

Additional Booster shielding calculations

R. Casey

October 1987

Collider Accelerator Department
Brookhaven National Laboratory

U.S. Department of Energy

USDOE Office of Science (SC)

Notice: This technical note has been authored by employees of Brookhaven Science Associates, LLC under Contract No.DE-AC02-76CH00016 with the U.S. Department of Energy. The publisher by accepting the technical note for publication acknowledges that the United States Government retains a non-exclusive, paid-up, irrevocable, world-wide license to publish or reproduce the published form of this technical note, or allow others to do so, for United States Government purposes.

DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or any third party's use or the results of such use of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof or its contractors or subcontractors. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

ADDITIONAL BOOSTER SHIELDING CALCULATIONS

AD

Booster Technical Note

No. 93

R. CASEY

OCTOBER 22, 1987

ACCELERATOR DEVELOPMENT DEPARTMENT
Brookhaven National Laboratory
Upton, N.Y. 11973

ADDITIONAL BOOSTER SHIELDING CALCULATIONS

R. CASEY

I. INTRODUCTION

An earlier note by Gollon¹ estimated shielding requirements for the Booster. Since the publication of that note, a number of changes have occurred which require additional analysis. The purpose of this report is to document those analyses.

II. SOURCE TERMS

Beam losses associated with Booster have been previously estimated by Lee². However, for purposes of shielding design, a more conservative set of loss assumptions have now been used to assure that the shielding analysis has an adequate margin of safety³. The new assumptions are listed in Table I.

Table I

ASSUMPTIONS FOR SHIELDING DESIGN

- Operating Beam - $6E13$ p/s @ 1.5 GeV
- 20% Beam losses at injection - $1E13$ p/s @ 200 MeV
- 1% Beam loss during acceleration - $6E11$ p/s @ 0.7 GeV
- 1% Beam loss at extraction - $6E11$ @ 1.5 GeV
- Maximum Credible Accident - 100% of beam at a point

A significant source has been added since the previous note. A combination beamstop/scrapper has been added to the planned operation. The purpose of this device is to catch as much of the beam losses at one point rather than have it lost around the ring in general, and to provide a dump for accelerated beam that cannot be ejected to the AGS. Design considerations for the dump have been discussed by Stevens⁴. For purposes of the shielding calculation, we assume that the dump receives beam primarily during studies, which are performed 70 days/yr, 8 hours/study. Studies are assumed to average 1.5×10^{13} p/s at 1.5 GeV.

III. SHIELDING CRITERIA

The design criteria for shielding is to limit the dose rate in uncontrolled or normally occupied areas to less than 0.5 mRem/hr under normal operating conditions. Higher levels are permitted if the access control and warning systems as specified in OH&S Guide #2.4.0 are met.

IV. SHIELDING CALCULATIONS

Calculations are made using the formulation proposed by Tesch⁵ for estimating dose equivalent per proton outside a lateral concrete shield when protons strike a long copper target:

$$H = \frac{H_0}{r^2} \exp(-d/\lambda)$$

Here H is in rem/p, r is in meters, and d is in gcm⁻². From references 1 and 5, the other parameters required for these calculations are:

Table II

<u>Beam Energy</u>	<u>λ</u>	<u>H_0</u>
200 MeV	72 g/cm ²	3x10 ⁻¹⁴ rem-m ² /p
700 MeV	95 g/cm ²	6x10 ⁻¹³ rem-m ² /p
1.5 GeV	110 g/cm ²	1.3x10 ⁻¹² rem-m ² /p

Attached are Tables III, IV, and V showing the results of these calculations at each energy at a given beam loss. These results can be used to show the resulting dose rates for each of the situations reviewed below.

A. NORMAL BEAM LOSSES AT INJECTION OR ACCELERATION

We assume that one-half of the losses listed in Table I occur at a single point where the vertical thickness of shield is 15 feet and the minimum horizontal thickness is 20 feet.

5x10 ¹² p/s @ 200 MeV -	0.18 mRem/hr (vertical), <0.01 mRem/hr (horizontal)
3x10 ¹¹ p/s @ 700 MeV -	3.3 mRem/hr (vertical), 0.12 mRem/hr (horizontal)

B. NORMAL BEAM LOSSES AT EXTRACTION

We assume that one-half of the extraction loss occurs on the extraction magnet located under the 10 foot earth shield over Bldg. 914.

3x10 ¹¹ p/s @ 1.5 GeV -	525 mRem/hr (vertical)
------------------------------------	------------------------

In addition, a shield wall will be provided between the occupiable area of Bldg. 914 and the portion containing the Booster line. This wall must be sufficient to reduce the levels in the occupiable part to <0.5 mRem/hr. The wall is at a distance of 37 feet from the principal loss point (the extraction magnet). Table VI shows the result of this calculation. An equivalent of 19 feet of earth will be necessary for this shield wall.

C. BEAM DUMP

The beam dump consists of a 18.3cm radius steel ($\rho=8.1 \text{ g/cm}^3$) object which will be enclosed in a 20cm thick marble (2.7 g/cm^3) shield. The additional shielding provided by the marble and steel is equivalent to 3.7 feet of earth, which gives the equivalent of 18.7 feet of shielding vertically. At the location of the dump there is approximately 60 feet horizontal shielding.

$$1.5 \times 10^{13} \text{ p/s @ } 1.5 \text{ GeV} - 130 \text{ mRem/hr (vertical)} \\ < 0.05 \text{ mRem/hr (horizontal)}$$

The dose equivalent rate at the fence will be increased by scattered radiation from the high dose rate penetrating vertically. The area of the radiation levels vertically is about 600 feet². The scattered levels at the fence from the emerging vertical fields are approximated by the formula

$$D_s = \frac{A}{24\pi d^2} D_v$$

Where D_v is the dose equivalent rate vertically, A is the area of the berm through which D_v emerges, and d is the distance from the center of A to the fence line.

$$A = 600 \text{ ft}^2 \\ D_v = 210 \text{ mRem/hr} \\ d = 42 \text{ ft}$$

$$D_s = \frac{600 \text{ ft}^2}{24\pi (42 \text{ ft})^2} \times 130 \text{ mRem/hr} = 0.6 \text{ mRem/hr}$$

E. SKYSHINE

The high energy portion of the emerging neutron field can create radiation fields at ground level from scattering in air. This type of radiation is commonly called skyshine radiation and can be estimated from the formula $H(r) = 3 \times 10^{-13} \exp(-r/\lambda)/r^2 \text{ rem/n}$ developed by Stevenson and Thomas⁶. The number of neutrons escaping can be estimated from the of the escaping field. Therefore, from the beam dump

$$H(r) = 3 \times 10^{-13} \frac{\exp(-r/\lambda)}{r^2} \frac{130 \text{ mRem/hr}}{18.4 \frac{\text{nRem}}{\text{ncm}^{-2}}} \text{ Rem/n} \\ = 3.4 \times 10^{-6} \frac{\exp(-r/\lambda)}{r^2} \frac{\text{n}}{\text{cm}^2 \text{ hr}} \frac{\text{rem}}{\text{n}} \times 600 \text{ ft}^2 \times \left(\frac{30.48 \text{ cm}}{\text{ft}} \right)^2 \\ H(r) = 1.2 \frac{e^{-r/\lambda}}{r^2} \text{ rem/hr} \quad \lambda = 700 \text{ m}$$

The nearest routinely occupied area is approximately 450 feet (140m) away.

$$H(r) = \frac{1.2 e^{-r/\lambda}}{r^2} = \frac{1.2 e^{-140/700}}{(140)^2} = 4.6 \times 10^{-5} = 46 \text{ } \mu\text{Rem/hr}$$

The site boundary is approximately 1.1 km

$$H(1.1 \text{ km}) = \frac{1.2 e^{-1100/700}}{(1100)^2} = 2.1 \times 10^{-7} \text{ Rem/hr} = 0.2 \text{ } \mu\text{Rem/hr}$$

Another skyshine source that should be considered is the emerging field through the top of 914 from the routine extraction losses. The area of this source is approximately 400 ft².

$$\begin{aligned} H(r) &= 3 \times 10^{-13} \frac{\exp(-r/\lambda)}{r^2} \frac{525 \text{ mRem/hr}}{18.4 \text{ nRem/cm}^{-2}} \times 400 \text{ ft}^2 \times \left(\frac{30.48}{\text{ft}} \right)^2 \\ &= 3.2 \frac{e^{-(r/\lambda)}}{r^2} \text{ rem/hr} \end{aligned}$$

at 140 m

$$H(140) = 3.2 \frac{e^{-(140/700)}}{(140)^2} = 134 \text{ } \mu\text{Rem/hr}$$

at site boundary

$$H(1.1 \text{ km}) = 3.2 \frac{e^{-1100/700}}{(1100)^2} = .55 \text{ } \mu\text{Rem/hr}$$

Therefore, the total outside dose in a 2000 hr. work year at 140m is

$$\begin{aligned} &46 \times 10^{-6} \text{ rem/hr} \times 70 \text{ day} \times 8 \text{ hr/day} + 134 \times 10^{-6} \times 140 \text{ day/yr} \times 8 \text{ hr/day} \\ &= 26 + 150 = 176 \text{ mRem/yr.} \end{aligned}$$

and at 1.1 km

$$H(1.1 \text{ km}) = .2 \text{ } \mu\text{Rem/hr} \times 70 \times 8 + .55 \text{ } \mu\text{Rem/hr} (130 \times 24 + 70 \times 16) = .1 + 2.3 = 2.4 \text{ mRem/yr.}$$

F. MAXIMUM CREDIBLE ACCIDENT

If the full circulating beam at 1.5 GeV is lost at a point in the ring, the resulting dose rate can be calculated using the Tesch formula above

$$\begin{aligned} 6 \times 10^{13} \text{ p/s @ 1.5 GeV} &- 105 \text{ Rem/hr (vertical - 914 roof)} \\ &4.7 \text{ Rem/hr (vertical - ring)} \end{aligned}$$

Beam loss monitors which alarm and interlock the beam will be necessary to assure that substantial beam losses are promptly detected and inhibited. It should be recognized that the assumption of full beam being lost at a single point is very conservative. Even in the absence of radiation monitors, such a beam loss would be quickly observed by the operators and corrected.

REFERENCES

1. P. Gollon, "Booster Tunnel Shielding Calculation", Booster Tech. Note #66 (1986).
2. Y. Y. Lee, Memorandum Y.Y. Lee to P. Gollon, dated 6/16/86.
3. R. Casey, Memorandum R. Casey to B. Weng, dated 6/8/87.
4. A. Stevens, Memorandum A. Stevens to B. Weng, dated 7/30/87.
5. K. Tesch, Radiation Protection Dosimetry 11,165 (1985).
6. G. R. Stevenson and R. H. Thomas, Health Physics, 46, p.115 (1984).

TABLE III

100 MeV SHIELDING VALUES I RING

LIST RUN

Enter the energy of the incident proton: 200

ENTER THE APPROPRIATE HCASC 3e-14

ENTER THE APPROPRIATE LAMBDA 72

Enter the beam losses that you want to calculate (p/s) 1e13

This calculation is for a proton energy of 200

It uses a lambda = 72 g/cm^2

Shielding Thickness Ft. (soil)	Dose Rate mRem/Hr.
10	29.09
11	11.83
12	4.85
13	2.01
14	0.84
15	0.35
16	0.15
17	0.06
18	0.03
19	0.01
20	0.00
21	0.00
22	0.00

This calculation assumes a point loss of 1E+13 p/s
Ok

TABLE IV
700 MeV SHIELDING VALUES IN RING

RUN
Enter the energy of the incident proton: 700
ENTER THE APPROPRIATE HCASC $6e-13$
ENTER THE APPROPRIATE LAMBDA 95
Enter the beam losses that you want to calculate (p/s) $3e11$
This calculation is for a proton energy of 700
It uses a lambda = 95 g/cm²

Shielding Thickness Ft. (soil)	Dose Rate mRem/Hr.
10	110.45
11	54.00
12	26.64
13	13.25
14	6.63
15	3.34
16	1.69
17	0.86
18	0.44
19	0.23
20	0.12
21	0.06
22	0.03

This calculation assumes a point loss of $3E+11$ p/s
Ok

TABLE V

1500 MeV SHIELDING VALUES IN RING

LOAD"RUN

Enter the energy of the incident proton: 1500

ENTER THE APPROPRIATE HCASC 1.3e-12

ENTER THE APPROPRIATE LAMBDA 110

Enter the beam losses that you want to calculate (p/s) 3e11

This calculation is for a proton energy of 1500

It uses a lambda = 110 g/cm²

Shielding Thickness Ft. (soil)	Dose Rate mRem/Hr.
10	525.99
11	278.25
12	148.52
13	79.89
14	43.28
15	23.59
16	12.93
17	7.12
18	3.94
19	2.19
20	1.22
21	0.68
22	0.38

This calculation assumes a point loss of 3E+11 p/s

Ok

TABLE VI
SHIELDING VALUES FOR 914 SHIELD WALL

RUN
Enter the energy of the incident proton: 1500
ENTER THE APPROPRIATE HCASC 1.3e-12
ENTER THE APPROPRIATE LAMBDA 110
Enter the beam losses that you want to calculate (p/s) 3e11
This calculation is for a proton energy of 1500
It uses a lambda = 110 g/cm²

Shielding Thickness Ft. (soil)	Dose Rate mRem/Hr.
10	46.67
11	27.17
12	15.84
13	9.24
14	5.39
15	3.15
16	1.84
17	1.08
18	0.63
19	0.37
20	0.22
21	0.13
22	0.07

This calculation assumes a point loss of 3E+11 p/s
Ok