



BNL-104062-2014-TECH

AGS.SN185;BNL-104062-2014-IR

Contribution of F5, F10 Extraction Magnets to Slow Spill

I. H. Chiang

June 1986

Collider Accelerator Department
Brookhaven National Laboratory

U.S. Department of Energy

USDOE Office of Science (SC)

Notice: This technical note has been authored by employees of Brookhaven Science Associates, LLC under Contract No.DE-AC02-76CH00016 with the U.S. Department of Energy. The publisher by accepting the technical note for publication acknowledges that the United States Government retains a non-exclusive, paid-up, irrevocable, world-wide license to publish or reproduce the published form of this technical note, or allow others to do so, for United States Government purposes.

DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or any third party's use or the results of such use of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof or its contractors or subcontractors. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

AGS Studies ReportDate(s) June 6, 1985 Time(s) _____Experimenter(s) I-H Chiang, R. DiFranco, C. Eld, J. Funaro,
J.W. Glenn, R. Lockey, A. McNerneyReported by I-H ChiangSubject Contribution of F5, F10 Extraction Magnets to
Slow SpillObservations and Conclusion

Technical Note 199 reported the transfer function of the extraction power supplies. There existed a large component of LILCO 360 in the spill can not be explained by the ripple of the extraction power supplies. The present effort is to establish a permanent easy-to-use system such that we can monitor the power supplies and the slow spill routinely. The system consists of a HP 3651A Signal Analyzer, two sets of cables between control room and the power supplies houses. Also some work was done on the power supplies such that we can easily drive the power supplies with non 60 cycle source. A dedicated source synchronizer was built. This is to provide a Syn. trigger for the HP analyzer. Since the SEB ripple can be derived from various sources, the Syn. box provides a mean to average out the uncorrelated signal.

During the study, it was observed that the F10 power supplies has large LILCO Syn. ripples. J.W. Glenn observed that there is correlation between the spill ripple and the F10 power supply ripple. The transfer function of the F5 and F10 to the slow spill were measured. The results are shown in Tables 1 and 2.

From Table 2 the implied transfer function of 360 component is 2.1% [(2.09 + 2.29)/2] spill modulation per 34.5 mv [(35.2 + 33.7)/2]. Which is equivalent to 16.4 mv per 1% of beam modulation. Figures 1-4 show the effects of the F10 360 Hum Bucking circuit. The 360 component change from 36.41 mv to 6.1 mv. The net reduction is about 30 mv. From the measured transfer function we predict the 360 component of spill should be reduced by

$$30 \text{ mv}/16.4 \text{ (mv/\%spill)} = 1.8\%$$

The dc component of the C10SEC is 395 mv. The predicted reduction at 360 is 7.1 mv. The 360 components of C10SEC is 14 mv and 7.1 mv before and after Hum Bucking circuit activated. The net reduction is 6.9 mv which agree with the prediction. This agreement gives more confidence about the method. We will continue to perform the measurement of the other pertinent power supplies. With all the data in hand, we will then decide how to proceed to reduce the ripple of the power supplies.

ld

Freq	tabel 1 F5		Transfer Function				Ratio
	Power supply mv. DC	@freq	%	C10 Sec DC	Meas. @Freq	%	
50.00	5167.00	491.00	9.50	585.50	331.30	56.58	5.95
80.00	5245.00	402.00	7.66	1030.00	536.00	52.04	6.79
140.00	5360.00	214.30	4.00	880.00	293.00	33.30	8.33
200.00	5430.00	113.00	2.08	811.00	146.50	18.06	8.68
260.00	5489.00	70.60	1.29	784.00	66.40	8.47	6.58
314.00	5489.00	51.20	0.93	699.00	41.20	5.89	6.32
380.00	5489.00	35.10	0.64	813.00	23.50	2.89	4.52

Freq	tabel 2 F10		Transfer Function				Ratio
	Power supply mv. DC	@freq	%	C10 Sec DC	Meas. @Freq	%	
50.00	7210.00	104.00	1.44	798.50	111.60	13.98	9.69
80.00	7230.00	69.70	0.96	798.50	68.40	8.57	8.89
140.00	7220.00	46.80	0.65	767.40	37.80	4.93	7.60
200.00	7240.00	40.40	0.56	775.00	29.80	3.85	6.89
260.00	7215.00	36.80	0.51	794.00	24.80	3.12	6.12
320.00	7230.00	35.20	0.49	793.00	16.60	2.09	4.30
380.00	7207.00	33.70	0.47	795.70	18.20	2.29	4.89

F10 V

RANGE: 20 dBV

STATUS: PAUSED

TIME: 28

A: MAG

10
Vrms

Fig 1

F10 Volt
360 Hum Bucking off

10
dB
/DIV

X: 360 Hz
Y: 36.41 mVrms

1
mVrms

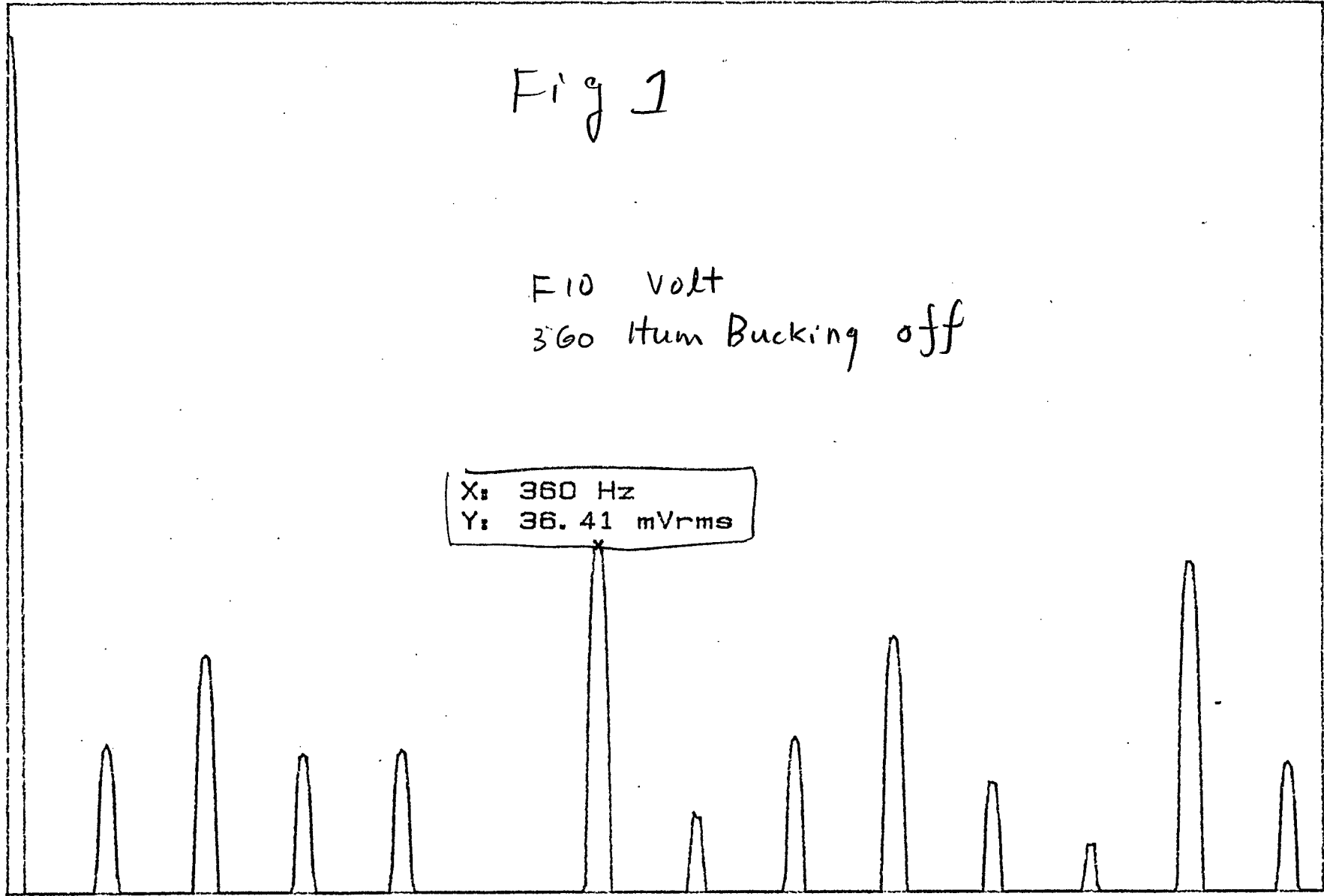
START: 0 Hz

BW: 7.6388 Hz

STOP: 800 Hz

X: 360 Hz

Y: 36.41 mVrms



RANGE: 20 dBV

STATUS: PAUSED

A: MAG

TIME: 9

10
Vrms

Fig 2

10
dB
/DIV

F10 Voltage
360 Hum Bucking on

X: 720 Hz
Y: 31.39 mVrms

X: 120 Hz
Y: 11.81 mVrms

X: 50 Hz
Y: 4.441 mVrms

X: 360 Hz
Y: 6.092 mVrms

1
mVrms

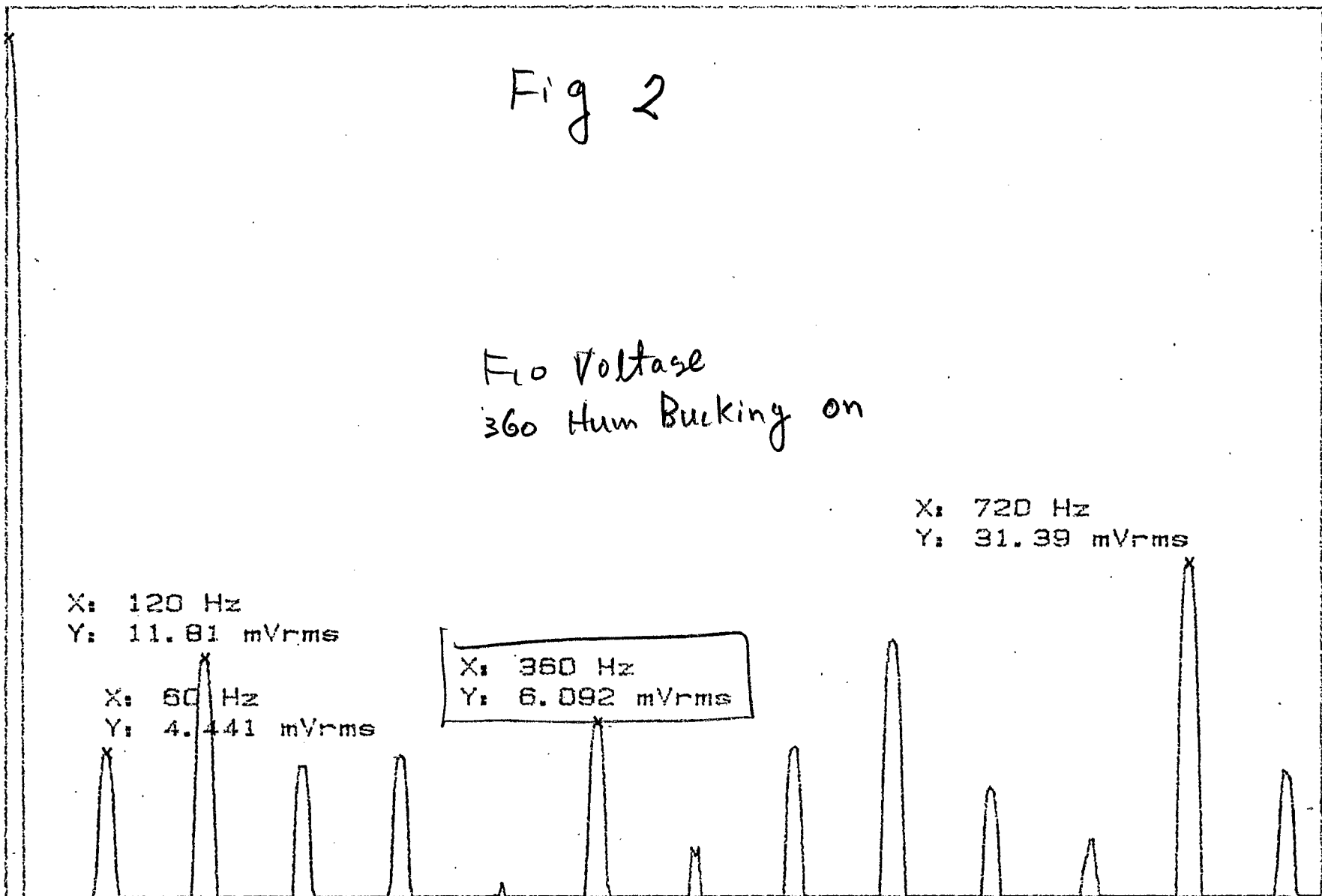
START: 0 Hz

BW: 7.6388 Hz

STOP: 800 Hz

X: 0 Hz

Y: 7.253 Vrms



RANGE: 10 dBV

STATUS: PAUSED

TIME: 50

A: MAG

3.162
Vrms

Fig 3

X: 0 Hz
Y: 395.1 mVrms

C10 SEC
F10 360 Hum Buck off
↓

10
dB
/DIV

X: 60 Hz
Y: 19.45 mVrms

X: 360 Hz
Y: 14.00 mVrms

X: 720 Hz
Y: 4.822 mVrms

316.2
uVrms

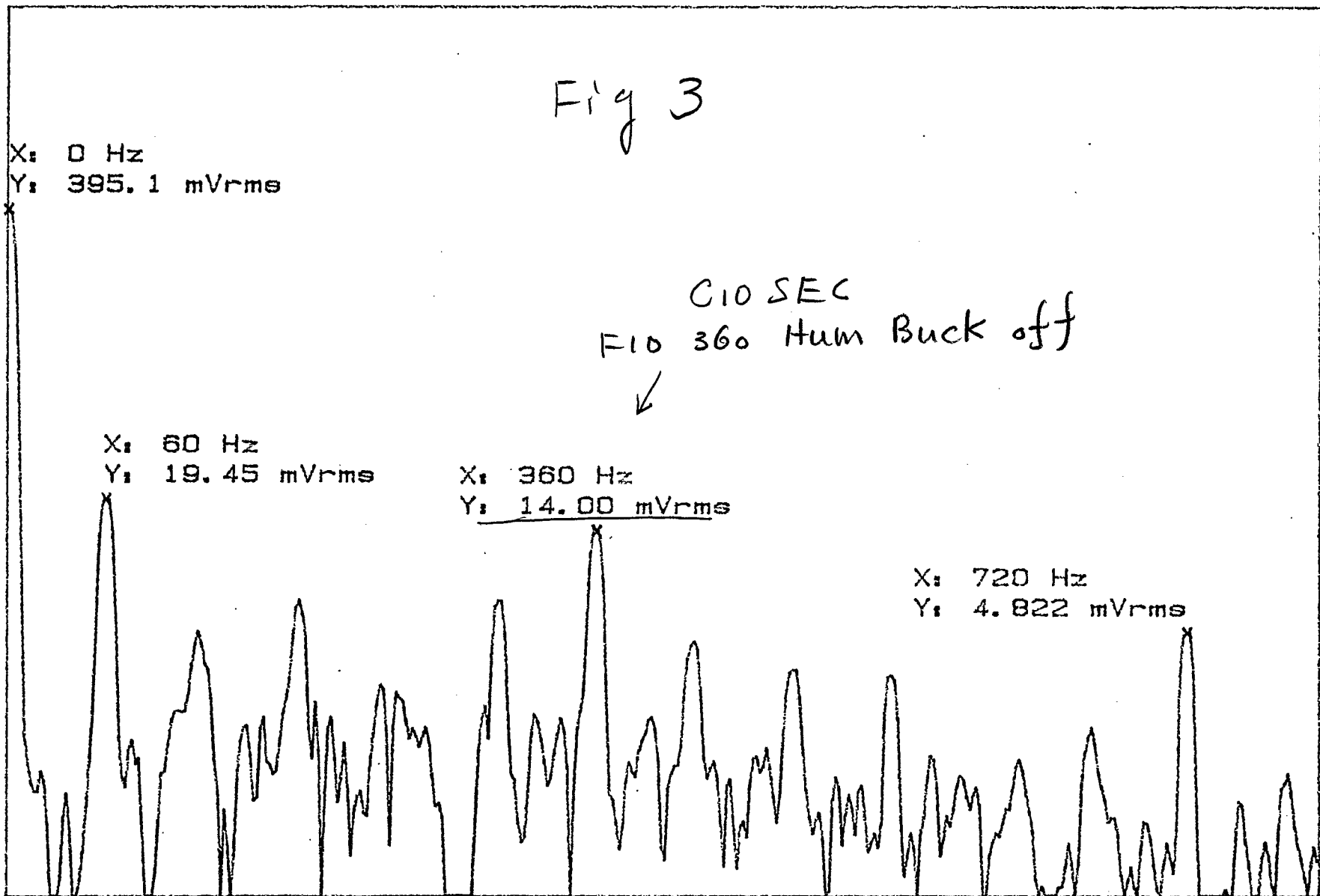
START: 0 Hz

BW: 7.6388 Hz

STOP: 800 Hz

X: 360 Hz

Y: 14.00 mVrms



RANGE: 10 dBV

STATUS: PAUSED

A: MAG

TIME: 50

3.162
Vrms

Fig 4

C10 SEC

F10 360 Hum Bucking on

10
dB
/DIV

X: 60 Hz
Y: 22.82 mVrms

X: 300 Hz
Y: 12.34 mVrms

X: 178 Hz
Y: 5.556 mVrms

X: 362 Hz
Y: 7.051 mVrms

X: 720 Hz
Y: 8.251 mVrms

316.2
uVrms

START: 0 Hz

BW: 7.6388 Hz

STOP: 800 Hz

X: 0 Hz

Y: 401.3 mVrms

