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Radial-offset Optics in EIC Hadron Lattices. Trajectory Lengthening

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² Abstract

This Tech. Note describes a method for a radial orbit offset in the arcs of the EIC hadron lattices, based on the perturbation dB/B of the magnetic field of the arc main bend magnets. This can be done independently for each arc (allowing multiple rigidities) and requires the use of pairs of orbit correctors at the extremities of the arc to ensure that the radially shifted orbit is on the *zero-orbit* (*i.e.* with the horizontal coordinates x = 0, $p_x = 0$) at the exit and entry point of the respectively upstream and downstream interaction region (IR). The goal is to produce appropriate orbit lengthening as required for time of flight adjustments between the electron and hadron beams as part of EIC operations. An *ad hoc* parameter is introduced: a "geometric compaction factor" $\alpha_B = (dC/C)/(dB/B)$, to quantify the orbit lengthening, or equivalently the radial orbit shift $dR = R \cdot \alpha_B \cdot dB/B$, from bending perturbation. Detailed numerical results are produced and discussed.

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1 INTRODUCTION

21 **1** Introduction

The EIC electron-hadron collider project, currently in its conceptual design stage, calls for repurposing parts of the existing RHIC to serve as the EIC hadron lattices in order to transport hadron bunches towards the collision point IP6 with electron bunches inside of IR6 where the STAR detector is located. The EIC is being designed for a wide range of center of mass energies, with $\sqrt{s_{e-h}} = 29-140$ GeV, with Tab. 1 listing all design beam energies for hadron species being considered.

Table 1: Design beam energies for the species planned for EIC operations at $\sqrt{s_{e-h}} = 29-140$ GeV.

Species	Polarized electrons	Polarized protons	Heavy ions Au
Energy [GeV, GeV/u]	5, 10, 18	41, 100, 275	41, 100

Electron-ion collision at IP6 requires the revolution frequency of the hadron bunches to match that of the electron bunches; from a practical standpoint, and given the energies listed in Tab. 1, it will not be possible to have bunches circulating through the magnetic center of the arc magnets for all modes of operation if the revolution frequency is to be matched across all cases. This change of circumference has to take place in the arcs of the EIC hadron lattices in order to preserve the integrity of each IR by keeping the circulating beam on the magnetic center of all dipole and quadrupole magnets that constitute the IR layout.

Since modifying the circumference of a hadron ring using only the arcs is equivalent to changing the radius of the dipole magnets in these arcs, there are two ways that one can apply this change:

• design the hadron lattices as if the circulating beam is off-momentum: this would take care of the circumference change since the shifted orbit would be proportional to the dispersion function, however it does not address the need to maintain a zero-orbit (for which x = 0, $p_x = 0$) in the IRs, and furthermore any $\delta p/p \neq 0$ creates discrepancies with the rest of the EIC machine design;

• apply a small relative deviation dB/B to all dipole magnets of a given arc (most direct way to change the bending radius of a given section of the machine) and use pairs of horizontal orbit correctors at each end of the considered arc to set the circulating beam back on the zero-orbit going out of and into the neighboring IRs.

The second method is the one being studied in this document, with the goal to generate hadron lattices for a number of different values of dB/B in order to establish the correlation between this variable and the resulting relative change in lattice circumference dC/C.

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The established codes MAD-X and zgoubi are used to set up the radial-shift lattices:

- using two codes is just for convenience, mostly because one of the authors is a MAD-X user,
- the complete study discussed here may anyway be achieved with whatever code can handle orbit offset;

- on the other hand the EIC hadron ring is translated to zgoubi from its original MAD-X files, thus any ancillary

⁵⁰ work (as re-tuning the IRs in the present case, see below) can readily be performed using these existing MAD-X files;

- a third, obvious advantage of this opportunity to use two codes concurrently, is in its allowing tight cross-checks.

- ⁵² Using the two codes, the procedure is as follows:
- 1. with the MAD-X sequence file for the design (on-momentum, zero-orbit) lattice, generate a Twiss file of the
 entire ring, as a reference;
- using this sequence file and the Twiss file as input for zgoubi, generate a zgoubi Twiss file for consistency check
 on the main linear optics parameters (circumference, tunes, chromaticities, optical functions);
- 57 3. isolate each arc and apply a value of dB/B, taken in the following as [-0.01, -0.005, 0, 0.005, 0.01];

2 LATTICE VERSION V200512_MOD OF 08/10/2020

- 4. calculate the required strengths of the horizontal orbit correctors selected to put the circulating beam back on the zero-orbit at the edges of the arc being modified (see Tab. 2 for the full list of utilized correctors);
- 5. recalculate the periodic solution of the linear optics functions along with the shifted orbit (zero at both ends);

6. with the new boundary conditions ($\beta_{x,y}$, $\alpha_{x,y}$, D_x) set by these periodic solutions, rematch the linear optics of 62 each IR - this is readily done in MAD-X;

7. in order to keep the tunes constant, calculate the total changes in phase advances in the arcs due to the shifted
 orbit (using the initial Twiss files from the design lattice), and adjust the phase advances in each IR accordingly;

- 8. translate the rematched IRs, with updated quadrupole strengths, to zgoubi and produce the periodic solutions of
 the shifted orbit (radially offset in the arcs, zero in the IRs, as a consequence of the previous steps) and linear
 optics functions, together with tunes, chromaticities and other paraxial parameters.
- 9. a small rematch of the ring, for exact tune and chromaticity values, may be needed. It will be shown that this can be performed with just two families of lenses (main QF and QD quadrupoles for tunes, main SF and SD sextupoles for chromaticities), with moreover very small tweak of their strengths, in the $10^{-2} - 10^{-3}$ range, relative. Note that in the present study, this global ring re-match leaves the quadrupoles and sextupoles of the
- ⁷² IRs untouched, which may introduce a modulation of the resulting optical functions including the dispersion -
- and subsequently the orbit offset in the arcs. This can be refined, if needed, as part of an iteration of the process.
- 74 Once all these steps are completed, one can calculate such quantities as
- the resulting relative change in lattice circumference dC/C under the effect of a dB/B perturbation of the main magnet field in one or more arcs,
- a "geometric compaction factor" $\alpha_B = (d\mathcal{C}/\mathcal{C})/(dB/B)$ so the radial offset then writes $dR/(dB/B) = R \cdot \alpha_B$.

In addition, a new MAD-X sequence file can be generated that would include the value of dB/B in the form of a specific syntax when defining the SBEND arc dipoles, along with the corresponding strengths of orbit correctors as calculated by zgoubi to obtain a closed, shifted orbit. This MAD-X sequence file could then be used in Y. Luo's SimTrack for dynamic aperture tracking.

83 2 Lattice Version V200512_Mod of 08/10/2020

This is the lattice used in this study. Its origin is the hadron lattice V200512 taken from the "EIC HCR Task Force" sharepoint, set to proper tunes and chromaticities, namely $Q_x = 28.228$, $Q_y = 29.21$ and $\xi_x = \xi_y = 1$.

Working hypotheses

All ak11 (quadrupole component) and ak21 (sextupole) in BEND are removed, because they cause orbit. That jeopardizes both the tunes and the chromaticities. QF* and QD* are then tweaked to get back to QX=28.228 and Qy=29.21: this is a minor scaling, about 1.5e-3 relative, see page 4. SF* and SD* are tweaked to recover chromaticities close to 1, this is a small scaling factor, see page 4.

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• SCALING factor settings to meet nominal tunes and chromaticities (an excerpt from the input data file):

• Twiss file header:

0	TENCEU	2022 064014			
G	LENGIH	3833.864914			
0	ALFA	0.1873813140E-02			
0	ORBIT5	-0			
0	GAMMATR	23.10132340			
0	Q1	0.2279989283	[f	ractional]	
0	Q2	0.2099931863	[f	ractional]	
0	DQ1	1.121545684			
0	DQ2	0.9511037990			
0	DXMAX	2.08901372E+00	Q	DXMIN	-5.65589170E-01
0	DYMAX	0.0000000E+00	0	DYMIN	0.0000000E+00
0	XCOMAX	2.48096733E-04	Q	XCOMIN	-2.22126673E-04
0	YCOMAX	0.0000000E+00	0	YCOMIN	0.0000000E+00
0	BETXMAX	1.20917125E+03	0	BETXMIN	2.11749487E-01
0	BETYMAX	1.26772319E+03	Q	BETYMIN	1.06715632E-01
Ø	XCORMS	3.55396598E-01			



⁹⁶ **3** Method for an Orbit Offset $\propto \eta_x$ in the Arcs

⁹⁷ The orbit offset is made to scale the dispersion function.

• This is a simple way to get $\Delta R/R / \Delta B/B$ close to $\Delta R/R / \Delta p/p$.

• A double pair of steerers, located at the both ends of the arc, are used to force the orbit bump (which is excited along the arc, due to $\Delta B/B$) to follow the chromatic orbit.

• In this method, the arcs are treated independently, one by one, each as a periodic structure.

102 103

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94 95 MULTIPOL QF* 0.99841335 MULTIPOL QD* 1.0014330 MULTIPOL SF* 1.005000000E+00 MULTIPOL SD*

1.025000000E+00 MULTIPOL MULT -2.00000000E-01

Strategy for geometric orbit to follow the chromatic orbit:

- Hill's equation for magnetic defect $\Delta B(s) = \Delta B_y$, or for momentum offset $\delta p/p$, have the same form, respectively: tively:

$$x'' + Kx = -\frac{\Delta B_y}{B\rho}$$
 and $x'' + Kx = \frac{1}{\rho}\frac{\Delta p}{p}$ (1)

- thus, the geometric orbit $x_{co}(s)$ will follow $-\eta_x$ along the arc if its coordinates at the origin of the arc (say, s=0) satisfy

$$x_{co}(s=0) = -\eta_x \frac{\Delta B}{B}$$
 and $x'_{co}(s=0) = -\eta'_x \frac{\Delta B}{B}$ (2)

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The latter are the two constraints applied at the downstream steerer of the upper pair (next to the upstream IR), with both these upstream steerers as variables in the matching procedure. Zero orbit and angle are the constraints applied at the downstream steerer of the downstream pair (just before the downstream IR), with both these downstream steerers as variables. 113

By analogy with the momentum compaction factor $\alpha_p = dC/C/dp/p$ to quantify the trajectory lengthening due to momentum offset, we introduce here a "geometric compaction" factor α_B to quantify the trajectory lengthening due to geometric (ΔB induced) orbit offset.

$$\alpha_B = d\mathcal{C}/\mathcal{C}/dB/B$$

4 Orbit Offset in the Arcs; Optical Functions

• Table 2 displays the strengths of the orbit offset steerers, for the four values $dB/B = \pm 0.05$ and ± 0.01 . It can be seen that the steerers response to dB/B is close to linear.

Table 2: Strengths of the orbit offset steerers (in units of 10^{-7} rad), for the four values $dB/B = \pm 0.05$ and ± 0.01 .

	Steerer		ue	D/D	
Arc	name	-0.01	-0.005	+0.005	+0.01
5-4	BI5_TH11	-366.12237	-181.23473	177.58894	351.61844
	BI5_TH13	3372.6357	1762.8166	-1913.8606	-3977.4355
	BI4_TH13	3753.3446	1857.6984	-1840.8107	-3747.1045
	BI4_TH11	-421.07912	-219.78372	333.82121	869.69872
3-2	BO3_TH10	-597.03541	-301.57065	307.70386	621.64203
	BO3_TH12	3715.0344	1853.0320	-1844.2605	-3679.4619
	BO2_TH12	3283.7361	1724.3471	-1911.7728	-3960.2274
	BO2_TH10	-192.04674	-171.75164	227.22489	418.70345
1-12	YO1_TH10	-474.49310	-235.62872	232.33654	461.53095
	YO1_TH12	3364.4473	1759.1452	-1911.7317	-3973.9201
	YO12_TH12	3443.0085	1790.1885	-1845.2136	-3689.3433
	YO12_TH10	-675.48512	-326.73983	313.25103	666.51374
11-1	BO11_TH10	-585.02791	-295.54350	301.58831	609.34504
	BO11_TH12	3667.5721	1829.6686	-1821.0114	-3633.3650
	BO10_TH12	3322.0473	1747.0506	-1932.9582	-3992.5256
	BO10_TH10	-233.14673	-184.67045	224.34123	399.27264
9-8	BI9_TH11	-393.62525	-194.96887	191.30175	379.01094
	BI9_TH13	3375.2837	1765.2944	-1918.7588	-3989.5041
	BI8_TH13	3764.6706	1866.5856	-1854.5600	-3777.1755
	BI8_TH11	-445.60501	-230.70777	340.20023	875.87467
7-6	YI7_TH11	-532.34972	-268.97830	274.60244	554.97529
	YI7_TH13	3684.7731	1838.4168	-1830.7798	-3653.4931
	YI6_TH13	3489.2447	1814.6292	-1854.8456	-3663.3062
	YI6_TH11	-435.94046	-202.53789	161.67522	331.84953
	Arc 5-4 3-2 1-12 11-1 9-8 7-6	Arc name Arc name 5-4 BI5.TH11 BI5.TH13 BI4.TH13 BI4.TH13 BI4.TH13 BI4.TH13 BI4.TH13 BO2.TH10 BO3.TH12 BO2.TH10 BO2.TH10 1-12 YO1.TH12 YO12.TH12 YO12.TH10 11-1 BO11.TH12 BO10.TH12 BO10.TH10 9-8 BI9.TH11 BI9.TH13 BI8.TH13 BI8.TH13 BI8.TH13 YI7.TH11 YI7.TH13 YI6.TH13 YI6.TH11	Arc name -0.01 5-4 BI5.TH11 -366.12237 BI5.TH13 3372.6357 BI4.TH13 3753.3446 BI4.TH13 3753.3446 BI4.TH11 -421.07912 3-2 BO3.TH12 3715.0344 BO2_TH12 3283.7361 BO2_TH10 -192.04674 1-12 YO1.TH10 -474.49310 YO1_TH12 3364.4473 YO12_TH12 3443.0085 YO12_TH12 3443.0085 YO12_TH12 3443.0085 YO12_TH12 3667.5721 BO11_TH12 3364.4473 BO10_TH12 3322.0473 BO10_TH12 3322.0473 BO10_TH10 -233.14673 9-8 BI9_TH11 -393.62525 BI9_TH13 3375.2837 BI8_TH13 3764.6706 BI8_TH13 3764.6706 BI8_TH13 3684.7731 YI6_TH13 3489.2447 YI6_TH13 3489.2447	Arc name -0.01 -0.005 5-4 BI5_TH11 -366.12237 -181.23473 BI5_TH13 3372.6357 1762.8166 BI4_TH13 3753.3446 1857.6984 BI4_TH11 -421.07912 -219.78372 3-2 BO3_TH10 -597.03541 -301.57065 BO2_TH10 -192.04674 -171.75164 1-12 YO1_TH10 -474.49310 -235.62872 YO1_TH12 3364.4473 1759.1452 YO12_TH12 3443.0085 1790.1885 YO12_TH10 -675.48512 -326.73983 11-1 BO11_TH10 -585.02791 -295.54350 BO11_TH12 3322.0473 1747.0506 BO10_TH10 -233.14673 -184.67045 9-8 BI9_TH11 -393.62525 -194.96887 BI9_TH13 3375.2837 1765.2944 BI8_TH13 3764.6706 1866.5856 BI8_TH11 -445.60501 -230.70777 7-6 YI7_TH13 3684.7731 1838.4168	Arc name -0.01 -0.005 +0.005 5-4 BI5_TH11 -366.12237 -181.23473 177.58894 BI5_TH13 3372.6357 1762.8166 -1913.8606 BI4_TH13 3753.3446 1857.6984 -1840.8107 BI4_TH11 -421.07912 -219.78372 333.82121 3-2 BO3.TH10 -597.03541 -301.57065 307.70386 BO2_TH12 3715.0344 1853.0320 -1844.2605 BO2_TH10 -192.04674 -171.75164 227.22489 1-12 YO1_TH10 -474.49310 -235.62872 232.33654 YO1_TH12 3364.4473 1759.1452 -1911.7317 YO12_TH12 3443.0085 1790.1885 -1845.2136 YO12_TH10 -675.48512 -326.73983 313.25103 11-1 BO11_TH10 -585.02791 -295.54350 301.58831 BO11_TH12 3322.0473 1747.0506 -1932.9582 BO10_TH10 -233.14673 -184.67045 224.34123 9-8

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• The graphs in pp. 6, 7 show the orbit offset in the arcs (treated each one as a separate, periodic structure), for the four values $dB/B = \pm 0.05$ and ± 0.01 . It can be seen that the orbit excursion reacts essentially linearly to dB/B. The exact values of orbit excursion extrema are given in pp. 8 and 9 under the "Twiss output file header".

Once the arcs are individually set (closed orbit bump and periodic optics, for each arc concerned), the IRs are re-tuned to match them, and the 12 segments so obtained (6 arcs and 6 IRs, in the present case where orbit has been offset in all 6 arcs) are re-assembled:

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• The graphs and tables in pp. 8, 9 show the global, periodic ring optics parameters, closed orbits, and optical functions, in the presence of orbit steerer settings (Tab. 2) yielding the arc orbit offsets of pp. 6, 7. One can observe some modulation of the dispersion function extrema, greater for greater dB/B, and, by correlation (Eq. 2), of the orbit offset extrema. The probable cause has been discussed in item 9 page 3. This is however a minor effect and can be taken care of with an iteration of the process.



150 s [m]

s [m]

200

s [m]

150 s [m]

150 s [m]

from zgoubi.TWISS.out

from zgoubi







dB/B = -0.01



6



dB/B = +0.005

dB/B = +0.01

dB/B = -0.01

RING, PERIODIC: ORBIT OFFSET AND OPTICAL FUNCTIONS





• SCALING settings to meet nominal tunes and chromaticities

Input data file excerpt, shows that adjustment of the main quads (QF and QD) within a few permil is required to reset tunes to 28.228/29.21, adjustment of the sextupoles (SF, SD) within a few percent to reset chromaticities to 1/1

-1 -1 0.99700601 0.9901268 1 1 MULTIPOL QD* -1 -1 1.0001647 1 1.0001647 1 1 MULTIPOL SF* -1 -1 0.9960790 1 0.96960790 1 1 MULTIPOL SD* -1 -1 1.1139358 1 1.1139358	MULTIPOL QF*	MULTIPOL QF*
0.99700601 0.99901268 1 1 MULTIPOL QD* -1 -1 1.0001647 1 1 MULTIPOL SF* 1 -1 .0990000E+00 1 0.99001268 .0021175 1.0001647 1 1 MULTIPOL SF* -1 -1 .9300000E+00 0.96960790 1 1 MULTIPOL SD* -1 -1 .0600000E+00 1.1139358 1 1	-1	-1
1 1 MULTIPOL QD* -1 -1 -1 1.0021175 1.0001647 1 1 MULTIPOL SF* -1 -1 .930000E+00 0.96960790 1 1 MULTIPOL SD* -1 -1 1.001140 1 .1001170 1 .1001170 1 .1001170 1 .1001170 1 .11139358 1 .11139358	0.99700601	0.99901268
MULTIPOL QD* MULTIPOL QD* -1 -1 1.0021175 1.0001647 1 1 MULTIPOL SF* -1 -1 0.96960790 1 1 MULTIPOL SD* -1 -1 1 1 1 MULTIPOL SD* -1 -1 1 MULTIPOL SD* -1 -1 1 1.0600000E+00 1 1 1.1139358 1 1	1	1
-1 -1 1.0021175 1.0001647 1 1 MULTIPOL SF* -1 -1 0.96960790 1 1 MULTIPOL SD* 1 -1 1.0600000E+00 1.0600000E+00 1.1139358 1 1	MULTIPOL QD*	MULTIPOL QD*
1.0021175 1.0001647 1 1 MULTIPOL SF* MULTIPOL SF* -1 -1 .930000E+00 1 MULTIPOL SD* -1 -1 1.0600000E+00 1 MULTIPOL SD* -1 1.1139358 1 1	-1	-1
1 1 MULTIPOL SF* -1 .9300000E+00 0.96960790 1 1 MULTIPOL SD* -1 -1 1 1.0600000E+00 1.1139358 1 1	1.0021175	1.0001647
MULTIPOL SF* MULTIPOL SF* -1 -1 .9300000E+00 0.96960790 1 1 MULTIPOL SD* -1 -1 1 1.0600000E+00 1.1139358 1 1	1	1
-1 -1 .9300000±+00 0.9690790 1 1 MULTIPOL SD* -1 -1 1.06000000±+00 1 1.1139358 1 1	MULTIPOL SF*	MULTIPOL SF*
.9300000E+00 0.96960790 1 1 MULTIPOL SD* -1 1.06000000E+00 1.1139358 1 1	-1	-1
1 1 MULTIPOL SD* -1 -1 -1 1.06000000E+00 1.1139358 1 1	.930000E+00	0.96960790
MULTIPOL SD* MULTIPOL SD* -1 -1 1.0600000E+00 1.1139358 1 1	1	1
-1 -1 1.0600000E+00 1.1139358 1 1	MULTIPOL SD*	MULTIPOL SD*
1.06000000E+00 1.1139358 1 1	-1	-1
1 1	1.0600000E+00	1.1139358
	1	1



dB/B = +0.005

dB/B = +0.01

• SCALING settings to meet nominal tunes and chromaticities

Input data file excerpt, shows that adjustment of the main quads (QF and QD) within a few permil is required to reset tunes to 28.228/29.21, adjustment of the sextupoles (SF, SD) within a few percent to reset chromaticities to 1/1

MULTIPOL QF*	MULTIPOL QF*
-1	-1
0.99620822	0.99837974
1	1
MULTIPOL QD*	MULTIPOL QD*
-1	-1
1.0014792	1.0012825
1	1
MULTIPOL SF*	MULTIPOL SF*
-1	-1
0.88229274	0.99723158
1	1
MULTIPOL SD*	MULTIPOL SD*
-1	-1
1.0165657	1.0290099
1	1

5 TRAJECTORY LENGTHENING

133 5 Trajectory Lengthening

Trajectory lengthening in the arcs, under the effect of orbit offset, for the four values $dB/B = \pm 0.05$ and ± 0.01 , is displayed in Tab. 3, together with (i) the geometric compaction $\alpha_B = \frac{dC/C}{dB/B}$, (ii) the average radial offset dR/dB/B =R × $\alpha_B = 610.17 \times \alpha_B$.

			d	B/B	
Arc		-0.01	-0.005	+0.005	+0.01
5-4	(mm)	8.438	4.314	-4.351	-8.938
3-2	(mm)	9.409	4.812	-4.821	-9.856
1-12	(mm)	9.498	4.831	-4.823	-9.867
11-1	(mm)	9.417	4.814	-4.819	-9.851
9-8	(mm)	8.443	4.316	-4.352	-8.937
7-6	(mm)	8.458	4.320	-4.350	-8.953
all arcs	(mm)	53.663	27.409	-27.520	-56.405
EIC Hadro	on ring (C	= 3833.8	865 m, R=	610.17 m):	
$\alpha_{\rm B}$	(10^{-3})	-1.40	-1.430	-1.4356	-1.4712
dR/dB/B	(m)	-0.854	-0.872	-0.876	-0.898

Table 3: This table displays, as a function of dB/B: (i) trajectory lengthening in individual arcs (rows 3 to 8), (ii) summed up over all 6 arcs (row 9), (iii) geometric compaction α_B over the ring (row 11), (iv) radial offset (row 12).

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Table 4 shows the orbit length around the ring in the presence of orbit offset in the arcs (i.e., the length of the periodic orbits displayed in pp. 8, 9). This is a kind of "double check": the resulting trajectory lengthening (bottom line in Tab. 4) is expected to coincide the values in the "all arcs" row in Tab. 3 (the agreement is within $1\sim 2\%$).

Table 4: Orbit length in the complete ring, from a "Twiss" computation (which yielded the graphs in pp. 8, 9), and difference with respect to the unperturbed optics. The table also summarizes the extreme orbit excursion in presence of the orbit offset ("XCOMAX" or "XCOMIN" values taken from the "Twiss file header", pp. 8, 9).

				dB/B		
		-0.01	-0.005	0	+0.005	+0.01
extreme orbit excursion	(mm)	18.336	9.249	0	-9.404	-19.329
orbit length \mathcal{C}	(m)	3833.91808	3833.89191	3833.86491	3833.83695	3833.80816
orbit lengthening $\mathcal{C} - \mathcal{C}_{\mathrm{unperturbed}}$	(mm)	+53.17	+27	0	-27.958	-56.745

141 Greater Azimuthal Orbit Offset Extent

By comparison with $|\alpha_B|$ values in Tab. 3, the momentum compaction is substantially greater (see p. 4, "Twiss file header"), $\alpha_p = 1.8738 \times 10^{-3}$. The bulk of the difference between both comes from the geometric orbit offset being zero in the IRs, whereas the chromatic orbit is not.

Namely, if the orbit offset is extended beyond the corrector pairs presently assumed (Tab. 2), into the IRs, and assuming the same extreme excursions along the arcs (pp. 6, 7), then

$$\alpha_B \to -\alpha_p$$

Referring to the α_p values of the present $-0.01 \le dB/B \le +0.01$ designs (assuming similar values upon extended orbit offset, pp. 8, 9), this gives the following majoring dC values (which cannot be reached, as in this limit the orbit offset extends over the IR):

			dE	B/B	
		-0.01	-0.005	+0.005	+0.01
Extreme orbit excursion in arcs	(mm)	+18.3	+9.2	-9.4	-19.3
$\alpha_{\mathbf{B}} \to -\alpha_{\mathbf{p}}$	(10^{-3})	-1.80	-1.84	-1.91	-1.95
dR/dB/B	(m)	-1.1	-1.12	-1.17	-1.19
Majoring $d\mathcal{C}$ values	(mm)	+69	+35	-37	-71

149 6 Short-Term DA

Short-term DA estimates have been performed using the rings of pp. 8, 9. They may be used for consistency checks
 against SimTrack.

• For the 5 cases of concern here, $dB/B = 0, \pm 0.005, \pm 0.01,$

- DAs are computed for 1000 turns, for sample dp/p taken over the maximum stable dp/p range (max. |dp/p| values explored in the figures below are at $\leq 0.5 \times 10^{-3}$ from stability limit),

- accuracy on x and y boundaries is 0.1 mm.



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dB/B = -0.01dB/B = -0.0051000-turn DA within max dp/p stable range, dB/B=-0.01 1000-turn DA within max dp/p stable range. dB/B=-0.005 20 5e-3 3e-3 1e-3 20 5e-3 3e-3 1e-3 -1e-3 -3e-3 4 5e-3 -1e-3 -3e-3 15 15 y (mm) y (mm) 10 10 -5 x (mm) dB/B = 01000-turn DA, no orbit offset 25 =5e-3 4e-3 3e-3 2e-3 1e-3 -1e-3 -2e-3 -2e-3 -2e-3 -3e-3 -2e-3 -5e-3 -55e-3 20 15 (mm) / 10 0 (mm) dB/B = +0.005dB/B = +0.011000-turn DA within max dp/p stable range. dB/B=+0.005 1000-turn DA within max dp/p stable range. dB/B=+0.01 20 20 =40-3 3e-3 2e-3 1e-3 0e-3 -1e-3 -2e-3 -3e-3 -4e-3 3e-3 2e-3 1e-3 0e-3 -1e-3 -2e-3 -3e-3 -4e-3 15 15 y (mm) y (mm) 10 10 25

7 CONCLUSION

7 Conclusion

In conclusion, the following table recapitulates the extreme orbit excursion, trajectory lengthening, geometric compaction α_B , and radial shift dR/dB/B values, in the hypothesis of the $\Delta x_{\text{offset}} \propto \eta_x$ method described in Sec. 3, and in the case of identical $\Delta B/B$ in all 6 arcs:

			dE	5/B	
		-0.01	-0.005	+0.005	+0.01
Extreme orbit excursion	(mm)	+18.336	+9.249	-9.404	-19.329
Orbit lengthening	(mm)	+53.17	+27	-27.958	-56.745
$\alpha_{\mathbf{B}} = \frac{\mathbf{d}\mathcal{C}/\mathcal{C}}{\mathbf{d}\mathbf{B}/\mathbf{B}}$	(10^{-3})	-1.40	-1.430	-1.4356	-1.4712
$rac{\mathrm{d}\hat{\mathrm{R}}}{\mathrm{d}\mathrm{B}/\mathrm{B}}$	(m)	-0.854	-0.872	-0.876	-0.898

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The trajectory lengthening so obtained assume an azimuthal extent of the orbit offsets of about 250 m meters, between dedicated corrector pairs. A greater extent, toward the IRs, assuming the same extreme excursions in the arcs, would result in greater trajectory lengthening.

170 Arbitrary Radial Offset

As pointed out in the foregoing, the radial offset does not have to be applied to all 6 EIC hadron ring arcs, and does 171 not have to be the same in all arcs concerned. This is apparent in the EIC ring input data file given in Appendix. The 172 interest is in the possibility of simulating cases where greater (or smaller) aperture would be available in some arcs, 173 compared to others. This obviously would assume that independent dB/B perturbation in the arcs of the EIC hadron 174 ring is available. To that end, a decision must be made as to the implementation of this perturbation: the "simplest" 175 solution would be to use a single shunt supply on the main bus line powering all arc dipoles, and control the amplitude 176 of dB/B via the current of that shunt. If the need arises for individual control of each arc of the EIC hadron lattices, 177 then there would need to be one shunt supply per determined value of dB/B for each requested radial offset. 178 179

180 Simulation I/O Files

All the input files used for the simulations discussed here, as well as the output files so produced, can be found at the #EIC Task Force" sharepoint:

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184 https://brookhavenlab.sharepoint.com/sites/EIC-Radial-Shift/Shared%20Documents/Forms/

Appendix 185

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Multiple Different Rigidities 186

In the input data file below (which performs a "TWISS" computation), 'SCALING' is a power supply command rack. 187 It sets bending magnets, quadrupoles and sextupoles, and orbit offset steerers to proper field values. The 6 arcs and 6 188 IRs are in separate files, subject to 'INCLUDE' (the equivalent of a "call" in MAD, with some additional subtleties). 189 In this example a case of three different rigidities is shown: 190

- the reference rigidity is 1 (dB/B=0) in all IRs, resulting in no orbit offset,

- it is perturbed by dB/B=0.005 in arcs 5-4, 3-2, 11-10, 9-8, 7-6, resulting in the orbit offsets displayed in p. 7 192

- it is perturbed by 0.0025 instead in arc 1-12, and there only, resulting by linearity in about half the orbit offset 193 displayed under "arc 1 - arc 12" in p. 7. 194

Moving 'SCALING' around as illustrated here, allows arbitrary change of the reference rigidity in any arc. 195

MULTIPOL BO2 TH12 ! close orbit OBJET MULTIPOL YI6 TH111 ! close orbit 1000.000000 -1911.7728 161.67522 .001 .001 .001 .001 0. .0001 MULTIPOL BO2_TH10 ! close orbit 0. 0. 0. 0. 0. 1. 'INCLUDE' 227.22489 'SCALING' ../arc5-arc4.TWIS56.inc[#S_arc5-arc4:#E_arc5-arc4] INCLUDE 33 MULTIPOL YO1 TH10 ! close orbit ARC 1-12 BEND ../madIRs_fromGRD/ir4.inc[#S_ir4:#E_ir4] 116. 1.005 'INCLUDE' 1 MULTIPOL YO1 TH12 ! close orbit ../arc3-arc2.TWISS.inc[#S_arc3-arc2:#E_arc3-arc2] 'INCLUDE' BEND IR* -960. 1. ./madIRs_fromGRD/ir2.inc[#S_ir2:#E_ir2] MULTIPOL YO12 TH12 ! close orbit MULTIPOL SCALING' 33 -923. 1. BEND MULTIPOL Y012_TH10 ! close orbit 1.0025 MULTIPOL IR* 155. 'INCLUDE' 1. MULTIPOL BO11_TH10 ! close orbit ARC 11-10 ./arc1-arc12.TWISS.inc[#S arc1-arc12:#E arc1-arc12] MULTIPOL OF* 'SCALING' 301.58831 0.99700601 1 33 BEND MULTIPOL BO11_TH12 ! close orbit MULTIPOL OD* 1.0025 -1821.0114 1.0021175 BEND IR* MULTIPOL BO10 TH12 ! close orbit MULTIPOL SF* 1. -1932 9582 .9300000E+00 'INCLUDE' MULTIPOL BO10_TH10 ! close orbit MULTIPOL SD* 1 ./madIRs_fromGRD/ir12.inc[#S_ir12:#E_ir12] 224.34123 1.0600000E+00 'INCLUDE' 1 MULTIPOL BI9 TH11 ! close orbit ARC 9-8 MULTIPOL MULT ./arc11-arc10.TWISS.inc[#S_arc11-arc10:#E_arc11-arc10] ../arcii-'INCLUDE' 191.30175 -2.00000000E-01 1 ./madIRs_fromGRD/ir10.inc[#S_ir10:#E_ir10] MULTIPOL BI9_TH13 ! close orbit 'INCLUDE' MULTIPOL BI5 TH11 ! close orbit ARC 5-4 1 -1918.7588 177.58894 ./arc9-arc8.TWISS.inc[#S_arc9-arc8:#E_arc9-arc8] 'INCLUDE' MULTIPOL BI8 TH13 ! close orbit MULTIPOL BI5_TH13 ! close orbit 1 ../madIRs_fromGRD/ir8.inc[#S_ir8:#E_ir8] -1854.5600 'INCLUDE' -1913.8606 1 MULTIPOL BI8_TH11 ! close orbit MULTIPOL BI4 TH13 ! close orbit ../arc7-arc6.TWISS.inc[#S_arc7-arc6:#E_arc7-arc6] 'INCLUDE' 340.20023 -1840.8107 1 ../madIRs_fromGRD/ir6.inc[#S_ir6:#E ir6] MULTIPOL YI7 TH11 ! close orbit ARC 7-6 MULTIPOL BI4_TH11 ! close orbit 'FIT' 274.60244 333.82121 1 30 0 [-1.,1.] MULTIPOL YI7 TH13 ! close orbit MULTIPOL BO3 TH10 ! close orbit ARC 3-2 1 31 0 [-10.,10.] 1e-8 -1830.7798 3.1 1 2 #End 0. 1. 0 307.70386 3.1 1 3 #End 0. 1. 0 MULTIPOL YI6_TH13 ! close orbit MULTIPOL BO3_TH12 ! close orbit TWISS' 2 1. 1. -1854.8456 -1844.2605 'END'

• Complete EIC Hadron Ring:

EIC Hadron Ring With 3 Different Rigities