

BNL-104062-2014-TECH AGS.SN185;BNL-104062-2014-IR

Contribution of F5, F10 Extraction Magnets to Slow Spill

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June 1986

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U.S. Department of Energy

USDOE Office of Science (SC)

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Number	185

AGS Studies Report

Date(s)June	6, 1985 Time(s)
Experimenter(s)	I-H Chiang, R. DiFranco, C. Eld, J. Funaro,
	J.W. Glenn, R. Lockey, A. McNerney
Reported by	I-H Chiang
Subject	Contribution of F5, F10 Extraction Magnets to
	Slow Spill

Observations and Conclusion

Technical Note 199 reported the transfer function of the extraction power supplies. There existed a large component of LILCO 360 in the spill can not be explained by the ripple of the extraction power supplies. The present effort is to establish a permanent easy-to-use system such that we can monitor the power supplies and the slow spill routinely. The system consists of a HP 3651A Signal Analyzer, two sets of cables between control room and the power supplies houses. Also some work was done on the power supplies such that we can easily drive the power supplies with non 60 cycle source. A dedicated source synchronizer was built. This is to provide a Syn. trigger for the HP analyzer. Since the SEB ripple can be derived from various sources, the Syn. box provides a mean to average out the uncorrelated signal.

During the study, it was observed that the F10 power supplies has large LILCO Syn. ripples. J.W. Glenn observed that there is correlation between the spill ripple and the F10 power supply ripple. The transfer function of the F5 and F10 to the slow spill were measured. The results are shown in Tables 1 and 2.

From Table 2 the implied transfer function of 360 component is 2.1% [(2.09 + 2.29)/2] spill modulation per 34.5 mv [(35.2 + 33.7)/2]. Which is equivalent to 16.4 mv per 1% of beam modulation. Figures 1-4 show the effects of the F10 360 Hum Bucking circuit. The 360 component change from 36.41 mv to 6.1 mv. The net reduction is about 30 mv. From the measured transfer function we predict the 360 component of spill should be reduced by

The dc component of the C10SEC is 395 mv. The predicted reduction at 360 is 7.1 mv. The 360 components of C10SEC is 14 mv and 7.1 mv before and after Hum Bucking circuit activated. The net reduction is 6.9 mv which agree with the prediction. This agreement gives more confidence about the method. We will continue to perform the measurement of the other pertinent power supplies. With all the data in hand, we will then decide how to proceed to reduce the ripple of the power supplies.

1d

Freq	Power su	pply mv.		C10 Sec	Meas.		Ratio
	DC	@freq	%	DC	@Freq	7/-	
50.00	5167.00	491.00	9.50	585.50	331.30	56.58	5.95
80.00	5245.00	402.00	7.66	1030.00	536.00	52.04	6.79
140.00	5360.00	214.30	4.00	880.00	293.00	33.30	8.33
200.00	5430.00	113.00	2.08	811.00	146.50	18.06	8.68
260.00	5489.00	70.60	1.29	784.00	66.40	8.47	6.58
314.00	5489.00	51.20	Ø. 93	699.00	41.20	5.89	6.32
380.00	5489.00	35.10	0.64	813.00	23.50	2.89	4.52
		F10					
Freq	Power sup	oply mv.		C10 Sec	Meas.		Ratio
Freq	Power sup			C10 Sec	Meas.		Ratio
	Power sup DC	oply mv.	%	C10 Sec DC	Meas. @Freq	%	Ratio 9.69
50.00	Power sup DC	oply mv. Ofreq 104.00	%	C10 Sec DC 798.50	Meas. @Freq 111.60	% 13.98	9.69
50.00	Power suj DC 7210.00 7230.00	oply mv. Ofreq 104.00	% 1.44 Ø.96	C10 Sec DC 798.50 798.50	Meas. @Freq 111.60 68.40	% 13.98 8.57	9.69 8.89
50.00 80.00	Power sup DC 7210.00 7230.00 7220.00	oply mv. @freq 104.00 69.70 46.80	% 1.44 Ø.96	C10 Sec DC 798.50 798.50 767.40	Meas. @Freq 111.60 68.40 37.80	% 13.98 8.57 4.93	9.69 8.89 7.60
50.00 80.00 140.00	Power suj DC 7210.00 7230.00 7220.00 7240.00	oply mv. Efreq 104.00 69.70 46.80 40.40	% 1.44 Ø.96 Ø.65	C10 Sec DC 798.50 798.50 767.40 775.00	Meas. @Freq 111.60 168.40 37.80 29.80	% 13.98 8.57 4.93 3.85	9.69 8.89 7.60 6.89
50.00 80.00 140.00 200.00	Power suj DC 7210.00 7230.00 7220.00 7240.00	oply mv. @freq 104.00 69.70 46.80 40.40 36.80	% 1.44 Ø.96 Ø.65 Ø.56 Ø.51	C10 Sec DC 798.50 798.50 767.40 775.00 794.00	Meas. @Freq 111.60 68.40 37.80 29.80 24.80	74 13.98 8.57 4.93 3.85 3.12	9.69 8.89 7.60 6.89 6.12
50.00 80.00 140.00 200.00 260.00	Power sup DC 7210.00 7230.00 7220.00 7240.00 7215.00	oply mv. @freq 104.00 69.70 46.80 40.40 36.80 35.20	% 1.44 0.96 0.65 0.56 0.51 0.49	C10 Sec DC 798.50 798.50 767.40 775.00 794.00 793.00	Meas. @Freq 111.60 168.40 37.80 29.80 24.80 16.60	74 13.98 8.57 4.93 3.85 3.12 2.09	9.69 8.89 7.60 6.89 6.12 4.30

Transfer Function

tabel i F5







