

Ring-based electron cooler for EIC

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An Electron Ion Collider (EIC) at Brookhaven National Laboratory (BNL) is being proposed as a new discovery machine for the nuclear physics and quantum chromodynamics. The hadron beam cooling plays an important role in the EIC machine to achieve its physics goals. The most challenging is cooling of protons at the highest energy in the EIC. In this paper, we present a possible design of a ring-based electron cooler for the high energy hadron beam cooling. In proposed approach, the electrons will cool the hadrons while being cooled themselves by radiation damping in the storage ring. For design of the cooler using storage ring approach several aspects becomes very important, including electron ring optics design, chromaticity correction, calculate the dynamic aperture, radiation damping, quantum excitation, and intrabeam scattering (IBS). In addition, such effects as beam-beam scattering (BBS) due to interaction of electrons with hadrons become of special concern. In this paper, we discuss and take into design all the effects above, as well as introduce generalized treatment of the BBS and 3-D quantum lifetime. A special feature of our design is an effective use of dispersion in the cooling section, both for the ions and electrons, to redistribute the cooling rate between the longitudinal and horizontal planes. Finally, the cooling performance is simulated for proton beam at the top energy of the EIC. Our conclusion is that such ring-based cooler could be a feasible approach to provide required parameters of hadron beam at the top energy of 275 GeV for the EIC.

I. INTRODUCTION

Electron cooling is a powerful method to shrink the size and momentum spread of the stored ion beams for accumulation and high-precision experiments. Since it was first proposed by G. I. Budker in 1967 [1], this technique has been widely applied and developed in many heavy ion accelerators around the world [2–5]. With the development of particle accelerators and the higher requirements for experimental physics, beam cooling with much higher energy electron beam is demanded. In 2005, the first relativistic electron cooling was demonstrated at Fermilab [6]. Recently, the world’s first rf-based electron cooler was successfully commissioned at BNL and became the first electron cooler to directly cool colliding ion beams [7]. It provides the possibility to use similar approach to develop high-energy electron coolers in the future.

Brookhaven National Laboratory (BNL) is designing an Electron-Ion Collider (EIC), which will be a new discovery machine that opens new frontiers for the researches in nuclear physics and quantum chromodynamics [8]. In order to maintain the high luminosity during long collision runs, it is desirable to cool the hadron beam to counteract the emittance growth caused by intrabeam scattering (IBS). There are several new cooling concepts proposed for the EIC, such as coherent electron cooling [9] and micro-bunched electron cooling [10]. In addition to these new concepts, conventional electron cooling schemes, such as ERL-based electron cooler [11] and ring-based electron cooler using dc electron beam [12], are also under consideration. In this paper, we present a design of electron storage ring cooler with bunched electron beam for the EIC.

Electron cooling using a storage ring was considered before [13, 14]. In our design we employ bunched electron beams without continuous magnetic field in the cooling section, similar to [7], and make effective use of dispersive cooling by introducing dispersions for the ions and electrons in the cooling section.

The ring-based cooler approach is based on conventional electron cooling technique, but the electrons which continuously interact with the hadron beam are being cooled by radiation damping in the storage ring. For a good cooling performance, the electron beam with low-temperature and high-intensity is needed, which requires a strong damping effect in electron storage ring. Therefore, this concept strongly depends on electron ring design and is feasible only at high energies, at which the IBS heating is reduced while the radiation damping is enhanced. In the paper, we describe the ring optics design and achieved equilibrium parameters of electron beam due to the radiation damping, quantum excitation, IBS effect and Beam-Beam scattering (BBS). We also introduce a general treatment of the BBS and the 3-D quantum lifetime.

To calculate the cooling process, a cooling simulation code was developed, in which the 3-D non-magnetized cooling force, IBS and the dispersion effect on cooling are considered. It is also shown that the dispersions of hadron and

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electron beams can be effectively used to redistribute the horizontal and longitudinal cooling rates. Based on the simulation results, we conclude that such ring-based cooler with bunched electron beam could be a feasible approach to provide required parameters of proton beam at the top energy of 275 GeV for the EIC.

The paper is organized as follows. In Sec. II, the main beam parameters in EIC and the cooling requirement are introduced. In Sec. III, the lattice design of the ring cooler is presented. In Sec. IV, the electron beam parameters in the ring are calculated and some important properties of the cooler are described. Then the cooling simulation results on hadron beam are presented in Sec. V. Finally, a summary is given in Sec. VI.

II. COOLING REQUIREMENT

In the design of beam cooling for the EIC, the most demanding case is to cool protons with the energy of 275 GeV. During the long collision stores, the emittance growth of proton beam due to IBS is the dominant limitation for the luminosity. The requirement for the hadron beam cooling is mainly to counteract the IBS heating effect. Table I summarizes the proton beam parameters which are relevant for the calculation of IBS growth rates and are used to specify the required cooling rates. The evolution of the 275 GeV proton beam emittance caused by IBS is shown in Fig. 1. It shows that the IBS heating effect for the flattened proton beam is dominated by the horizontal and longitudinal planes. As a result, vertical cooling is not needed for these parameters. We should note that required small vertical emittance of protons, shown in Table I, is assumed to be available at the start of the store, for example by pre-cooling of protons at injection energy. Because vertical cooling is not required, one can effectively use horizontal dispersion to redistribute the cooling rates between the longitudinal and horizontal planes, and achieve required cooling performance.

TABLE I. Proton beam parameters for cooling

Proton beam energy [GeV]	275
Relativistic Factor γ	293.1
Number of protons per bunch	6.88×10^{10}
Number of bunches	1160
Average beam current [A]	1
RMS emittance (x/y) [nm]	9.6/1.5
RMS momentum spread	6.6×10^{-4}
RMS bunch length [cm]	6
Max. space charge	0.003
Transverse IBS growth time (H/V) [hours]	2.0/12
Longitudinal IBS growth time [hours]	3.4
Electron cooling beam energy [MeV]	149.8
Required cooling time [hours]	≤ 2

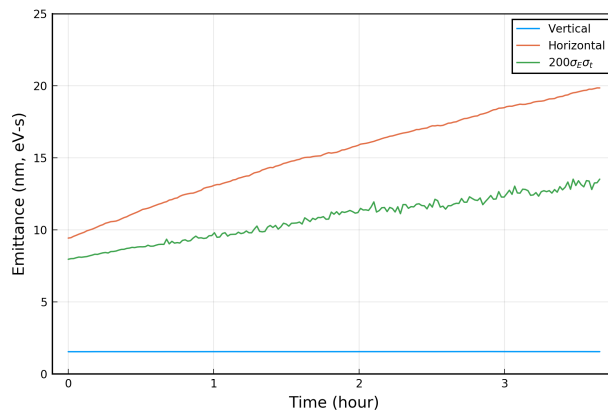


FIG. 1. Emittance growth of the 275 GeV proton beam caused by IBS.

III. ELECTRON RING LATTICE OVERVIEW

The electron storage ring has a race track shape, with the cooling section located in one long straight section and wigglers in the other. The ring is mirror symmetric around the center of the cooling section, and the top view of the ring is shown in Fig. 2. The cooling section has a length of 170 m and it fits into the straight section of the hadron ring. There are four arcs with radius of 3.42 m, each of them has 10 dipoles and a 90 degree phase advance per cell. The mid-arc adapter is quadrupole section to adjust the tunes of the machine. The wiggler section is also mirror symmetric with four pairs of wigglers in each half. In our setup, the alternating horizontal and vertical wigglers are used, and the wiggler poles are shaped as combined function sector dipoles. The mid-wiggler adapter connects the two parts and is also used to optimize the high order chromaticity. The optics of the ring cooler is shown in Fig. 3 [15].

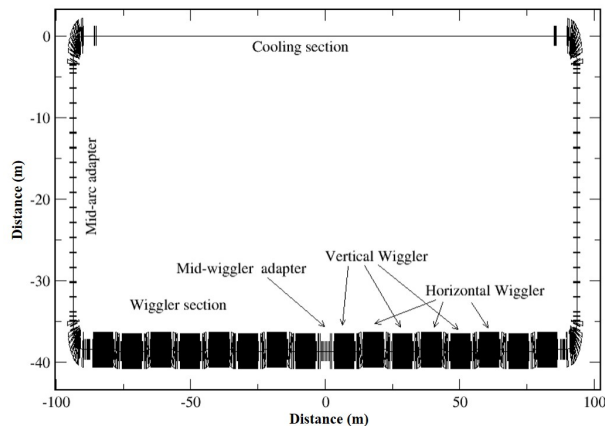


FIG. 2. Layout of the ring cooler.

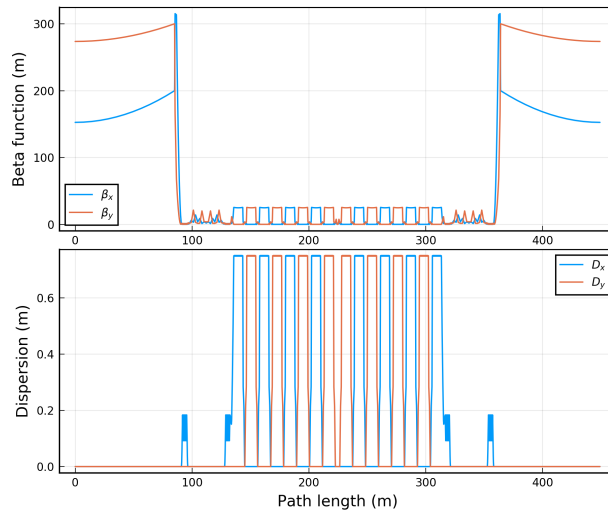


FIG. 3. Optics of the ring cooler.

Because of the edge focusing of the dipoles, the wigglers will create a large chromaticity. The contribution of the arcs are relatively small and there are only a few slots available to place sextupoles. Simultaneously, the dispersion in the arc has to be kept small to avoid transverse emittance growth from IBS. This would require strong sextupoles decreasing the dynamic aperture significantly. In order to reduce the strength of the sextupoles, the sextupoles could be placed inside the wiggler magnets, where a small dispersion can be available throughout the length of the magnet, requiring smaller sextupole field strength. Also, since the edge focusing is only in one plane, a large ratio between horizontal and vertical beta functions can be maintained, making the chromaticity compensation more effective.

As shown in Fig. 4, there are two dipoles on each side of the wigglers to create dispersion. The dispersion is then

amplified to the desired value by the following quadrupoles. Considering IBS, the increase of the transverse emittance, which is proportional to $H = \gamma D^2 + 2\alpha DD' + \beta D'^2$, must be minimized. The beta function in wiggler plane is chosen to be 25 m, which makes the D'^2 term of the H function two orders of magnitude bigger than the other terms. Therefore, the dispersion in the wiggler section doesn't have to be small as long as D' is kept small. In addition, to avoid the large closed orbit distortion by large dispersion, we finally set the dispersion in wiggler section to 75 cm, which works well for both chromaticity correction and dynamic aperture.

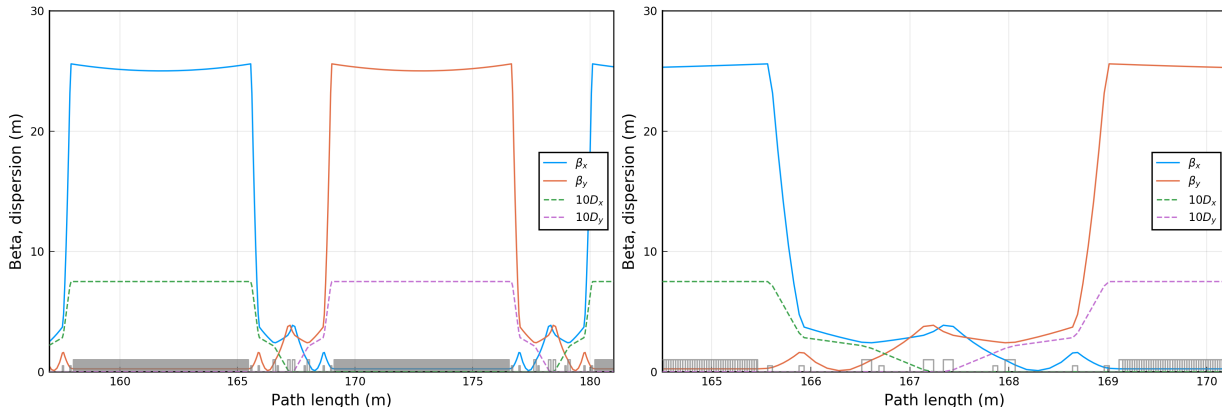


FIG. 4. Twiss functions in the wiggler and in the transition between wigglers.

In order to minimize the non-linear effect from sextupole, the phase advance over a wiggler pair needs to be $\pi/2$ or $3\pi/2$ so that the focusing kicks caused by sextupole are compensated in the next pair and orbit kicks are compensated in the second next pair. This phase advance is dominated by the beta function in the non-wiggler plane, which set to be the bend radius and therefore keeps constant. The wiggler field strength needs to be optimized to fulfill the above condition. Since wiggler field also affects the damping and IBS, we finally set the magnetic field of the wiggler to 1.88 T, which, based on the simulations, results in good beam emittance and momentum spread. The preliminary parameters of the ring cooler are summarized in Table. II.

TABLE II. Parameters of the ring cooler

Circumference [m]	449.079
Length of cooling section [m]	170
Average β function in cooling section [m]	170/280
Dispersion in arc [cm]	18.5
Wiggler field [T]	1.88
Length of wiggler [m]	7.44
Bend radius of wiggler [m]	0.246
Poles in wiggler	158
Wiggler period [cm]	4.8
β function in wiggler [m]	25
Max. Dispersion in wiggler [cm]	75
Number of wiggler magnets	16
Tune (Q_x/Q_y)	59.92/59.85
Chromaticity before correction (x/y)	-117.8/-114.4
Momentum compaction factor α	-3.21×10^{-3}
Natural emittance (x/y) [nm]	3.1/3.1
Natural momentum spread	2.6×10^{-4}

IV. BEAM PARAMETERS OF THE COOLER

A. Emittance and momentum spread

In the ring cooler, the cooling performance is directly determined by achieved electron beam quality. Based on the lattice design, the equilibrium electron beam parameters can be calculated by considering the radiation damping,

quantum excitation and the IBS effects. In addition, since the electron beam will be stored in the ring and continuously interact with hadrons, the heating effect on electrons by the hadron beam also needs to be considered, which is referred here as the Beam-Beam Scattering (BBS) effect. The differential equation of the emittance of electron beam is given by

$$\frac{d\epsilon}{dt} = (-2\lambda_{damp} + \lambda_{IBS} + \lambda_{BBS})\epsilon + C_q \quad (1)$$

where λ_{damp} is the radiation damping rate, C_q is the factor of quantum excitation, λ_{IBS} and λ_{BBS} are the heating rates from IBS and BBS, respectively. The equation of momentum spread has the same form as Eq. (1). It is known that the radiation damping rate λ_{damp} and the factor of quantum excitation C_q only depend on the ring lattice, while the heating rates from IBS λ_{IBS} and BBS λ_{BBS} depend on beam parameters dynamically. In order to get the equilibrium beam parameters in the ring cooler, a simulation code was developed which allows to perform turn-by-turn tracking.

In the simulation, the radiation damping rates are calculated from the radiation integrals [16] based on the optics of the ring. The factor of quantum excitation can be obtained by $C_q = 2\lambda_{damp}\epsilon_{nat}$, where ϵ_{nat} is the natural emittance of electron beam. The Bjorken-Mtingwa IBS model [17] with horizontal and vertical dispersion is used in the code. The code also uses fast algorithm for IBS calculation in the absence of x-y coupling [18, 19]. In our case, the IBS heating rates for electrons are close to the radiation damping rates due to the small beam emittance caused by the strong damping effect. As a result, the IBS effect is important for accurate calculation of electron beam dynamics in the simulation.

Similar to the cooling effect, the BBS effect is caused by the Coulomb interaction between the electrons and hadrons. Starting with Boltzmann transport equation, the model for such heating of electrons due to collisions with hadrons was developed using the full Landau collision integral [20] that allows for different temperatures in all three dimensions. Considering that both the electron beam and hadron beam have Gaussian velocity distribution with standard deviation σ_{v_e} and σ_{v_i} , the horizontal heating rate for electrons can be obtained as

$$\langle \dot{v}_x^2 \rangle = \frac{\gamma_{ei} n_i}{(2\pi)^3 \sigma_{v_{ex}} \sigma_{v_{ey}} \sigma_{v_{es}} \sigma_{v_{ix}} \sigma_{v_{iy}} \sigma_{v_{is}}} \frac{L_{cool}}{C} \int d^3 u \left\{ \frac{u^2 - u_x^2}{u^3} \frac{1}{\sigma_{v_{ex}}^2} I_{x,2} I_{y,0} I_{s,0} - \frac{u_x u_y}{u^3} \frac{1}{\sigma_{v_{ey}}^2} I_{x,1} I_{y,1} I_{s,0} - \frac{u_x u_s}{u^3} \frac{1}{\sigma_{v_{es}}^2} I_{x,1} I_{y,0} I_{s,1} \right\} \quad (2)$$

where $\gamma_{ei} = \frac{e_e^2 e_i^2 \ln \Lambda}{4\pi \epsilon_0^2 m_e^2}$, e_e, e_i are the charges of electron and hadron, $\ln \Lambda$ is the Coulomb logarithm, n_i is the density of hadron beam, L_{cool} is the length of cooling section and C is the circumference of the ring, $u = v_e - v_i$ is the velocity difference between electron and hadron. The simplified integrals $I_{m,n} = I\left(\frac{1}{2\sigma_{v_{em}}^2}, \frac{1}{2\sigma_{v_{im}}^2}, u_m, n\right)$ are described by

$$\begin{cases} I(\alpha, \beta, u, 0) = \sqrt{\frac{\pi}{\alpha + \beta}} \exp\left(-\frac{\alpha\beta}{\alpha + \beta} u^2\right) \\ I(\alpha, \beta, u, 1) = -\frac{\beta u}{\alpha + \beta} I(\alpha, \beta, u, 0) \\ I(\alpha, \beta, u, 2) = \left[\frac{1}{2(\alpha + \beta)} + \frac{\beta^2 u^2}{(\alpha + \beta)^2}\right] I(\alpha, \beta, u, 0). \end{cases} \quad (3)$$

The final BBS heating rate is $\lambda_{BBS,x} = \langle \dot{v}_x^2 \rangle / 2\sigma_{v_x}^2$. The vertical and longitudinal BBS rates have the form similar to Eq. (2). This model was benchmarked with the IBS effect as well as other simplified models, more details can be found in Ref. [21]. Since the beta functions at the cooling section are large, the evolution of the beam distribution along the cooling section is small and thus not included in the BBS calculation.

The simulation code, which includes all these effects described above, was used for calculation of the electron beam parameters. Based on the ring lattice and proton beam parameters listed in Table I, the evolution of the electron beam in the ring cooler with two sets of arbitrary initial parameters is shown in Fig. 5. After several turns, the electron beam converges to an equilibrium state. The equilibrium beam parameters are list in Table. III. We can see that the longitudinal BBS rate is close to the IBS heating rate which means the BBS is important for the beam dynamics in the ring cooler.

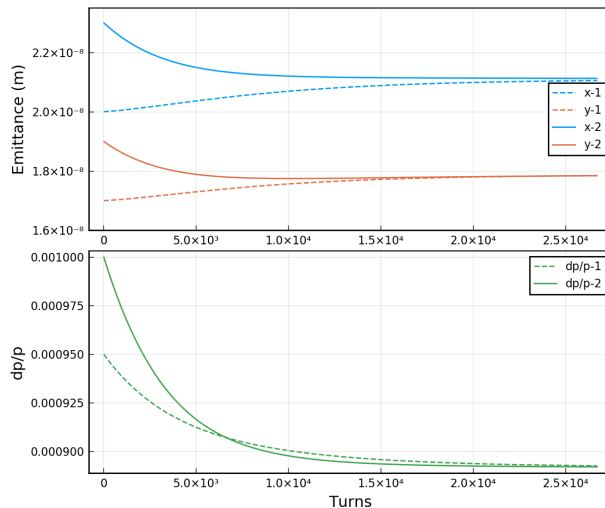


FIG. 5. Evolution of the electron beam parameters in the ring cooler with two sets of arbitrary initial parameters.

B. Dynamic aperture

In the ring cooler, there are two families of sextupoles to minimize the chromaticity. The non-linear behavior of the ring is minimized by changing the sextupole strength and the phase advance across the mid-arc and mid-wiggler adapters. Meanwhile, the off-energy closed orbit deviation is also minimized. The dynamic aperture is calculated with particle tracking using ELEGANT [22]. In the calculation, the RF cavity is included to match the longitudinal beam emittance. The coordinates of particles are recorded and tracked in 1000 turns (\sim one synchrotron period). Then the dynamic aperture is defined by the surviving particles. The tracking result is shown in Fig. 6, in which the survived particles are marked in black and lost in red. The axis are in units of sigmas. We see that the maximum dynamic apertures in horizontal, vertical and momentum planes are about $6\sigma_x$, $6\sigma_y$ and $16\delta_p$, respectively.

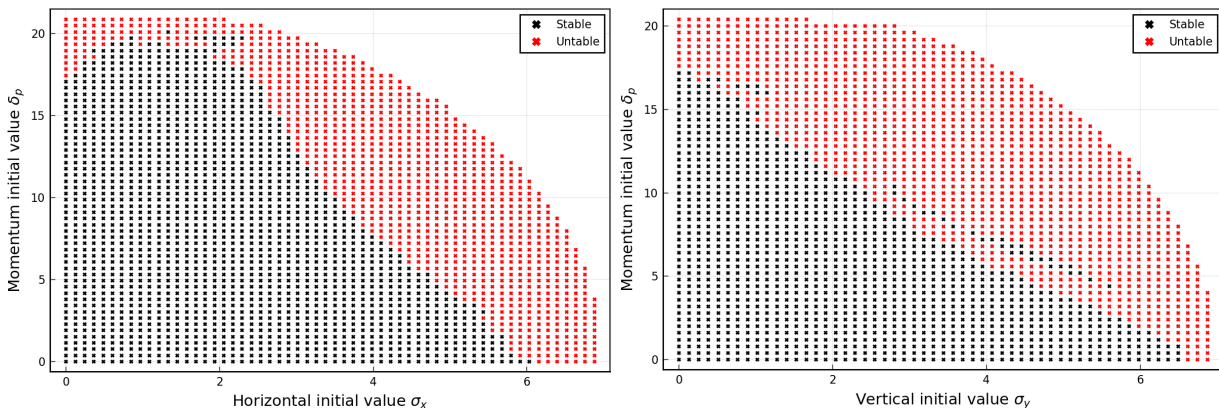


FIG. 6. Dynamic aperture tracking result by ELEGANT. (Black: survived particles, Red: lost particles)

C. Beam lifetime

For the beam in the ring cooler, the Touschek lifetime is larger than 10 hours. Therefore, in this section, we only discuss the quantum lifetime. Without consideration of collective effects, a stationary distribution of the electron beam in a storage ring can be estimated based on the heating effects, quantum fluctuation and the radiation damping. As a result of the physical and dynamic aperture, the distribution is cut off with a steady loss of particle, which defines the quantum lifetime. The 1-d quantum lifetime has been analyzed by A. Piwinski [23]. Here we give the derivation

of the 3-d quantum lifetime. Based on the same method as Piwinski, the 3-dimensional continuity equation becomes

$$\frac{\partial w}{\partial t} + \frac{\partial I_x}{\partial \epsilon_x} + \frac{\partial I_y}{\partial \epsilon_y} + \frac{\partial I_p}{\partial \delta_p^2} = 0, \quad (4)$$

where $w = w(\epsilon_x, \epsilon_y, \delta_p^2, t)$ is the beam distribution function and I is the flux of density. The beam lifetime is defined by the decay of beam density:

$$\frac{1}{\tau} = -\frac{1}{N} \frac{dN}{dt} = -\frac{1}{dt} \iiint_V w d\epsilon_x d\epsilon_y d\delta_p^2 = \iiint_V \frac{\partial I_x}{\partial \epsilon_x} + \frac{\partial I_y}{\partial \epsilon_y} + \frac{\partial I_p}{\partial \delta_p^2} d\epsilon_x d\epsilon_y d\delta_p^2 = \frac{1}{\tau_x} + \frac{1}{\tau_y} + \frac{1}{\tau_p}, \quad (5)$$

where $V = f(\epsilon_{xm}, \epsilon_{ym}, \delta_{pm}^2)$ is the beam acceptance defined by the 3-d aperture, and ϵ_{xm} , ϵ_{ym} and δ_{pm}^2 are the maximum beam emittance and momentum spread. Here we assume the 3-d aperture has an ellipsoid shape:

$$\frac{\epsilon_{xm}}{A_x^2 \hat{\epsilon}_x} + \frac{\epsilon_{ym}}{A_y^2 \hat{\epsilon}_y} + \frac{\delta_{pm}^2}{A_p^2 \hat{\delta}_p^2} = 1, \quad (6)$$

where $A_x = a/\hat{\sigma}_x$, $A_y = b/\hat{\sigma}_y$ and $A_p = c/\hat{\delta}_p$ are the ratios between aperture and rms beam size in horizontal, vertical and longitudinal planes, respectively. The lifetime, for example τ_x , can be written by

$$\frac{1}{\tau_x} = \int_0^{\epsilon_{ym}} \int_0^{\delta_{pm}^2(\epsilon_y)} I_{xm}(\epsilon_y, \delta_p^2) d\delta_p^2 d\epsilon_y. \quad (7)$$

Comparing with the Fokker-Planck equation in Ref. [23], the beam flux of density is

$$I_x = 2\lambda_x \epsilon_x M_x + \epsilon_x M_x \partial w / \partial \epsilon_x, \quad (8)$$

where λ is the effective damping rate and M is the factor of quantum excitation. Considering Gaussian distribution, the stationary beam distribution function ($\partial w / \partial t = 0$) is

$$w(\epsilon_x, \epsilon_y, \delta_p^2) = \frac{1}{8\hat{\epsilon}_x \hat{\epsilon}_y \hat{\delta}_p^2} \exp\left(-\frac{\epsilon_x}{2\hat{\epsilon}_x} - \frac{\epsilon_y}{2\hat{\epsilon}_y} - \frac{\delta_p^2}{2\hat{\delta}_p^2}\right), \quad (9)$$

where $\hat{\epsilon}_x$, $\hat{\epsilon}_y$ and $\hat{\delta}_p$ are the rms beam emittance and momentum spread, which can be written into $\hat{\epsilon}_{x,y} = 2\lambda_{x,y}/M_{x,y}$ and $\hat{\delta}_p^2 = 2\lambda_p/M_p$. Approximately, the maximum flux $I_{xm} = \int_0^{\epsilon_{xm}} \partial I_x / \partial \epsilon_x d\epsilon_x$ can be derived by

$$\frac{I_{xm}}{\epsilon_{xm}} \int_0^{\epsilon_{xm}} \exp\left(\frac{\epsilon_x}{2\hat{\epsilon}_x}\right) d\epsilon_x = M_x w(\epsilon_x = 0, \epsilon_y, \delta_p^2). \quad (10)$$

Considering $\epsilon_{xm} = A_x^2 \hat{\epsilon}_x (1 - \frac{\epsilon_y}{A_y^2 \hat{\epsilon}_y} - \frac{\delta_p^2}{A_p^2 \hat{\delta}_p^2})$ and substituting Eq.(9,10) into Eq.(7), τ_x can be calculated. With the help of *Mathematica*, the final form of the 3-d quantum lifetime is

$$\frac{1}{\tau} = A_x^2 A_y^2 A_p^2 (k_x e^{-\frac{A_x^2}{2}} + k_y e^{-\frac{A_y^2}{2}} + k_p e^{-\frac{A_p^2}{2}}) \quad (11)$$

$$k_{x,y,p} = \frac{1}{(A_{p,x,y}^2 - A_{x,y,p}^2)^2 (A_{y,p,x}^2 - A_{x,y,p}^2)^2} \{ \lambda_{x,y,p} [A_{x,y,p}^2 (A_{x,y,p}^2 - A_{y,p,x}^2 - A_{p,x,y}^2) + A_{y,p,x}^2 A_{p,x,y}^2] \\ + 2A_{x,y,p}^2 (2\lambda_{x,y,p} - \lambda_{y,p,x} - \lambda_{p,x,y}) + 2A_{y,p,x}^2 (\lambda_{p,x,y} - \lambda_{x,y,p}) + 2A_{p,x,y}^2 (\lambda_{y,p,x} - \lambda_{x,y,p}) \}.$$

The effective damping rate is $\lambda = \lambda_{damp} - \lambda_{IBS}/2 - \lambda_{BBS}/2$, which depends on the radiation damping and heating effects. If the apertures in the other two dimensions are very large, the formula agrees with the 1-d form: $\tau = \exp(\frac{A^2}{2})/(\lambda A^2)$, which is consistent with the Ref. [23]. For the ring cooler, dynamic aperture is the main limitation of the quantum lifetime. Fig. 7 gives the dependency of the quantum lifetime on the transverse aperture with $A_p = 16$. With present dynamic aperture of the ring cooler $A_x/A_y/A_p = 6/6/16$, the quantum beam lifetime is about 4.8 hours.

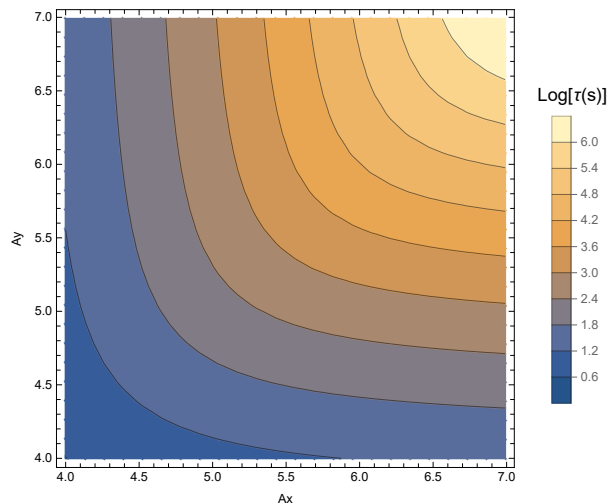


FIG. 7. The dependency of the quantum lifetime on the horizontal and vertical apertures with $A_p = 16$. ($\lambda_x/\lambda_y/\lambda_p = 5.2/5.0/5.5 \text{ s}^{-1}$)

D. Impedance and instabilities

Because of the high beam density the collective instabilities require attention. The main component of the ring impedance is the resistive wall impedance of the vacuum chamber. Other elements like bellows and BPMs should be less important because of the large bunch length. Here, we only discuss the microwave instabilities of the single bunch.

Based on bunch parameters, the threshold impedance for the longitudinal single-bunch instability is given by Boussard criterion [24]

$$\left| \frac{Z}{n} \right|^{thr} = \frac{\sqrt{2\pi\alpha} E \delta_p^2 \sigma_s}{e I_b R} = 49 \text{ m}\Omega, \quad (12)$$

where α is the momentum compaction factor, R is the average bending radius and I_b is the average bunch current. Assuming a circular copper chamber of radius $b = 3 \text{ cm}$, the effective longitudinal resistive wall impedance can be obtained:

$$\left| \frac{Z}{n} \right|_{eff}^{RW} = \frac{(1-i)C}{2\pi b \sigma_c \delta_{skin} n_{eff}} = (1-i)20 \text{ m}\Omega, \quad (13)$$

where C is the ring circumference, σ_c is the conductivity of the pipe wall, δ_{skin} is the skin depth and $n_{eff} \sim C/(2\pi\sigma_s) = 596$ is the effective harmonic. The effective wall impedance is below the threshold impedance. Besides resistive wall impedance, the coherent synchrotron radiation (CSR) effect is also important for the longitudinal instability in a electron storage ring. Usually, the CSR effect can be significantly suppressed by a shielding provided by two paralleled conducting plates. Since we have a long wiggler section, the CSR effect was investigated. Applying the model of wiggler with finite length from Ref. [25], the CSR impedance from wigglers can be calculated numerically. Based on the parameters list in Table. II, the CSR impedance for a single wiggler with a shielding gap of 2 cm and 4 cm are calculated, as shown in Fig. 8. The effective CSR impedance at the resonance frequencies for both cases is about $|Z/n|_{eff}^{CSR} = 0.1 \Omega$. In the ring cooler with a long wiggler section, the CSR impedance is much larger than the threshold. For the electron bunch, the highest frequencies might become unstable. Although we have not had a chance to do the simulations to investigate the microwave instabilities caused by CSR, with the resonance frequency corresponding to the shielding gap, one can spread the peak value out by smoothly varying the gap in the wiggler, thus reducing the impedance. Detailed study of the instabilities is left for future work.

The threshold for the transverse mode-coupling instability is

$$Z_{\perp}^{thr} = \frac{2E w_0 Q_s \tau_L}{e I_b \beta_{\perp}} = 2.0 \text{ k}\Omega/m, \quad (14)$$

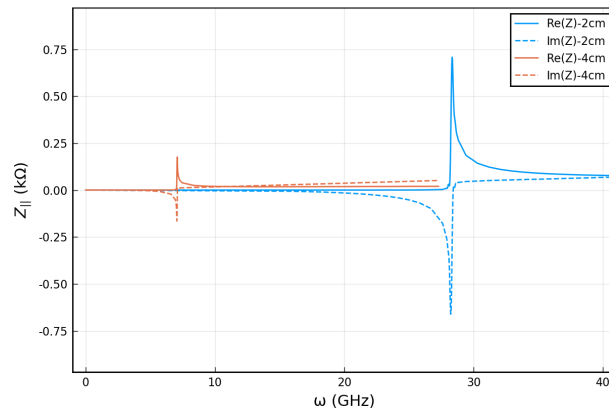


FIG. 8. CSR impedance of a single wiggler with the shielding gap of 2 cm and 4 cm.

where Q_s is the synchrotron tune, τ_L is the full bunch length and $\bar{\beta}_\perp$ is the average of the β function. The transverse resistive wall impedance can be calculated from the Panofsky-Wenzel theorem

$$Z_\perp^{RW} = \frac{2R}{b^2} \left| \frac{Z}{n} \right|_{eff}^{RW} = (1 - i)3.2 \text{ k}\Omega/m. \quad (15)$$

It shows the transverse resistive wall impedance is slightly above the threshold. This problem can be solved by choosing a larger beam pipe radius. However, we only give an estimate of the impedance and instabilities in the ring cooler, more details about the instabilities and beam dynamics on single-bunch and multi-bunches need to be further studied through simulation.

TABLE III. Electron beam parameters in the ring cooler

Beam energy [MeV]	149.8
Relativistic Factor γ	293.1
Number of electrons per bunch	3×10^{11}
Peak current [A]	48.3
Number of bunches	135
Average current [A]	4.4
RMS emittance (x/y) [nm]	21/18
RMS Momentum spread	8.9×10^{-4}
RMS Bunch length [cm]	12
Required RF voltage [kV]	6.1
Synchrotron tune Q_s	1.63×10^{-3}
Max. space charge (x/y)	0.19/0.21
Damping rates (x/y/z) [s^{-1}]	32/32/64
IBS rates (x/y/z) [s^{-1}]	54/53/68
BBS rates (x/y/z) [s^{-1}]	-0.4/1.0/49
Dynamic aperture (x/y/s)	$6\sigma/6\sigma/16\sigma$
Quantum lifetime [hour]	4.8
Touschek lifetime [hour]	> 10

In summary, the final electron beam parameters are summarized in Table III. The bunch charge of electron beam is 48 nC and the total charge in the ring is 6.5 μ C. At such high beam intensity the peak space charge tune shift is about 0.2. These numbers are challenging and should be further optimized and improved during design stage of such ring-based electron cooler. But so far, all parameter look feasible.

V. COOLING SIMULATION

In order to estimate the cooling performance of the ring cooler, a simulation code was developed, in which several effects relevant to the cooling approach were included. The B-M IBS model and the 3-d non-magnetized cooling force

were included and benchmarked with the experimental results in the Ref. [26]. In addition, the dispersion effects on electron and ion beams are also included, which are used to redistribute the cooling rates between horizontal and longitudinal direction [27–29].

At high energy, the horizontal angular spread of electron beam in the rest frame is much larger than in the longitudinal plane, which creates unbalanced cooling rates between the horizontal and longitudinal cooling. Unlike conventional low-energy electron coolers, we do not use the magnetized cooling method in our design to enhance the transverse cooling. Instead, we introduce the dispersions both for the hadron and electron beams to increase the horizontal cooling rate at the expense of the longitudinal cooling. As we known, dispersion on ions will introduce the coupling between transverse coordinate and longitudinal momentum, and thus change the beam distribution. This effect can be used to redistribute the cooling rates, and it has been measured and analyzed in Ref. [30].

Besides the dispersion on ion beam, we can also apply dispersion on electron beam in a ring-based cooler, which is also helpful to the cooling redistribution effect [28, 29]. In the simulation code, we include the electron dispersion and the dispersive cooling force is calculated based on the new electron beam distribution. We know that the cooling force depends on the electron beam distribution in 6-d phase space

$$\mathbf{F} = -4\pi n_e m_e r_e^2 Z^2 c^4 \int L_c \frac{\mathbf{u}_i - \mathbf{u}_e}{|\mathbf{u}_i - \mathbf{u}_e|^3} f_e(\mathbf{u}_e) d\mathbf{u}_e. \quad (16)$$

With the transverse dispersion D , position offset x_{off} and energy offset δ_{off} , the new density distribution (Gaussian) of electron beam in comoving frame becomes

$$n_e(r) = n_{e0} \exp\left[-\frac{(x - x_{off} - D\delta_{off})^2}{2(\epsilon_x \beta_x + D^2 \delta_p^2)} - \frac{y^2}{2\epsilon_y \beta_y} - \frac{s_0^2}{2\sigma_s^2}\right], \quad (17)$$

and the standard form of velocity distribution is

$$f_e(u_x, u_y, u_z) = \frac{1}{(2\pi)^{3/2} \sigma_1 \sigma_2 \sigma_3 \sqrt{1 - \rho^2}} \exp\left\{-\frac{1}{2(1 - \rho^2)} \left[\frac{(u_x - \bar{u}_x)^2}{\sigma_1^2} + \frac{(u_z - \bar{u}_z)^2}{\sigma_3^2} - 2\rho \frac{(u_x - \bar{u}_x)(u_z - \bar{u}_z)}{\sigma_1 \sigma_3} \right] - \frac{(u_y - \bar{u}_y)^2}{2\sigma_2^2} \right\}. \quad (18)$$

The various parameters are given by:

$$\begin{aligned} \bar{u}_x &= -\frac{\gamma \alpha_x \epsilon_x (x - x_{off} - D\delta_{off})}{\epsilon_x \beta_x + D^2 \sigma_p^2} \\ \bar{u}_y &= -\frac{\gamma \alpha_y y}{\beta_y} \\ \bar{u}_z &= \frac{D\sigma_p^2 (x - x_{off}) + \epsilon_x \beta_x \delta_{off}}{\epsilon_x \beta_x + D^2 \sigma_p^2} \\ \sigma_1^2 &= \frac{\epsilon_x \gamma^2}{\beta_x} \left(1 + \frac{\alpha_x^2 D^2 \sigma_p^2}{\epsilon_x \beta_x + D^2 \sigma_p^2}\right) \\ \sigma_2^2 &= \frac{\epsilon_y \gamma^2}{\beta_y} \\ \sigma_3^2 &= \frac{\sigma_p^2 \epsilon_x \beta_x}{\epsilon_x \beta_x + D^2 \sigma_p^2} \\ \rho &= \frac{\alpha_x D \sigma_p}{\sqrt{\epsilon_x \beta_x + D^2 \sigma_p^2 (1 + \alpha_x^2)}}. \end{aligned}$$

The cooling force is then calculated using the new distribution function given by Eq. (17-18).

In the cooling simulation code, the variation of the electron and proton beam size along the long drift cooling section is included. Actually the space charge effect will also distort the beam distribution, especially for the electron beam. Taking into account the space charge force from electron and proton beams, the evolution of the rms electron beam size and angular spread along cooling section was calculated, as shown in Fig. 9. Since the charge density of electron beam is higher than proton beam, the distortion is mainly due to the electron beam space charge force. Fig. 9 shows that the effect of space charge on the beam distribution is less than 2%, which does not have a significant effect on the cooling force. Therefore, for simplicity, the space charge effect is not included in present simulation.

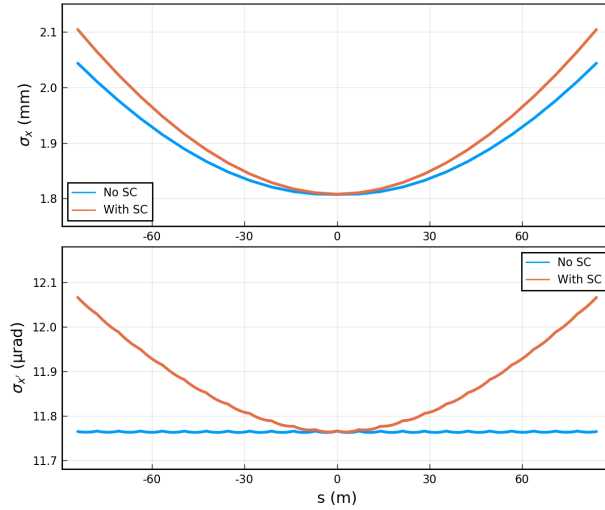


FIG. 9. Evolution of the rms electron beam size and angle spread along cooling section with and without the space charge effect ($\beta_i^* = 100 m$).

Finally, cooling simulation is performed with the electron beam parameters list in Table III. Fig. 10 shows the evolution of the hadron beam transverse and longitudinal emittance with cooling. The beta function of hadron beam in the center of cooling section is $\beta^* = 100 m$. When there is no dispersion, it shows that there is almost no transverse cooling but a strong longitudinal cooling, which is due to the large difference in cooling gradients. By applying the dispersion both for the proton and electron beam in the cooling section with $D_i = 2.5 m$ and $D_e = 2 m$, the proton beam can be cooled more effectively in the horizontal plane. With cooling, the proton beam emittance is essentially unchanged within two hours, which is close to the requirement in the EIC.

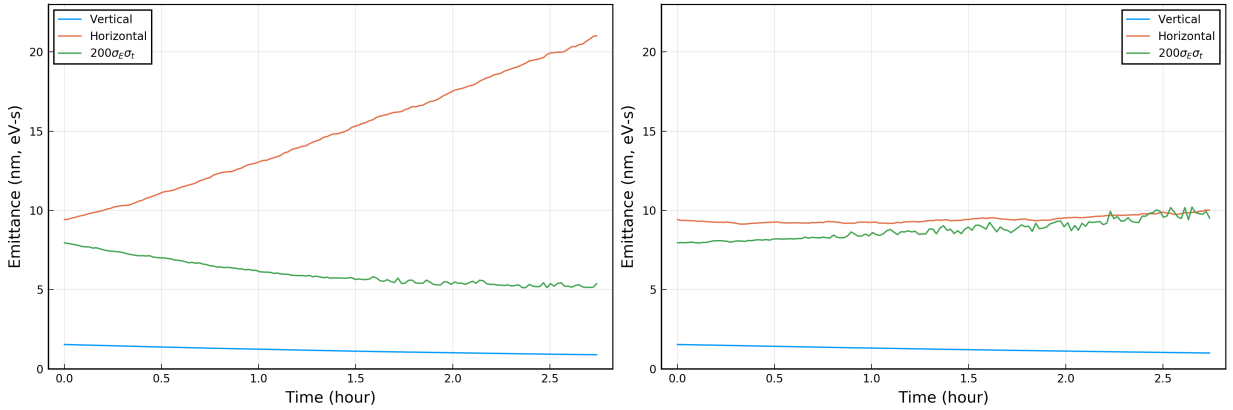


FIG. 10. The evolution of the hadron beam emittance during cooling. (Left plot: $D_i = 0 m$, $D_e = 0 m$, Right plot: $D_i = 2.5 m$, $D_e = 2 m$)

However, dispersion will affect the IBS rate as well as BBS rate on electron beam, which means that the equilibrium state of electron beam in the ring cooler might be different. We didn't include this effect so far. Moreover, for the present design, the beam sizes of the proton beam and the electron beam in the cooling section are not well matched. More optimization and matching work need to be done in the future.

VI. SUMMARY

The hadron beam cooling at high energy is an important part of the EIC. In this paper, we present a possible design of such high-energy ring-based electron cooler using bunched electron beam. The electron beam can continuously cool the hadrons while electrons are being cooled by the radiation damping in the storage ring. This approach strongly depends on the design of electron ring which is described here in detail. The electron beam parameters in such ring

cooler are calculated taking into account several effects. In addition to the radiation damping, quantum excitation and IBS, the electron beam in the ring cooler is affected by the BBS effect. In this paper, we used the model of the BBS effect which was derived directly from the collision integral. We also generalized treatment of quantum lifetime of the electron beam to 3-d.

Based on such ring cooler design, the cooling performance on the hadron beam was simulated, in which the dispersions of the ion and electron beams in the cooling section were effectively employed to redistribute the cooling rate between the longitudinal and horizontal planes. Although there are still some challenges which have to be addressed during the design stage of such a cooler, it appears that the ring-based electron cooler concept, presented in this paper, offers a viable path for cooling of protons at the top energy in the EIC.

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