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EDDY CURRENT HEATING OF BOOSTER DIPOLE VACUUM **CHAMBER**

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EDDY CURRENT HEATING OF BOOSTER DIPOLE VACUUM CHAMBER

AD *Booster Technical Note No.* **71**

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INTRODUCTION:

This report covers two experiments performed to determine the magnitude of eddy current heating of the Booster dipole vacuum chamber. Results are presented for insulated and uninsulated chambers.

In the results secticn graphs of temperatures vs. time illustrate thermal gradients and terminal temperatures encountered. Also included are the calculated values of heat generation, convection and conduction.

Raw data and sample calculations are included so the reader may verify the assumptions made.

BACKGROUND:

The vacuum chamber used for the tests was manufactured from 14Ga. (.075") Gr 316L stainless steel. The dimensions of the chamber are shown in Figure 1.

Two separate experiments were performed to the vacuum chamber section described above. In the first experiment the exterior of the chamber was uninsulated. In the second run the chamber was insulated with three layers of "Ultra Insulation K" (Oike Industrial Co., Ltd). Figure 3 gives a detail of the insulation. In both cases the interior of the chamber was tightly packed with fiberglass insulation to simulate vacuum.

tion of the thermocouples for both cases are shown in Figure 2. Thermocouples were used to measure temperatures during the tests. Loca-

The test specimen was loaded into the dipole test magnet and the magnet powered with the current excitation shown in Figure 4 .

During the test, temperatures were recorded at five minute intervals for 120 minutes and 285 minutes respectively.

After powering the insulated sample for 285 minutes power to the magnet was terminated and the specimen allowed to cool in place. During cooling, temperatures were measured at one minute intervals.

The data collected during cooling of the insulated chamber was used to calculate convection and conduction coefficients in the absence of the unknown heat generation.

The calculated convection and conduction parameters were then applied to the powered data to determine the heat generated by eddy currents.

RESULTS :

Measured temperatures around the chamber $\frac{1}{4}$ circumference are presented graphically as a function of time for both insulated and uninsulated data. Circumferential thermal gradients and terminal temperatures are of particular interest.

At the given excitation, power dissipation for the vacuum chamber is 32 watts/linear ft. of chamber.

Power dissipation was calculated for 32 different time intervals between the insulated and uninsulated data. Repeatability over a wide range of temperatures was excellent (see Tables 2 and 3, calculations section).

The conductive resistance of the insulation (R_K) was found to be 0.776 ^{oK}/watt-linear ft.

The mean convective resistance (\bar{R}_{h}) within the magnet aperture is 0.890 ^{oK}/watt-linear ft. Convective resistance is assumed constant for a surface temperature range of 30-55°C.

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UNINSULATED CHAMBER

PT-POLE FACE

INSULATED CHAMBER

INSULATION OF CHAMBER

CURRENT EXCITATION

 $\overline{7}$

CALCULATIONS:

Based upon temperature gradients observed and chamber geometry the average chamber temperature T_{ss} is taken as;

$$
\overline{T}_{SS} = \overline{T}_D (.2) + T_B (.8)
$$

During cool down of the chamber;

$$
Qout = \frac{\rho V C \rho \Delta \bar{T}_{SS}}{\Delta t}
$$

V - Volume of 1 foot section of chamber = 2.7867x10⁻⁴m³
\n
$$
\rho
$$
 - Density of stainless steel = 7817 kg/m^3
\n $C\rho$ - Stainless steel specific heat = 461 $J/kg\degree$ k
\nAt - Time increment = 60 sec.

Conductive Resistance (R $_{\rm K}$)

$$
\text{Quot } \uparrow \overset{\bar{T}_{1}}{\neq} R_{K}^{\text{R}}
$$

$$
T_{\text{ss}}
$$

$$
R_K = \frac{\bar{T}_{SS} - \bar{T}_i}{\sqrt{2\pi}} \left(\frac{\delta K}{\text{Watt}} - \text{linear ft} \right)
$$

Ti – average insulation temperatuare = $\mathrm{T_{E}}$ + $\mathrm{T_{F}}$ 2

Convective Resistance (\bar{R}_{hc})

$$
\text{Quot } \uparrow \frac{1}{\frac{1}{T}} \mathop{\mathbf{R}}\limits_{\mathop{\mathbf{T}}\limits_{\mathop{\mathbf{I}}}}^{T\mathop{\mathbf{a}}}
$$

$$
\bar{R}_{\text{hc}} = \frac{T_i - T_a}{Quot} \quad (\text{oK}_{\text{Watt}} - \text{linear ft})
$$

 T_a - ambient temperature within magnet aperture.

 $*$ \bar{T}_F extrapolaited from previous test

 R_K = .780 \circ ^K/watt - ft \bar{R}_{hc} = .890 \circ ^K/watt - ft \bar{R}_T = 1.67 \circ K/watt - ft During operation heat generation (Qgen) is given by:

$$
\text{Qgen} = \frac{\rho V C \rho \Delta \bar{T}_{SS}}{\Delta t} + \frac{\bar{T}_{SS} - \bar{T}_{A}}{R_{T}}
$$

 \bar{T}_{ss} and \bar{T}_{a} defined previously are averaged over the measurement interval.

$$
\bar{Q} = 32.6
$$
 watts/ft

* Excluded as transient data

 $Qgen = 31.4$

 \mathbf{I}

*excluded as transient data

