAX, BEAM HALF SIZE FOR PLOTTING, INCH)	1.0000

21-OCT-81 16:37

RMS PARAMETERS: ALPHA, BETA, EPSILDM (H,V) AT H13: -5.6700 2.2620 0.0064 0.9870 0.1457 0.0064

UQ1 (-2727) UQ2 ( 3235) UD1-3( 2998) UD1-3( 2998) UD1-3( 2998) UQ3-6(-2845) UQ3-6(-2845) UQ3-6(-2845) UQ3-6(-2845) UQ7 ( 1727) 5-6( 3847) UD5-6( 3847) UQ8-9(-3534) UQ84 ( 240) UQ8-9(-3534) UQ10 ( 1345) UQ11 ( 435) UQ12 (-2916) UQ13 (-2746) UQ14 ( 1894) U82MD U82MP UT2HZ UT2HX UT2VZ UT2VX TGZUH TGZUV 339.76 -2040.37 -133.88 31.04 30.02 24.62 256.90 76.09

- 11

Div.

Tech.

Note

No.

176

#### 21-0CT-81 14:37

"U" LINE MAGNETS FROM HIS TO U TARGET

еге * NAME	MENT Label	MAGNET XIND GROUP		Z(U/S) INCH	lencth Inch	XAPER Inch	YAPER INCH	PON F DDF	JER SUPPLY RIMARY AMPS/DCN	INFORM MAX- KAMPS	ATION -SEC DDF	ONDARY- AMPS/DCN	
12 34 5 UO1 6 7 UQ2	15F UQ1 UQ2	DRIFT DRIFT DRIFT QUAD N3Q3A DRIFT QUAD N3Q3A DRIFT	00000-0-0	0.000 120.000 192.320 192.321 211.570 249.070 268.570 306.070	120.000 72.320 0.001 19.249 37.500 19.500 37.500 18.800	1.440 1.440 1.440 1.440 1.440 1.440 1.440 1.440	1.800 1.440 1.440 1.440 1.440 1.440 1.440	UQ1 UQ2	0.7500 0.6250	2,400 2,300			Figure 1 a

9	UD1	UDi	RDPOL	4D78	11	324.870	81.900	1.940	1.44()	UD1-3	1.0000	3,300	
10 11	UD2	UD2	RDPOL	4D78	0 11	404.770 424.848	18.098 81.900	$1.940 \\ 1.940 \\ 1.940 $	1,440 1,440	UD1-3	1.0000	3,300	
1914	UD3	UD3	DRIFT RDPÖL DRIFT	4078	0 11 0	524,866 524,866 606,766	18.098 81.900 548.000	1,940 1,940 2,690	1.440 1.940 2.690	UD1-3	1,0000	3.300	
15 15 17	UQ3	UQ3	DRIFT QUAD DRIFT	4026	0 16 0	1154.766 1230.646 1259.244	75,880 28,598 40,000	1.690	1.690	UQ3-6	0.0750	0,400	
16 19 20	UQ4	UQ4	DEIFT QUAD DEIFT	4026	ð 16 0	1299.244 1532.204 1540.802	232.960 28.598 200.000	2.490 1.690 2.490	2.490 1.690 2.490	UQ3-6	-0,0750	0.400	
21 22 23	1105	UQS	DRIFT QUAD DETFT	4026	Ö 16 6	1740,802 1833,762 1842,340	72.960	1.490 1.690	1,690 1,690	UQ3-6	-0.0750	0.400	
24 25		165F	DRIFT		Õ	1973.860		Õ, ÕÕÕ	0.000 2.000				
26	UQ6	UQ6	QUAD DRIFT	4026	1Å 0	2135,319 2143,917	28.598 272.940	1.690	1.690	UQ3-6	0.0750	0.400	
28 29	UQ7	UQ7	QUAD DEIFT	4026	1Å 0	2436.877 2465.475	28,598	1.690 1.790	1.690	UQ7	-0. <del>0750</del> -0.100	0,300	
$\frac{30}{31}$		2737	DRIFT DRIFT		Ô	3274,560 3274,561	0.001 95.499	0.000 1.790	0,000 1,790				
92 92	UDS	UD5	RDPOL DRIFT	36072	19 0	3370.060 3445.060	75.000 42.010	1.940	1,940	UD5-6	0.2500	1.000	
34 35	UD6	UD4	RDPOL DRIFT	38072	19 0	3487.070 3562.070	75,000 115,430	1,940	1.940	UD5-6	0,2500	1,000	
997 197	UQB	UQB	QUAD DRIFT	4026	1.Š 0	3677.700 3706.298	28.598 88.000	1.690 1.940	1.490 1.940	008-9	-0,0625	0.250	
38 39 40	UQ8A	UQ8A	DRIFT QUAD DRIFT	8016P	0 17 0	3774,298 3896,248 3916,248	121,950 20,000 457,362	3.690 3.690 3.490	3.690 3.690 3.690	UQBA	0.0625	0.250	
41 42		380F	DRIFT DRIFT		Ö Ö	4573,610 4573,611		0.000 3.690	0.000 3.490				
43 44	UQ9	UQŸ	QUAD DRIFT	4026	1Å 0	4669,060	28,598 1081,260	1.890	1.690	008-9	0.0625	ó.250	
45 46	UQ10	UQ10	QUAD DRIFT	4926	1Å 0	5778.918 5807.514	28.598 1408.484	1,290	1.690 1.490	UQ10	0.1000	0.388	
47 48 49		618F 4477	DRIFT DRIFT NETET		ŏ	7416.000	0,001 591,139	0.000 1.670	0.000				
50	UQ11	UQ11	DRIFT QUAD	4026	ŏ 1¢	8007.171 8091.371	84.200 	1.490	1,490	UQ11	0.1000	0.115	
ala lat. Ta lat.		772F	DRIFT DRIFT		ŏ	9275,297 9275,271 9275,272	1155.302 0.001 16.Z30	0.000 1.670	1,000 1,000				
	UQ12	UQ12	RUAD	8Q32P	0 1.8	9292.002 2302.771	15./69 34.000	2°140 2°240	2 ° 2 40 2 ° 2 40	UQ12	0.3750	1.200	
2-00- 	UQ13	UQ13	QUAD	8032P	18	7343.771 9350.511	36.000	2+740 2+740	2.740	UQ13	0.3750	1.200	
57 57	UQ14	UG14	UKIFI QUAD Noter	N3036	U 1	7300.011 9492.021	102,510 37,500	2*/40 1*440	z:/40 1:440	UQ14	0.7500	2.400	
62		815F	DRIFT		ŏ	7.527.521 .9771.671	292,130 0,001	1.444V 0.000	1.440 0.000				
00 64		UTGT	DRIFT		0 0	7771+072 9782.672	11,000	1,440 0,000	1,440 0,000				

21-0CT-81 16:38

<u>Figure 1 b</u>

I 12 I

"U" LINE MAGNETS FROM H13 TO U TARGET

99	ELEM Name	TENT LABEL	MA KIND	GNET	***	EFF.LEN INCH	A0	KG/I	N OR KG-IN POW	JER SERIES COEFF A2	ICIENTS FOR I 1 AS	N KILOAMPS	MAX.MAGNE KAMPS	:2
4		157	DRIFT DRIFT DRIFT	2 9 2	0000	$\begin{array}{c} 120.000\\ 72.320\\ 0.001\end{array}$	k 1							
2 2	UQ1	001	QUAD	N3036	0 1 2	37.500	1.520163	0E-02	4.4772430E+0C	1.9792940E-01	4.7379500E-02	-9.1596540E-02	2:600	
Ž	ugz	UQ2	QUAD	N3036	ľ A	37.500	1,520163	0E-02	4 <i>.4</i> 772430E+00	1.9792940E-01	4.7379500E-02	-9,15965408-02	2.600	
ğ 10	UD1	UD1	RDPOL	4D78	1ľ		2,606888	0E-01	3.2376880E+02	9.2981530E-01	-3,0072690E-01	0.0000000E+00	3.400	
11	UD2	UD2	ŘDPOL	4D78	1Ž		2.606888	0E-01	3.2376880E+02	9.2981530E-01	-3.0072490E-01	0.0000000E+00	3,400	
473245	003	UD3 <sup>°</sup>	RDPOL DEIFT	4D78	11 0	81.900 548.000	2.606888	0E-01	3+2376880E+02	9,2981530E-01	-3.0072690E-01	0.000000E+00	3.400	
16 17 18	003	003	QUÃD DRIFT DRIFT	4026	16 0	28.598	7.387751	0E-03	9.2529370E+00	2.4783180E+00	-8.1294770E400	-6.7577510E+00	0.550	
19 20 21	UQ4	004	QUAD DRIFT DRIFT	4926	1Š 0	28,598 200,000 79,940	7.887751	02-03	9,2529370E+00	2.4783180E+00	-8.1294770E+00	-6.7577510E+00	0.550	
234	UQS	UQ5 145F	QUAD DRIFT NETET	4026	16 0	28.598 111.500	7.887751	0E-03	9.2529370E+00	2.4783180E+00	-8.1294770E+00	-6.7577510E÷00	0,550	I
25	069	UQA	DRIFT QUAD DRIFT	4026	ŏ 16	161,458 28,598 272,960	7.887751	0E-03	9.2529370E+00	2,4783180E+00	-8.1294770E+00	-6.75775102+00	0.550	13 -
28 29 30	UQ7	UQ7 273F	QUAD DRIFT DRIFT	4026	1Å 0 0	28.598 809.085 0.001	7.887751	0E-03	9.2529370E+00	2.4783180E+C0	-8.1294770E+00	-6.7577510E+00	0.530	
992 1992	U05	UD5	DRIFT RDPOL	39072	0 19	95,499 75,000	-9,134979	0E+00	3,2169220E+03	-3,5253800E+01	-5.2960020E+02	0.000000E+00	1.100	A
00 34 94	UDA	UD6	ROPOL	38072	19 19	42.010 75.000	-9,134979	05+00	3.2169220E+03	-3.5253600E+01	-5.2960020E+02	0.0000000E+00	1,100	ទី
3637	008	108		4026	0 16 0		7.887751	)E-03	9.25293702+00	2.4783180E+00	-8.1294770E+00	-6.7577510E+00	0,550	Div.
39 40 41	UQBA	UQSA BAOF	QUAD DRIFT	8016P	17 0	20,000	-1,234660(	)E-03	2,5374830E+00	-1.5826770E-01	1.01573208-01	0.000000E+00	1.200	Tech.
42 43	UQ9	UQ9	DRIFT QUAD	4026	0 16	95,449 28,598	7.8877510	)E-03	9₊2529370E+00	2.47831806+00	-8.1294770E±00	-4.75775108200	0. EEA	Not
44	UQIO	UQ10	DRIFT QUAD	4026	0 16	1081.260 28.598	7.887751(	)E-03	9.25293708+00	2.4783180E+00	-A.1294770E+00	-4.7577510FL00	0.550 A.556	e I
46 47		618F	DRIFT DRIFT		Ô	$1608.484 \\ 0.001$						ha the suit of selection of the formation	~~~~~~	No.
48 49		667F	DRIFT DRIFT		0 0	591.169 0.001								176
01522 51522	UQ11	UQ11 7778	DRIFT QUAD DRIFT NETET	4026	0 16 0	84.200 28.598 1155.302	7.687751(	)E-03	9.2529370E+00	2.4783180E+00	-8.1294779E+00	-6.7577510E+00	0,550	5
54		8 6 <u>6</u> 44	ÖRÍFÍ		ŏ	16.730						Figure 1	e	

55		DEIFT		0	15.769						
<u>54 UQ12</u>	0615	QUAD	8032P	18	36,000	-1.2346600E-03	2.5374830E+00	-1.5824770E-01	1.01573208-01	0.000000E+00	1,200
<u> </u>	0013	QUAD	8032P	18		-1,2346600E-03	2.5374830E+00	-1.58267702-01	1.0157320E-01	0.0000000E+00	1.200
šý UQ14	UQ14	QUAD	N3036	ľ	37,500	1.5201630E-02	4.4772430E+00	1.97929408-01	4.73795006-02	-9.1596540E-02	2.600
82 43	815F	DRIFT		Õ							
ĂĂ	HTGT	ĎŔŤŔŤ		ŏ	11.000						

21-0CT-81 16:38

"U" LINE MAGNETS FROM H13 TO U TARGET

₩	ELEI NAME	MENT LABEL	MAGNET KIND	DDF1	OWER SUPPL CHD/RDBK	Y DATA DDF2	CMD/RDBK	MAGNET DATA CURRENT(KA)	FOR 29,400 GEV/C KG-IN OR KG/IN	GAIN(GEL)
20		157	DRIFT DRIFT DRIFT							0.0 0.0
ren z	901	UQ1	QUAD Notet	UQ1	-2727		0	2.04525	-8.8028	-8.80283
Ž	UG2	U02	QUAD	UQ2	3235		0	2.02187	8.7376	v.v §.73765
9 1 A	UD1	UDi	ŘĎĚÔĹ	UD1-3	2998		i,	2.99800	971.1733	1,44121
	UD2	UD2	RDPOL NETET	001-3	2998		0	2.99800	971.1733	V.V 1.44121
	UD3	ШЭЗ	ŘĎPÔĽ DRIFT	UD1 - 3	2998		0	2.99800	971,1733	0.0 1.44121 2.0
16 17 17	UQ3		QUAD DRIFT	N03-9	-2845		0	0.21338	-2.0021	-2.00208
19 20	UQ4	UQ4	QUAD DEIFT ASTET	7-88N	-2045		0	0.21338	2,0021	2.00208 0.0
223	UQ5	UQ5	QUAD DRIFT	` UQЗ-6	-2845		0	0,21338	2.0021	0.0 2.00208 0.0
25	15757	LOOF	DRIFT	110000	114 Hz .c pm		2			0.0
20 27	UWO	090	DRIFT	1113-6	-2845		Ŷ	0,21338	-2.0021	-2.00208
$\frac{28}{29}$	UQ7	UQ7	QUAD DRTFT	UQ7	1727		0	0.12953	-1.2284	-1.22839
30		273F	DRIFT							9.9
	UD5	UD5	RDPOL BATET	UD5-6	3847		Ô	0.96175	2581.0078	0.0 3.83019
34	UD6	UD6	RDPOL NETEP	UD5-6	3047		Ô	0.96175	2581.0078	2.83019
	uca	uqe	õuad DRIFT	UQ8-9	-3534		Ó	0.22088	2.0689	2.06885 0.0
39 39 40	UQBA	UQ8A	DRIFT DUAD DRIFT	UQBA	240		0	0.01500	0.0368	0.0 0.03679 0.0

- AGS Div. Tech. Note No. 176

- 14

---

Figure 1 d

41 19		380F	DRIFT								٥،٥	
43 43	UQŶ	UQ9	QUAD		UQ8-9	-3534		0	0.22088	-2,0489	-2.04885	
45	UQ10	U@10	QUAD		UQ10	1345		0	0.13450	1,2752	0.0 1.27525	
47 47 40		618F	DRIFT								0 • 0 0 • 0	
49 50		667F	DRIFT									
Š.	UQ11	UQ11			UQ11	435		0	0.04350	0.4144	0.0 · 0.41439	
ЌЭ К		772F	ĎŔĺĔĨ								· 0.0	
N. K.	1101 2	1101-5	ĎŘÍPŤ		1104.0			A	a sa sa sa sa sa sa	معدر سعور مسور	<u>````</u>	
57	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	1.4 .5 .5 .2.1 %.1.	DRIFT		UKIZ	-2710		V	1 * 0 4 3 2 0	-20/1/2	-2.71707 0.0	
55 59	OR13	DAT 3	QUAD DRIFT		0013	-2746		¢	1.02975	-2,5548	-2.55482	
60 61	UQ14	UQ14	QUAD DRTFT		UQ14	1894		0	1,42050	6.5374	X- X3737	
62		615F	DRIFT								0.0	
00 64		UTGT	DRIFT DRIFT								0.0 0.0	
NOT#	: ***** CM) DDI KG: CEI	₩ 0/RDBK F2 (SE IN :	REAL CONDARY KG/IN F( O FOR L	)INGS ARE I P.S. READB DR QUADS; KO DRIFT; -KG/1	FROM EMU ACKS) AR S-IN FOR IN FOR H	TQ PGM E NOT DIPOL .F. QU	THE "A" RDBX SA3 RDBKS BUT SS & OMLY APPRO SD & ⊀KG∕IN FOR	IS NE READIN X. FOF V.F. Q	CATIVE IE. CS OF TRIM P. DIPOLES WITH WAD; BEND ANC	2140A = -214( S. TRIM SUPPLIES, LE (DEGREES) FC	). DR DIPOLES (+ = EAST	1 .
									•			
jt li	AME(??:	277)AR	EA(FEB)	COMP()DE	VTP(	) ADDR (	) WHO(W	$\overline{\mathbb{R}}(\overline{\cdot})$	22-6CT-81			·
	i Ii	GZUM F	EB	REFERENCE	) }		(CALCULATED HC	RZ: HA	LE WIDTH BEAM	SIZE IN MILS 6	YT U TGT QTUNE PG	(M)
1	$\frac{2}{3}$ 0	GZUV F 82MD F	EB EB	( REFERENCE ( REFERENCE	) )		(CALCULATED VE (1000 X CALC:	RT. HA ROMENT	\LF W1DTH BEAM (→ DISPERSION(	ISIZE IN MILS A INCH/RATIO) AT	AT O TET UTOME PU END OF 8 DEC. MAGNE	(et) 37)
i	4 UI 5 II	BXMP F TZHX F	EB	( REFERENCE ( REFERENCE	) }		(1000 X CALC, (HALF WIDTH(M)	MOMENT LS) NF	C. DISPERSION Horz, ream a	PRIME(MR/RATIO) T WATST NEAR TO	) AT END OF 8 DEG, M ST OTHNE PGM, 11SF	1AG)    S)
					1		2 the Det Art Mat		2 4 505 8 5 600a C 100 8 64 8 8 8 8			
1	ន៍ ប៉ី 7 ព	TZHZ F TZUX F	EE ER	( REFERENCE ( REFERENCE	}		(Z PUS, UF U 1 (HALF MIDIMIMI	GT, HC LS) OF	DRZ. WAIST, IN Porrt, frám s	CH: 0=U TGT.: · T MATST NEAP TO	-50=50 IN, UPSTRM U St. – Ating pam. Ugg	TC) S)

-----

AGS Div. Tech. Note No. 176

•

Figure <u>1</u>e

55

I

27-0CT-81 11:43

. . . ...

. . ....

"U" LINE TRIM MAGNETS FROM HIS TO U TARGET

 $\sim$ 

 1 \$\$	ELEMENT Mame Larel	NAGNET Kind group *	Z(U/S) INCH	LENGTH TNCH	XAPER TNCH	YAPER THCH	P06/E PF nn#	R SUPPLY (IMARY	INFORM MAX- Kampe	ATION -SECONDARY- DDF AMPSIDEM
2AB 2BC NA	UP1 UQ1	DRIFT WDPOL 6.75D24 DRIFT BUAD M3B36 DRIFT	0.00 95.945 126.695 211.57 249.07	95,945 30,75 84,875 37,5	a, 11521 r	۲ ا <sup>ع</sup> د ۱ ( ده	UP1 UQ1	0.10 0.75	0.388 2.4	
16 17AB 17AB 17AB 17AB 17AB 17AB 17AB 17AB	UQ3 UP2 UQ4 UD4 UQ5	GUAD 4026 DRIFT WDPOL 6.75D24 DRIFT GUAD 4026 DRIFT WDPOL 6.75D24 DRIFT GUAD 4026	1230.444 1259.244 1268.821 1299.571 1532.204 1540.804 1779.439 1810.162 1833.762	28.6 9.575 202.633 28.635 218.635 218.635 20.75 23.573 28.6			UQ3-6 UP2 UQ3-6 UD4 UQ3-6	0.0750 0.10 -0.0750 0.10 -0.0750	0.400 0.388 0.400 0.388 0.400	
3773000444445 3773000444445	UQ8 UP3 UQ8A UQ8B UQ9 UD4A UQ10	QUAD 4026 DRIFT WDPOL 6.75D24 DRIFT QUAD 8016P DRIFT QUAD 8016P DRIFT QUAD 4026 DRIFT WDPOL 6.75D24 DRIFT QUAD 4026	3677.70 3706.30 3727.875 3876.248 3916.248 4262.248 4262.248 4262.248 4262.248 4262.248 4262.248 42697.66 4816.238 4816.238 4816.238 4846.988 5778.918	28.6 21.575 30.753 120.0 346.0 346.0 386.6 12 286.6 575 386.575 386.575 386.575 386.575 386.575 386.575 386.575 386.575 386.6 575 386.5 575 386.6 575 386.6 575 386.6 575 386.6 575 386.6 575 386.6 575 386.6 575 386.6 575 386.6 575 386.6 575 386.6 575 386.6 575 386.6 575 386.5 575 386.5 575 386.5 575 386.5 575 575 386.5 575 576 575 575 576 575 576 576 575 575			UQ8-9 UP3 UQ8A UQ8-9 UD4A UQ10	-0.0625 0.10 0.0625 0.0625 0.10 0.1000	0.250 0.388 0.250 0.250 0.388 0.388	
5968 5998 5998 5998 5998 5998 5998 5998	UQ13 UD7 UP4 UQ14	QUAD 8032P DRIFT WDPOL 6.75D24 DRIFT WDPOL 6.75D24 DRIFT DRIFT QUAD N3036	9350:511 9386:511 9408:929 9439:679 9438:934 9469:684 9492:012	36.0 22.418 30.745 745 22.329 32.329 37.5			UQ13 UD7 UP4 UQ14	0.3750 0.100 0.100 0.7500	1.200 0.388 0.388 2.400	

- . .

•.\_\_'

. . . . . . . . ....

Figure 1 f



$\underline{\square}$ \underline	
	<u>¥</u>
	<u></u>
	7
$H_{-0.25}$	
$9_{-0.50}$ $1/$ $1/$	V1
$\overline{\alpha}$	
0. 100. 200. 300. 400. 500. 600.	700.
<u>Z_(FEET_FROM_H13)</u>	
· · · · · · · · · · · · · · · · · · ·	2
	<u>У</u>

Figure 3 b

$\begin{array}{c} 1.00 \\ 0 \\ 1.00 \\ 0 \\ 0.75 \\ 0.75 \\ 0.00 \\ 0 \\ 0.25 \\ 0 \\ 0.25 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
$\begin{array}{c} 0.75 \\ \hline 0.75 \\ \hline 0.75 \\ \hline 0.50 \\ \hline 0.25 \\ \hline 0.25 \\ \hline 0.25 \\ \hline 0.00 \\ \hline 0.00 \\ \hline 7 \\ \hline \\ \hline 0.00 \\ \hline 7 \\ \hline \\ \hline 0.00 \\ \hline 7 \\ \hline \\ \hline \\ \hline \\ \hline 0.00 \\ \hline 7 \\ \hline \\$
0.75
₩   +   -   -     ₩   +       ₩   0.25       ×   0.00       ×   0.00       ×        ×
H   H     H     H  <
U   U </td
Z   0.25   ⊗   H1     >   0.00   S   S     ×   N   S   S     N   S   S   S     N   S   S   S     N   S   S   S     N   S   S   S
C   0.25   ⊗   H1     >   0.00   0.55   0.00     ×   1   1     W   1     W   1     W   1     W   1     W   1     W   1     W   1     W   1     W   1     W   1     W   1     W   1
→ 0.00 × 0.00 × 0.00 × 0.00 × 1 ↓ 0.25 N ↓ 0.25 ↓ 1 ↓ 0.25 ↓ 1 ↓ 0.25 ↓ 1 ↓ 0.25 ↓ 1 ↓ 0.25 ↓ 1 ↓ 0.25 ↓ 0.
× 0.00 <u>3 5</u> × <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u> <u>1</u>
$\frac{2}{10.25}$
Image: Windows   Image: Window   Image: Window   Image: Window<
<u>у -0.50</u> <u>Ц</u> <u>Щ</u> — 0.75
ц д-0.75
G-0.75
harding had B it had been
-1.00 $-1.00$ $-1.0$
۲. ۲.

<u>Figure 3 c</u>

			••
1,00.	3/2 U /2/2	LINE H13 TØ TGT	
H. U. U. U.	l I	1	÷.
U. /5			
() L			
	and the second	11 11 11	
	anno		
	a a' a' a'	() ()	
0.25			H1
>			Н2
~ 0.00 ×			¥2 -
M -0.23	94873		etidae
(O			21
			·
<u>LL</u>		<u> </u>	
<u>المالية المالية /u> مستحدية			AG
<u> </u>			Lv.
651	0. 700	750. 800.	850. <sub>e</sub>
MS PARAMETERS:	·····	HEEL FROM H13)	
LPHA, BETA, EPSILON (H,	V) AT H13: -5.6700 2.2620 0.0064	0.9870 0.1457 0.0064	No No
01 (-2727) U02 ( 3235 -A( 3847) U05-A( 3847)	;) UD1-3( 2998) UD1-3( 2998) UD1-3( UDA-9(-3534) UDAA ( - 240) UDA-9(-35	2998) UQ3-6(-2845) UQ3-6(-2845) UQ3-6(-2845) 534) UQ10 ( 1945) UQ11 ( 435) UQ19 ( 2014) U	UQ3-6(-2845) UQ7 (17276 013 (-2744) UD14 (1884)
UŠŽMD UŠŽMP UTŽAZ 339.74 -2040.37 -133		UH TGZUV 4.90 74.09	• • • • • • • • • • • • • • • • • • • •
		·····	
	174 mmm 60 am.mm		
MS PARAMETERS: LPHA, BETA, EPSILON (H,	V) AT H13: -5.6700 2.2620 0.0064	0.9870 0.1457 0.0064	
11, (-2727), UO2, (,3235	)_UD1-3(_2778)_UD1-3(_2778)_UD1-3(	_2??8/_UQ3-6(_2645)_UQ3-6(_2645)_UQ3-6(-2645)	_UQ3-6(-2945)_UQ7_(_1727)_
-o( 384/) UDD-6( 384/) U8%PD U8%PP UT%HZ S39,74 -2040 97 -4	UUB-4(-3354) UUBA ( 240) UUB-9(-3 UTXHX UTXYZ UTXYX TGX 40 33 UTXYZ UTXYX TGX	334) UMIO ( 1345) UMII ( -514) UQI2 (-2689) U UH - TCZUV 5 - 70 - 25 - 25	W13 (-2511) UQ14 ( 1963) — Figure 4
www.ell. awww.call "it	an 170aa Voov 20024 Da	2010 LI0LD	

;

ŝ

" U LINE - H13 THRU UTGT --H13 MOM. DISP & SEXTUPOLES ADDED" Õ. (CHANGE TO INCHES FOR MAGNET SIZES & THOUSAND INCH LENGTH) 15. 1. " IN" 2.54; 15. 8. "KIN" 25.4; "H13" ,365505' .930326 .092763 .894559 0.0 0.12 29.4x (FOR SECOND ORDER CALC.) 17. 12. "H13" .984801 0. 0. 0. 0. -.7024655; 13. 2.3 3. 0.0\$ 13. 4. : (UPDATE'R1 & R2 MATRIX & ADD H5 DISPERSION) 14. 1. 0. 0. 0. -1.145 1. 14. 0. 1. 0. 0. 0. -2.95 2.; 1.5 13. 3. 0.0; ( MATRIX ELEM. DIMENSIONS: R16 = INCH/Z, R26= MR/Z ) 3. 0.21157 jozz 0.00202 1. 5. 0.0195; "ÚQ2" (0375 -8.73765 1. 5. 0.0188: 3. (UD1-3 WITH POLEFACE ROTATION, EACH BEND = 1.4156 DEG) "UD1" 0.0819 11.85804 0.0; 2. 0.7077; 2+ .7077:4. 3. 0.018098; Ž, "UD2" 0.0819 11.85804 0.0; 2. 0.7077; 0.7077; 4. 0.018098; З. 2. 0.7077, 4. "UD3" .0819 11.85804 0.0; 2. 0.7077; 3. 0.3005 3. 0.32388; 5. "U<u>R3"</u>0.0286 2.00208 1.; 3. 0.27296; "UR4" 0.0286 -2.00208 1.; 5. ä. 0.27296: 5. "UR5" 0.0286 -2.00208 1.; 0.27296; 3. 5; "UQ6" 0.0286 2.00208 1.; 3, 0,27296; "UQ7" 5. 0.0286 1.22839 1.; 13. 3. \* 3. 0.45806; 0,400; "SIA " З. 18. .02606 5.9342 2.063; 3. 0,02047; (UD5-4 WITH POLEFACE ROTATION, BEND=4.00 DEG) 2. 2.00; 4. UD5 0.0375 66.82688 0.0; 2. 2.00; "8DSX" 0.0375 -3.4622 2.0; 18. 0.04201; \_\_\_\_\_\_805X...; З, 0.0375 -3.4622 2.03 18. "UD6" 0.0375 68.82688 0.0; 2. 2.00; 27 2.00; 4. 0.02648; S1B з. '.02606 5.9342 2.063<u>;</u> 18. 0.06310; 3. "ÜÜÄ" .0286 -2.06885 1.03 5. З. .18995: ( UQGA ONLY VERT, FOCUSING AS WE RAN) "UQ8A" 5. .020 -.03679 1.0; 3. 0.300; 0,45281; 3+

Figure 5 a

•

Ł

 $\sim$ 

N

AGS

Div.

Tech.

No

Ē

No

176

5. "UQ9" 0.0286 2.06885 1.0; 3. 0.300; 3. 48126; .0286 -1.27525 1.0; 3. 500; 3. 0.500; 3. 0.500; 3. 0.28386; 5. "UQ11" 0.0286 -0.41439 1.0; 3. 0.28386; 5. "UQ12" 0.036 2.71707 1.0; 3. 0.4878; 5. "UQ12" 0.036 2.55482 1.0; 3. 0.10551; 5. "UQ14" 0.0375 -6.53737 1.0; 3. 0.100; 3. 0.15315; 13. 4.; 3. "UTGT" 0.0; 5. "UTGT" 0.0; 5. SENTINEL SENTINEL

4

1

Figure 5 b

1. 3. 1.

- 23 -

AGS Div. Tech. Note No. 176

ł



Div. Tech. Note No.

	<i>17</i> <b>1 1 1</b>		<b>T</b> (2) <b>T</b> (3) <b>T</b> (3)		
<u> </u>	<u> </u>	LINE HI3		/	
Ta a la construcción de la constru					
1.50				6221 (49452) or 310	• (1010)#
	For UQ8.	A IKA (KG/in)		ALL	
<u> </u>	X0.015 (.037	)			eensen
	0.23	5 (.624)		X	
♡0.50L 🖋		70 KA, 1.73 Kola			
Smarts and states	م منه مرکز کرد منه منه مرکز کرد منه هم دی		$\boldsymbol{\chi}$	₩,H2	
<u>.</u> 0.00 <u>55</u>		() (			
			8 (		
- <u>W-0.50</u>	A A A A A A A A A A A A A A A A A A A		۲۵۵۰ <sup>(</sup> ۲۵۵) ۲۹۹۹ (۲۹۵) ۲۹۹۹ (۲۹۵) ۲۹۹۹ (۲۹۵) ۲۹۹۹ (۲۹۵) ۲۵۵۰ <sup>(۲</sup> ۹۹) ۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹۹ (۲۹۹		
		0.25 (.624)	an a	<u> </u>	
$\frac{0}{1-1.00}$	\$ \$				
	5 	KE	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		
<u></u>	<u>`~. 70</u> ,	<u>xA 1.73 m X</u>			676699
**************************************		می می اور			
<u> </u>					
3UU.	<u>400. 500</u>	I. GUU. <del>TEETEDAM</del>		800.	900.
	L		11101		
5		/ 			90 · · //
		\$			
	FFFECT DB	DARSonna Const	ant the l	li a ea	
			anne <u>e v</u> and	and the second	
••••••••••••••••••••••••••••••••••••••				Figure 7	

